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TMC2240 36V 2ARMS+ Smart Integrated Stepper Driver with S/D and SPI

General Description

The TMC2240 is a smart high-performance stepper motor driver IC with serial communication interfaces (SPI, UART) and extensive diagnosis capabilities.

It combines industries' most advanced stepper motor driver based on the 256 microsteps built-in indexer and two fully integrated $36V$, $3.0A_{MAX}$ H-Bridges plus non-dissipative integrated current sensing (ICS).

ADI-Trinamic's StealthChop2 chopper ensures absolutely noiseless operation combined with maximum efficiency and best motor torque.

High integration, high energy efficiency, and a small form factor enable miniaturized and scalable systems for costeffective solutions while giving best in class performance.

The H-Bridge FETs have very low impedance resulting in high driving efficiency and minimal heat generated. The typical total R_{ON} (high side + low side) is 0.23Ω.

The maximum output current per H-Bridge is I_{MAX} = 5.0A_{MAX} limited by the Overcurrent Protection (OCP).

The maximum RMS current per H-Bridge is I_{RMS} = 2.1ARMS at room temperature assuming a 4-layers PCB.

The maximum full-scale current per H-Bridge is $I_{FS} = 3.0A$ and can be set by an external resistor connected to IREF. This current is defined as the maximum current setting of the embedded current drive regulation circuit. The nondissipative ICS eliminates the bulky external power resistors resulting in a dramatic space and power saving compared with mainstream applications based on external sense resistor.

The TMC2240 features abundant diagnostics and protections such as short protection/OCP, thermal shutdown, undervoltage lockout (UVLO).

During thermal shutdown and UVLO events, the driver is disabled.

Furthermore, the TMC2240 provides functions to measure the driver temperature, estimate the motor temperature, and measure one external analog input.

The TMC2240 is available in a small TQFN32 5mm x 5mm package and a thermally optimized TSSOP38 9.7mm x 4.4mm with exposed pad.

Applications

- Textile, Sewing Machines, Knitting Machines
- Lab and Factory Automation
- 3D Printers, ID Printers/Card Printers
- Liquid Handling, Medical Applications
- Office Automation and Paper Handling
- POS, Massage Chairs
- ATM, Cash Recycler, Bill Validators, Cash Machines
- CCTV, Security
- Pumps and Valve Control
- Heliostat and Antenna Positioning

Benefits and Features

- Voltage Range 4.5V to 36V DC
- \bullet Low R_{DS(ON)} (HS + LS): 230mΩ Typical (T_A = 25°C)
- Current Ratings per H-Bridge (Typical at 25°C):
	- I_{MAX} = 5.0A (Bridge Peak Current) • $I_{RMS} = 2.1A_{RMS}$ (3A Sine Wave Peak)
- Fully Integrated Lossless Current Sensing
- Step/Direction (S/D) Interface with MicroPlyer Step Interpolation
- SPI and Single Wire UART
- Incremental Encoder Interface
- Highest Resolution 256 Microsteps per Full Step
- Flexible Wave Table and Phase Shift to Match Motor
- StealthChop2 Silent Motor Operation
- SpreadCycle Highly Dynamic Motor Control Chopper
- Jerk-Free Combination of StealthChop2 and **SpreadCycle**
- StallGuard2 and StallGuard4 Sensorless Motor Load **Detection**
- CoolStep Current Control for Energy Savings up to 75%
- Passive Braking and Freewheeling Mode
- Motor Phase and Chip Temperature Measurement
- General-Purpose Analog Input
- Full Protection and Diagnostics
- Overvoltage Protection Output
- Compact 5mm x 5mm TQFN32 package or 9.7mm x 4.4mm TSSOP38

Ordering Information appears at end of data sheet. 19-101548; Rev 0; 7/22

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Simplified Block Diagram

TMC2240

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Absolute Maximum Ratings

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for
extended periods may affect device reliabi

Package Information

TQFN32 5mm x 5mm

TSSOP38 9.7mm x 4.4mm EP

For the latest package outline information and land patterns (footprints), go to *www.maximintegrated.com/packages*. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to *www.maximintegrated.com/thermal-tutorial*.

