

SLAS205B − DECEMBER 1998 − REVISED OCTOBER 2003

- **8-Bit Resolution 80 MSPS Sampling Analog-to-Digital Converter (ADC)**
- **Low Power Consumption: 165 mW Typ Using External references**
- **Wide Analog Input Bandwidth: 700 MHz Typ**
- **3.3 V Single-Supply Operation**
- **3.3 V TTL/CMOS-Compatible Digital I/O**
- **Internal Bottom and Top Reference Voltages**
- **Adjustable Reference Input Range**
- **Power Down (Standby) Mode**
- **Separate Power Down for Internal Voltage References**
- **Three-State Outputs**
- **28-Pin Small Outline IC (SOIC) and Thin Shrink SOP (TSSOP) Packages**
- **Applications**
	- **− Digital Communications**
	- **− Flat Panel Displays**
	- **− High-Speed DSP Front-End (TMS320C6000)**
	- **− Medical Imaging**
	- **− Graphics Processing (Scan Rate/Format Conversion)**
	- **− DVD Read Channel Digitization**

#### **DESCRIPTION**

The TLV5580 is an 8-bit 80 MSPS high-speed A/D converter. It converts the analog input signal into 8-bit binary-coded digital words up to a sampling rate of 80 MHz. All digital inputs and outputs are 3.3 V TTL/CMOS-compatible.

The device consumes very little power due to the 3.3 V supply and an innovative single-pipeline architecture implemented in a CMOS process. The user obtains maximum flexibility by setting both bottom and top voltage references from user-supplied voltages. If no external references are available, on-chip references are available for



internal and external use. The full-scale range is 1 Vpp up to 1.6 Vpp, depending on the analog supply voltage. If external references are available, the internal references can be disabled independently from the rest of the chip, resulting in an even greater power saving.

While usable in a wide variety of applications, the device is specifically suited for the digitizing of high-speed graphics and for interfacing to LCD panels or LCD/DMD projection modules . Other applications include DVD read channel digitization, medical imaging and communications. This device is suitable for IF sampling of communication systems using sub-Nyquist sampling methods because of its high analog input bandwidth.



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The single-pipeline architecture uses 6 ADC/DAC stages and one final flash ADC. Each stage produces a resolution of 2 bits. The correction logic generates its result using the 2-bit result from the first stage, 1 bit from each of the 5 succeeding stages, and 1 bit from the final stage in order to arrive at an 8-bit result. The correction logic ensures no missing codes over the full operating temperature range.



#### **PACKAGE/ORDERING INFORMATION**

(1) For the most current specifications and package information, refer to our web site at www.ti.com.



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#### **CIRCUIT DIAGRAMS OF INPUTS AND OUTPUTS**





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### **Terminal Functions**





#### **ABSOLUTE MAXIMUM RATINGS OVER OPERATING FREE-AIR TEMPERATURE (unless otherwise noted)†**



(1) †Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### **RECOMMENDED OPERATING CONDITIONS OVER OPERATING FREE-TEMPERATURE RANGE**

#### **POWER SUPPLY**



#### **ANALOG AND REFERENCE INPUTS**



#### **DIGITAL INPUTS**





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# **ELECTRICAL CHARACTERISTICS OVER RECOMMENDED OPERATING CONDITIONS WITH FCLK = 80 MSPS AND USE OF EXTERNAL VOLTAGE REFERENCES (unless otherwise noted)**

#### **POWER SUPPLY**



#### **DIGITAL LOGIC INPUTS**



 $\dagger$ I<sub>IH</sub> leakage current on other digital inputs (OE, STDBY, PWDN\_REF) is not measured since these inputs have an internal pull-down resistor of 4 KΩ to DGND.

#### **LOGIC OUTPUTS**



#### **ELECTRICAL CHARACTERISTICS OVER RECOMMENDED OPERATING CONDITIONS WITH FCLK = 80 MSPS AND USE OF EXTERNAL VOLTAGE REFERENCES (unless otherwise noted)**

#### **DC ACCURACY**



1. Integral nonlinearity refers to the deviation of each individual code from a line drawn from zero to full scale. The point used as zero occurs 1/2 LSB before the first code transition. The full−scale point is defined as a level 1/2 LSB beyond the last code transition. The deviation is measured from the center of each particular code to the true straight line between these two endpoints.