Electrical Characteristics

Pin Configurations

TMC2240 TQFN Pin Configuration

TMC2240 TSSOP Pin Configuration

TMC2240 36V 2ARMS⁺ Smart Integrated Stepper Driver with S/D and SPI

Pin Description

Pin Description (continued)

Pin Description (continued)

Functional Diagrams

TMC2240

Figure 1. Block Diagram

Detailed Description

Principles of Operation

Step and Direction Driver with Serial Interface and Diagnostic Feedback

The TMC2240 is a smart Step and Direction stepper motor driver with serial interface (SPI, UART) for parameterization and monitoring & diagnostics.

An external high-performance motion controller like the TMC4361A or a CPU generates step and direction signals synchronized to other components like additional motors within the system. The TMC2240 takes care of intelligent current control and provides feedback on the state of the motor via one of its serial interfaces.

Figure 2. Block Diagram with Typical External Components

Key Concepts

The TMC2240 implements advanced features which are exclusive to ADI-Trinamic products. These features contribute toward greater precision, greater energy efficiency, higher reliability, smoother motion, and cooler operation in many stepper motor applications.

In addition to these performance enhancements, ADI-Trinamic motor drivers offer safeguards to detect and protect against shorted outputs, output open-circuit, overtemperature, and undervoltage conditions to enhance safety and recovery from equipment malfunctions.

Control Interfaces

The TMC2240 supports both, an SPI interface and a UART-based single wire interface with CRC checking. Selection of the actual interface combination is done through the UART_EN pin, which can be hardwired to GND or V_{CC} IO depending on the desired interface selection.

The SPI interface is a bit-serial interface synchronous to a bus clock. For every bit sent from the bus master to the bus slave another bit is sent simultaneously from the slave to the master. Communication between an SPI master and a TMC2240 slave always consists of sending one 40-bit command word and receiving one 40-bit status word.

The single-wire interface allows a bidirectional single wire interfacing. It can be driven by any standard UART. No baud rate configuration is required.

Step and Direction Interface

The motor is controlled using a step and a direction input. Active edges on the STEP input can be rising edges or both rising and falling edges as controlled by mode bit (*dedge*). Using both edges cuts the toggle rate of the STEP signal in half, which is useful for control over slow interfaces such as optically isolated couplers. On each active edge, the state sampled from the DIR input determines whether to step forward or back. Each step can be a fullstep or a microstep, in which there are 2, 4, 8, 16, 32, 64, 128, or 256 microsteps per fullstep. A step impulse with a low state on DIR increases the microstep counter and a high state decreases the counter by an amount controlled by the microstep resolution. An internal table translates the counter value into the sine and cosine values which control the motor current for microstepping.

Automatic Standstill Power Down

An automatic current reduction drastically reduces application power dissipation and cooling requirements. A reduction to half of the run current reduces standstill power dissipation to roughly 25%. Standstill current, delay time, and decay parameters can be configured via the serial control interfaces.

Automatic freewheeling and passive motor braking are provided as an option for stand still. Passive braking reduces motor standstill power consumption to zero, while still providing effective dampening and braking!

Figure 3. Automatic Motor Current Control at Standstill and Ramp-up

StealthChop2 and SpreadCycle Driver

StealthChop is a voltage-chopper based principle. It especially guarantees that the motor is absolutely quiet in standstill and in slow motion, except for noise generated by ball bearings. Unlike other voltage mode choppers, StealthChop2 does not require any configuration. It automatically learns the best settings during the first motion after power up and further optimizes the settings in subsequent motions. An initial homing sequence is sufficient for learning. Optionally, initial learning parameters can be loaded to the register set. StealthChop2 allows high motor dynamics, by reacting at once to a change of motor velocity.