- 2. An ideal ADC exhibits code transitions that are exactly 1 LSB apart. DNL is the deviation from this ideal value. Therefore this measure indicates how uniform the transfer function step sizes are. The ideal step size is defined here as the step size for the device under test (i.e., (last transition level – first transition level) ÷ (2n – 2)). Using this definition for DNL separates the effects of gain and offset error. A minimum DNL better than –1 LSB ensures no missing codes.
- 3. Zero error is defined as the difference in analog input voltage − between the ideal voltage and the actual voltage − that will switch the ADC output from code 0 to code 1. The ideal voltage level is determined by adding the voltage corresponding to 1/2 LSB to the bottom reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

Full-scale error is defined as the difference in analog input voltage – between the ideal voltage and the actual voltage – that will switch the ADC output from code 254 to code 255. The ideal voltage level is determined by subtracting the voltage corresponding to 1.5 LSB from the top reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

#### **ANALOG INPUT**



#### $R$ **EFERENCE INPUT (AV**<sub>DD</sub> = DV<sub>DD</sub> = DRV<sub>DD</sub> = 3.6 V)



#### **REFERENCE OUTPUTS**





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## **ELECTRICAL CHARACTERISTICS OVER RECOMMENDED OPERATING CONDITIONS WITH FCLK = 80 MSPS AND USE OF EXTERNAL VOLTAGE REFERENCES (unless otherwise noted) (continued) DYNAMIC PERFORMANCE†**



†Based on analog input voltage of −1 dBFS referenced to a 1.3 V<sub>pp</sub> full-scale input range and using the external voltage references at  $f_{\text{Clk}}$  = 80 MSPS with AV<sub>DD</sub> = DV<sub>DD</sub> = 3.3 V and DRV<sub>DD</sub> = 3.0 V at 25°C.

4. The analog input bandwidth is defined as the maximum frequency of a −1 dBFS input sine that can be applied to the device for which an extra 3 dB attenuation is observed in the reconstructed output signal.



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#### **ELECTRICAL CHARACTERISTICS OVER RECOMMENDED OPERATING CONDITIONS WITH FCLK = 80 MSPS AND USE OF EXTERNAL VOLTAGE REFERENCES (unless otherwise noted) (continued)**

#### **TIMING REQUIREMENTS**



5. Output timing  $t_{d(0)}$  is measured from the 1.5 V level of the CLK input falling edge to the 10%/90% level of the digital output. The digital output load is not higher than 10 pF.

Output hold time t<sub>h(o)</sub> is measured from the 1.5 V level of the CLK input falling edge to the 10%/90% level of the digital output. The digital output is load is not less than 2 pF.

Aperture delay  $t_{d(A)}$  is measured from the 1.5 V level of the CLK input to the actual sampling instant.

The OE signal is asynchronous.

OE timing t<sub>dis</sub> is measured from the V<sub>IH(MIN)</sub> level of OE to the high-impedance state of the output data. The digital output load is not higher than 10 pF.

OE timing t<sub>en</sub> is measured from the V<sub>IL(MAX</sub>) level of OE to the instant when the output data reaches V<sub>OH(min)</sub> or V<sub>OL(max)</sub> output levels. The digital output load is not higher than 10 pF.

6. The number of clock cycles between conversion initiation on an input sample and the corresponding output data being made available from the ADC pipeline. Once the data pipeline is full, new valid output data is provided on every clock cycle. In order to know when data is stable on the output pins, the output delay time  $t_{d(0)}$  (i.e., the delay time through the digital output buffers) needs to be added to the pipeline latency. Note that since the max.  $t_{d(o)}$  is more than 1/2 clock period at 80 MHz; data cannot be reliably clocked in on a rising edge of CLK at this speed. The falling edge should be used.







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**Figure 3. INL vs Input Code At 80 MSPS (With External Reference, PW Package)**



### **PERFORMANCE PLOTS AT 25**°**C (Continued)**



**Figure 4. S/(THD+N) vs VIN At 80 MSPS (Internal Reference), 60 MSPS (External Reference), 40 MSPS (External Reference)**



**Figure 5. Spectral Plot fIN = 1.011 MHz At 60 MSPS**



#### **PERFORMANCE PLOTS AT 25**°**C (Continued)**







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### **PERFORMANCE PLOTS AT 25**°**C (Continued)**



**Figure 11. ADC Output Power With Respect To −1 dBFS VIN (Internal Reference, DW Package)**





### **PRINCIPLE OF OPERATION**

The TLV5580 implements a high-speed 80 MSPS converter in a cost-effective CMOS process. Powered from 3.3 V, the single-pipeline design architecture ensures low-power operation and 8 bit accuracy. Signal input and clock signals are all single-ended. The digital inputs are 3.3 V TTL/CMOS compatible. Internal voltage references are included for both bottom and top voltages. Therefore the converter forms a self-contained solution. Alternatively the user may apply externally generated reference voltages. In doing so, both input offset and input range can be modified to suit the application.