For highest velocity applications, SpreadCycle is an option to StealthChop2. StealthChop2 and SpreadCycle may even be used in a combined configuration for the best of both worlds: StealthChop2 for no-noise standstill, silent and smooth performance, SpreadCycle at higher velocity for high dynamics and highest peak velocity at low vibration.

SpreadCycle is an advanced cycle-by-cycle chopper mode. It offers smooth operation and good resonance dampening over a wide range of speed and load. The SpreadCycle chopper scheme automatically integrates and tunes fast decay cycles to guarantee smooth zero-crossing performance.

Benefits

- Significantly improved microstepping with low-cost motors
- Motor runs smooth and quiet
- Absolutely no standby noise
- Reduced mechanical resonance improves torque output

StallGuard – Mechanical Load Sensing

StallGuard2 provides an accurate measurement of the load on the motor. It can be used for stall detection as well as other uses at loads below those which stall the motor, such as CoolStep load-adaptive current reduction. This gives more information on the drive allowing functions like sensorless homing and diagnostics of the drive mechanics. While StallGuard2 combines with SpreadCycle chopper, StallGuard4 uses a different principle to combine with StealthChop2.

CoolStep – Load Adaptive Current Control

CoolStep drives the motor at the optimum current. It uses the StallGuard2 or StallGuard4 load measurement information to adjust the motor current to the minimum amount required in the actual load situation. This saves energy and keeps the components cool. Due to driving the motor with the optimum current, CoolStep increases the motor efficiency compared to standard operation with ca. 50% torque reserve.

Benefits

● Highest energy efficiency, power consumption decreased by up to 75%

- Motor generates less heat
- Improved mechanical precision
- Less or no cooling
- Improved reliability
- Use of smaller motor is possible, less torque reserve required
- Less motor noise due to less energy exciting motor resonances

Encoder Interface

The TMC2240 provides an encoder interface for external incremental encoders. The encoder can be used for consistency checks on-the-fly between encoder position and external ramp generator position. A programmable prescaler allows the adaptation of the encoder resolution to the motor resolution. A 32-bit encoder counter is provided.

SPI Interface

SPI Datagram Structure

The TMC2240 uses 40-bit SPI datagrams for communication with a microcontroller. Microcontrollers which are equipped with hardware SPI are typically able to communicate using integer multiples of 8 bits. The CSN line of the device must stay active (= low) for the complete duration of the datagram transmission.

Each datagram sent to the device is composed of an address byte followed by four data bytes. This allows direct 32-bit data word communication with the register set. Each register is accessed via 32 data bits even if it uses less than 32 data bits.

For simplification, each register is specified by a one byte address:

- For a read access, the most significant bit of the address byte is 0.
- For a write access, the most significant bit of the address byte is 1.

All registers are readable, most of them are read write, some read only and some write 1 to clear (e.g., GSTAT registers).

Table 1. SPI Datagram Structure

Selection of Write/Read (WRITE_notREAD)

The read and write selection is controlled by the MSB of the address byte (bit 39 of the SPI datagram). This bit is 0 for read access and 1 for write access. So, the bit named W is a WRITE_notREAD control bit. The active high write bit is the MSB of the address byte. So, 0x80 has to be added to the address for a write access. The SPI interface always delivers data back to the master, independent of the W bit. The data transferred back is the data read from the address which was transmitted with the *previous* datagram, if the previous access was a read access. If the previous access was a write access, then the data read back mirrors the previously received write data. So, the difference between a read and a write access is that the read access does not transfer data to the addressed register but it transfers the address only and its 32 data bits are dummies, and, further the following read or write access delivers back the data read from the address transmitted in the preceding read cycle.

A read access request datagram uses dummy write data. Read data is transferred back to the master with the

subsequent read or write access. Hence, reading multiple registers can be done in a pipelined fashion.