A high-speed sampling-and-hold captures the analog input signal. Multiple stages will generate the output code with a pipeline delay of 4.5 CLK cycles. Correction logic combines the multistage data and aligns the 8-bit output word. All digital logic operates at the rising edge of CLK.

#### **ANALOG INPUT**



**Figure 12. Simplified Equivalent Input Circuit**

A first-order approximation for the equivalent analog input circuit of the TLV5580 is shown in Figure 12. The equivalent input capacitance C<sub>I</sub> is 4 pF typical. The input must charge/discharge this capacitance within the sample period of one half clock cycle. When a full-scale voltage step is applied, the input source provides the charging current through the switch resistance  $R_{SW}$  (200  $\Omega$ ) of S1 and quickly settles. In this case the input impedance is low. Alternatively, when the source voltage equals the value previously stored on C<sub>I</sub>, the hold capacitor requires no input current and the equivalent input impedance is very high.

To maintain the frequency performance outlined in the specifications, the total source impedance should be limited to about 80 Ω, as follows from the equation with f<sub>CLK</sub> = 80 MHz, C<sub>I</sub> = 4 pF, R<sub>SW</sub> = 200 Ω:

$$
R_{S} < \left[1 \div \left(2f_{CLK} \times C_{I} \times \ln(256)\right) - R_{SW}\right]
$$

So, for applications running at a lower  $f_{CLK}$ , the total source resistance can increase proportionally.



#### **PRINCIPLE OF OPERATION**



**Figure 13. DC-Coupled Input Circuit**

For dc-coupled systems an op amp can level-shift a ground-referenced input signal. A circuit as shown in Figure 13(a) is acceptable. Alternatively, the user might want a bipolar shift together with the bottom reference voltage as seen in Figure 13(b). In this case the AIN voltage is given by:

$$
AIN = 2 \times R_2 \div (R_1 + R_2) \times V_{REF} - V_{IN}
$$

**AC COUPLED INPUT**





For many applications, especially in single supply operation, ac coupling offers a convenient way for biasing the analog input signal at the proper signal range. Figure 14 shows a typical configuration. To maintain the outlined specifications, the component values need to be carefully selected. The most important issue is the positioning of the 3 dB high-pass corner point f\_<sub>3 dB</sub>, which is a function of R<sub>2</sub> and the parallel combination of  $C_1$  and  $C_2$ , called  $C_{eq}$ . This is given by the following equation:

$$
f_{-3 \text{ dB}} = 1 \div (2\pi \times R_2 \times C_{\text{eq}})
$$

where  $C_{eq}$  is the parallel combination of  $C_1$  and  $C_2$ .

Since C1 is typically a large electrolytic or tantalum capacitor, the impedance becomes inductive at higher frequencies. Adding a small ceramic or polystyrene capacitor, C2 of approximately 0.01 µF, which is not inductive within the frequency range of interest, maintains low impedance. If the minimum expected input signal frequency is 20 kHz, and R2 equals 1 kΩ and R1 equals 50  $\Omega$ , the parallel capacitance of C1 and C2 must be a minimum of 8 nF to avoid attenuating signals close to 20 kHz.



### **PRINCIPLE OF OPERATION**

#### **REFERENCE TERMINALS**

The voltages on terminals REFBI and REFTI determine the TLV5580's input range. Since the device has an internal voltage reference generator with outputs available on REFBO respectively REFTO, corresponding terminals can be directly connected externally to provide a contained ADC solution. Especially at higher sampling rates, it is advantageous to have a wider analog input range. The wider analog input range is achievable by using external voltage references (e.g., at  $AVDD = 3.3$  V, the full scale range can be extended from 1 Vpp (internal reference) to 1.3 Vpp (external reference) as shown in Table 1). These voltages should not be derived via a voltage divider from a power supply source. Instead, use a bandgap-derived voltage reference to derive both references via an op amp circuit. Refer to the schematic of the TLV5580 evaluation module for an example circuit.

When using external references, the full-scale ADC input range and its dc position can be adjusted. The full-scale ADC range is always equal to  $V_{REFT} - V_{REFB}$ . The maximum full-scale range is dependent on AV<sub>DD</sub> as shown in the specification section. In addition to the limitation on their difference, VREFT and VREFB each also have limits on their useful range. These limits are also dependent on  $AV<sub>DD</sub>$ . Table 3 summarizes these limits for 3 cases.