Whenever data is read from or written to the TMC2240, the MSBs delivered back contain the SPI status. The *SPI_STATUS* is a number of eight selected status bits.

Example:

For a read access to the register (*XACTUAL*) with the address 0x21, the address byte has to be set to 0x21 in the access preceding the read access. For a write access to the register (*VACTUAL*), the address byte has to be set to 0x80 + 0x22 = 0xA2. For read access, the data bit might have any value (-). So, one can set them to 0.

Table 2. SPI Read/Write Example Flow

* SS: is a placeholder for the status bits *SPI_STATUS*

SPI Status Bits Transferred with Each Datagram Read Back

New status information becomes latched at the end of each access and is available with the next SPI transfer.

Table 3. SPI_STATUS – Status Flags Transmitted With Each SPI Access In Bits 39 To 32

Data Alignment

All data are right aligned. Some registers represent unsigned (positive) values, some represent integer values (signed) as two's complement numbers, single bits or groups of bits are represented as single bits respectively as integer groups.

SPI Signals

The SPI bus on the TMC2240 has four signals:

- \bullet SCK bus clock input
- \bullet SDI serial data input
- \bullet SDO serial data output
- \bullet CSN chip select input (active low)

The slave is enabled for an SPI transaction by a low on the chip select input CSN. Bit transfer is synchronous to the bus clock SCK, with the slave latching the data from SDI on the rising edge of SCK and driving data to SDO following the falling edge. The most significant bit is sent first. A minimum of 40 SCK clock cycles is required for a bus transaction with the TMC2240.

If more than 40 clocks are driven, the additional bits shifted into SDI are shifted out on SDO after a 40-clock delay through an internal shift register. This can be used for daisy chaining multiple chips.

The CSN must be low during the whole bus transaction. When CSN goes high, the contents of the internal shift register are latched into the internal control register and recognized as a command from the master to the slave. If more than 40 bits are sent, only the last 40 bits received before the rising edge of CSN are recognized as the command.

SPI Timing

The SPI max frequency is at 10MHz. SCK is independent from the clock frequency of the system while the only parameter depending on the clock frequency is the minimum CSN high time. All SPI inputs are internally filtered to avoid triggering on pulses shorter than 10ns. The figure shows the timing parameters of an SPI bus transaction. Timing values are given in the EC table.

The SPI interfaces use SPI MODE 3.

Figure 4. SPI Timing Diagram

UART Single Wire Interface

The UART single wire interface allows control of the TMC2240 with any microcontroller UART. It shares transmit and receive line like an RS485-based interface. Data transmission is secured using a cyclic redundancy check, so that increased interface distances (e.g., over cables between two PCBs) can be bridged without danger of wrong or missed commands even in the event of electromagnetic disturbance. The automatic baud rate detection makes this interface easy to use.

Datagram Structure

Write Access

Table 4. UART Write Access Datagram Structure

A sync nibble precedes each transmission to and from the TMC2240 and is embedded into the first transmitted byte, followed by an addressing byte. Each transmission allows a synchronization of the internal baud rate divider to the master clock. The actual baud rate is adapted and variations of the internal clock frequency are compensated. Thus, the baud rate can be freely chosen within the valid range. Each transmitted byte starts with a start bit (logic 0, low level on DIAG1/ SW) and ends with a stop bit (logic 1, high level on DIAG1/SW). The bit time is calculated by measuring the time from the beginning of start bit (1 to 0 transition) to the end of the sync frame (1 to 0 transition from bit 2 to bit 3). All data is transmitted byte wise. The 32 bit data words are transmitted with the highest byte first.

A minimum baud rate of 9000 baud is permissible, assuming 20MHz clock (worst case for low baud rate). Maximum baud

rate is $f_{CLK}/16$ due to the required stability of the baud clock.

The initial slave address *SLAVEADDR* is selected by CSN_AD2, SCK_AD1, SDI_AD0 in the range 0 to 7.