#### **Table 1. Recommended Operating Modes**

#### **DIGITAL INPUTS**

The digital inputs are CLK, STDBY, PWDN\_REF, and OE. All these signals, except CLK, have an internal pull-down resistor to connect to digital ground. This provides a default active operation mode using internal references when left unconnected.

The CLK signal at high frequencies should be considered as an analog input. Overshoot/undershoot should be minimized by proper termination of the signal close to the TLV5580. An important cause of performance degradation for a high-speed ADC is clock jitter. Clock jitter causes uncertainty in the sampling instant of the ADC, in addition to the inherent uncertainty on the sampling instant caused by the part itself, as specified by its aperture jitter. There is a theoretical relationship between the frequency (f) and resolution ( $2^N$ ) of a signal that needs to be sampled and the maximum amount of aperture error dt<sub>max</sub> that is tolerable. The following formula shows the relation:

$$
dt_{\text{max}} = 1 \div \left[ \pi f 2^{(N+1)} \right]
$$

As an example, for an 8−bit converter with a 15-MHz input, the jitter needs to be kept <41 pF in order not to have changes in the LSB of the ADC output due to the total aperture error.



### **PRINCIPLE OF OPERATION**

#### **DIGITAL OUTPUTS**

The output of TLV5580 is a standard binary code. Capacitive loading on the output should be kept as low as possible (a maximum loading of 10 pF is recommended) to provide best performance. Higher output loading causes higher dynamic output currents and can increase noise coupling into the device's analog front end. To drive higher loads, use an output buffer is recommended.

When clocking output data from TLV5580, it is important to observe its timing relation to CLK. Pipeline ADC delay is 4.5 clock cycles to which the maximum output propagation delay is added. See Note 6 in the specification section for more details.

#### **LAYOUT, DECOUPLING AND GROUNDING RULES**

It is necessary for any PCB using the TLV5580 to have proper grounding and layout to achieve the stated performance. Separate analog and digital ground planes that are spliced underneath the device are advisable. TLV5580 has digital and analog terminals on opposite sides of the package to make proper grounding easier. Since there is no internal connection between analog and digital grounds, they have to be joined on the PCB. Joining the digital and analog grounds at a point in close proximity to the TLV5580 is advised.

As for power supplies, separate analog and digital supply terminals are provided on the device  $(AV_{DD}/DV_{DD})$ . The supply to the digital output drivers is kept separate also (DRV<sub>DD</sub>). Lowering the voltage on this supply from the nominal 3.3 V to 3 V improves performance because of the lower switching noise caused by the output buffers.

Due to the high sampling rate and switched-capacitor architecture, TLV5580 generates transients on the supply and reference lines. Proper decoupling of these lines is essential. Decoupling as shown in the schematic of the TLV5580 EVM is recommended.



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### **TLV5580 EVALUATION MODULE**

#### **TLV5580 EVALUATION MODULE**

TI provides an evaluation module (EVM) for TLV5580. The EVM also includes a 10-bit 80 MSPS DAC so that the user can convert the digitized signal back to the analog domain for functional testing. Performance measurements can be done by capturing the ADC's output data.

The EVM provides the following additional features:

- Provision of footprint for the connection of an onboard crystal oscillator, instead of using an external clock input.
- Use of TLV5580 internal or external voltage references. In the case of external references, an onboard circuit is used that derives adjustable bottom and top reference voltages from a bandgap reference. Two potentiometers allow for the independent adjustments of both references. The full scale ADC range can be adjusted to the input signal amplitude.
- All digital output, control signal I/O (output enable, standby, reference power-down) and clock I/O are provided on a single connector. The EVM can thus be part of a larger (DSP) system for prototyping.
- Onboard prototyping area with analog and digital supply and ground connections.

Figure 15 shows the EVM schematic.

The EVM is factory shipped for use in the following configuration:

- Use of external (onboard) voltage references
- External clock input

#### **ANALOG INPUT**

A signal in the range between V<sub>(REFBI)</sub> and V<sub>(REFTI)</sub> should be applied to avoid overflow/underflow on connector J10. This signal is onboard terminated with 50Ω. There is no onboard biasing of the signal. When using external (onboard) references, these levels can be adjusted with R7 ( $V_{(REFII)}$ ) and R6 ( $V_{(REFBI)}$ ). Adjusting R7 causes both references to shift. R6 only impacts the bottom reference. The range of these signals for which the device is specified depends on  $AV<sub>DD</sub>$  and is shown under the Recommended Operating Conditions.

Internally generated reference levels are also dependent on  $AV<sub>DD</sub>$  as shown in the electrical characteristics section.

#### **CLOCK INPUT**

A clock signal should be applied with amplitudes ranging from 0 to  $AV<sub>DD</sub>$  with a frequency equal to the desired sampling frequency on connector J9. This signal is onboard terminated with 50  $\Omega$ . Both ADC and DAC run off the same clock signal. Alternatively the clock can be applied from terminal 1 on connector J11. A third option is using a crystal oscillator. The EVM board provides the footprint for a crystal oscillator that can be populated by the end-user, depending on the desired frequency. The footprint is compatible with the Epson EG-8002DC series of programmable high-frequency crystal oscillators. Refer to the TLV5580 EVM Settings for selecting between the different clock modes.

### **TLV5580 EVALUATION MODULE**

#### **POWER SUPPLIES**

The board provides seven power supply connectors (see Table 2). For optimum performance, analog and digital supplies should be kept separate. Using separate supplies for the digital logic portion of  $TLV5580$  (DV<sub>DD</sub>) and its output drivers (DRV<sub>DD</sub>) benefits dynamic performance, especially when DRV<sub>DD</sub> is put at the minimum required voltage (3 V), while DV<sub>DD</sub> might be higher (up to 3.6 V). This lowers the switching noise on the die caused by the output drivers.



#### **Table 2. Power Supplies**

#### **VOLTAGE REFERENCES**

SW1 and SW2 switch between internal and external top and bottom references respectively. The external references are onboard generated from a stable bandgap-derived 3.3 V signal (using TI's TPS7133 and quad-op amp TLE2144). They can be adjusted via potentiometers R6 (V<sub>(REFBI)</sub>) and R7 (V<sub>(REFTI)</sub>). It is advised to power down the internal voltage references by asserting PWN\_REF when onboard references are used.

The references are measured at test points TP3 ( $V_{(REFB)}$ ) and TP4 ( $V_{(REFT)}$ ).

#### **DAC OUTPUT**

The onboard DAC is a 10-bit 80 MSPS converter. It is connected back-to-back to the TLV5580. While the user could use its analog output for measurements, the DAC output is directly connected to connector J8 and does not pass through an analog reconstruction filter. So mirror spectra from aliased signal components feed through into the analog output.

For this reason and to separate ADC and DAC contributions, performance measurements should be made by capturing the ADC output data available on connector J11 and not by evaluating the DAC output.



### **TLV5580 EVALUATION MODULE**

### **TLV5580 EVM SETTINGS**

#### **CLOCK INPUT SETTINGS**





### **TLV5580 EVALUATION MODULE**

#### **CONTROL SETTINGS (Continued)**





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**Figure 15. EVM Schematic**

### **TLV5580 EVALUATION MODULE**





**Digital +3.3 V (DVDD)**



**Digital +3.3 V (DRVDD)**







**Figure 15. EVM Schematic (Continued)**

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**Top Overlay**

**Figure 15. EVM Schematic (Continued)**







**Top Layer**

**Figure 15. EVM Schematic (Continued)**



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### **TLV5580 EVALUATION MODULE**



**Internal Plane 1**

**Figure 15. EVM Schematic (Continued)**







**Internal Plane 2**

**Figure 15. EVM Schematic (Continued)**



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**Drill Drawing for Through Hole**

**Figure 15. EVM Schematic (Continued)**









**Bottom Layer**

**Figure 15. EVM Schematic (Continued)**



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### **TLV5580 EVALUATION MODULE**

#### **Table 3. TLV5580EVM Bill of Material**



† Manufacturer and part number data for reference only. Equivalent parts might be substituted on the EVM.



### **TLV5580 EVALUATION MODULE**

### **Table 3. TLV5580EVM Bill of Material (Continued)**



† Manufacturer and part number data for reference only. Equivalent parts might be substituted on the EVM.



#### **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

**(2)** Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

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**(3)** MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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 $DW$  (R-PDSO-G28)

PLASTIC SMALL OUTLINE



NOTES:

A. All linear dimensions are in inches (millimeters). Dimensioning and tolerancing per ASME Y14.5M-1994.

B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion not to exceed 0.006 (0,15).

D. Falls within JEDEC MS-013 variation AE.



### **LAND PATTERN DATA**



NOTES:

A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Refer to IPC7351 for alternate board design.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



PW (R-PDSO-G28)

PLASTIC SMALL OUTLINE



This drawing is subject to change without notice. **B.** 

 $\hat{\mathbb{C}}$  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.

 $\hat{\mathbb{D}}$  Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.

E. Falls within JEDEC MO-153



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