The slave address is determined by the sum of the register *SLAVEADDR* and the pin selection given above. This means, that a high level on SDI (with CSN low and SCK low) increments the *SLAVEADDR* setting by one.

Bit 7 of the register address identifies a Read (0) or a Write (1) access. Example: Address 0x10 is changed to 0x90 for a write access.

The communication becomes reset if a pause time of longer than 63 bit times between the start bits of two successive bytes occurs. This timing is based on the last correctly received datagram. In this case, the transmission needs to be restarted after a failure recovery time of minimum 12 bit times of bus idle time. This scheme allows the master to reset communication in case of transmission errors. Any pulse on an idle data line below 16 clock cycles will be treated as a glitch and leads to a timeout of 12 bit times, for which the data line must be idle. Other errors like wrong CRC are also treated the same way. This allows a safe resynchronization of the transmission after any error conditions. Remark, that due to this mechanism an abrupt reduction of the baud rate to less than 15% of the previous value is not possible.

Each accepted write datagram becomes acknowledged by the receiver by incrementing an internal cyclic datagram counter (8 bit). Reading out the datagram counter allows the master to check the success of an initialization sequence or single write accesses. Read accesses do not modify the counter.

Read Access Table 5. UART Read Access Request Datagram Structure

The read access request datagram structure is identical to the write access datagram structure, but uses a lower number of user bits. Its function is the addressing of the slave and the transmission of the desired register address for the read access. The TMC2240 responds with the same baud rate as the master uses for the read request.

In order to ensure a clean bus transition from the master to the slave, the TMC2240 does not immediately send the reply to a read access, but it uses a programmable delay time after which the first reply byte becomes sent following a read request. This delay time can be set in multiples of eight bit times using *SENDDELAY* time setting (default = 8 bit times) according to the needs of the master. In a multi-slave system, set *SENDDELAY* to min. 2 for all slaves. Otherwise a non-addressed slave might detect a transmission error upon read access to a different slave.

Table 6. UART Read Access Reply Datagram Structure

The read response is sent to the master using address code %1111. The transmitter becomes switched inactive four bit times after the last bit is sent.

Address %11111111 is reserved for read accesses going to the master. A slave cannot use this address.

CRC Calculation

An 8-bit CRC polynomial is used for checking both read and write access. It allows detection of up to eight single bit errors. The CRC8-ATM polynomial with an initial value of zero is applied LSB to MSB, including the sync- and addressing byte. The sync nibble is assumed to always be correct. The TMC2240 responds only to correctly transmitted datagrams

containing its own slave address. It increases its datagram counter for each correctly received write access datagram. $CRC = x^8 + x^2 + x^1 + x^0$

Serial calculation example

CRC = (CRC << 1) OR (CRC.7 XOR CRC.1 XOR CRC.0 XOR [new incoming bit])

C-Code Example for CRC calculation

```
void swuart_calcCRC(UCHAR* datagram, UCHAR datagramLength) 
\{ int i,j; 
  UCHAR* crc = datagram + (datagramLength-1); // CRC located in last byte of message 
  UCHAR currentByte; 
 *crc = 0;
 for (i = 0; i<(datagramLength-1); i++) { // Execute for all bytes of a message currentByte = datagram[i]; \frac{1}{2} // Retrieve a byte to be sent from Array
                                              \frac{1}{2} Retrieve a byte to be sent from Array
   for (j = 0; j < 8; j++) {
     if ((*crc >> 7) ^ (currentByte&0x01)) // update CRC based result of XOR operation 
     { 
      *crc = (*csc << 1) ^ 0x07;
     } 
     else 
     { 
      *crc = (*csc < 1); } 
     currentByte = currentByte >> 1; 
   } // for CRC bit 
  } // for message byte 
}
```
UART Signals

The UART interface on the TMC2240 comprises five signals. In UART mode, the slave checks the single wire pin DIAG1/ SW for correctly received datagrams with its own address continuously. The pin is switched as input during this time. It adapts to the baud rate based on the sync nibble, as described earlier. In case of a read access, it switches on its output driver on DIAG1/SW and sends its response using the same baud rate.

Table 7. TMC2240 UART Interface Signals

Addressing Multiple Slaves

If only one or up to eight TMC2240 are addressed by a master using a single UART bus interface, a simple hardware address selection can be used. The individual UART addresses are set by connecting the UART address pins (SDI, SCK, CSN) to V_{CC} IO and GND.

If more than eight slaves need to be connected to the same UART bus, then a different approach must be used. This

approach can address up to 255 devices by using the output NAO (SDO) as a selection pin for the bit 0 address pin of the next device. Proceed as follows:

- Tie all address pins as well as SDI/AD0 of your first TMC2240 to GND.
- Connect SDO/NAO output of the first TMC2240 to the next drivers address[0] pin (SDI/AD0). Connect further drivers in the same fashion.
- Now, the first driver responds to address 0. Following drivers are set to address 1.
- Program the first driver to its dedicated slave address. **Note**: Once a driver is initialized with its slave address, its SDO/NAO output which is tied to the next drivers address[0] pin (SDI/AD0) has to be programmed to logic 0 in order to differentiate the next driver from all following devices.
- Now, the second driver is accessible and can get its slave address. Further units can be programmed to their slave addresses sequentially.

Figure 5. UART Daisy Chaining Example

Table 8. UART Example for Addressing up to 255 Slaves

Step/Direction Interface

The STEP and DIR inputs provide a simple, standard interface compatible with many existing motion controllers. The MicroPlyer step pulse interpolator brings the smooth motor operation of high-resolution microstepping to applications originally designed for coarser stepping.

Timing

The figure below shows the timing parameters for the STEP and DIR signals. When the *dedge* mode bit in the *CHOPCONF* register is set, both edges of STEP are active. If *dedge* is cleared, only rising edges are active. STEP and DIR are sampled and synchronized to the system clock. An internal analog filter of ca. 10ns removes glitches on the

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signals, such as those caused by long PCB traces. If the signal source is far from the chip, and especially if the signals are carried on cables, the signals should be filtered or transmitted differentially.

See the *Electrical Characteristics* table for the specified timing parameters.

Figure 6. STEP/DIR Signal Timing

Figure 7. STEP/DIR Signal Input Filter Structure

Changing Resolution

A reduced microstep resolution allows limitation of the step frequency for the STEP/DIR interface, or compatibility to an older, less performing driver. The internal microstep table with 1024 sine wave entries generates sinusoidal motor coil currents. These 1024 entries correspond to one electrical revolution or four fullsteps. The microstep resolution setting determines the step width taken within the table. Depending on the DIR input, the microstep counter is increased (DIR = 0) or decreased (DIR = 1) with each STEP pulse by the step width. The microstep resolution determines the increment respectively the decrement. At maximum resolution, the sequencer advances one step for each step pulse. At half resolution, it advances two steps. Increment is up to 256 steps for fullstepping. The sequencer has special provision to allow seamless switching between different microstep rates at any time. When switching to a lower microstep resolution, it calculates the nearest step within the target resolution and reads the current vector at that position. This behavior especially is important for low resolutions like fullstep and halfstep, because any failure in the step sequence would lead to asymmetrical run when comparing a motor running clockwise and counterclockwise.

Examples:

Fullstep: Cycles through table positions: 128, 384, 640, and 896 (45°, 135°, 225°, and 315° electrical position, both coils on at identical current). The coil current in each position corresponds to the RMS-Value (0.71 x amplitude). Step size is 256 (90° electrical)

Half step: The first table position is 64 (22.5° electrical), Step size is 128 (45° steps)

Quarter step: The first table position is 32 (90°/8 = 11.25° electrical), Step size is 64 (22.5° steps)

This way equidistant steps result and they are identical in both rotation directions. Some older drivers also use zero current (table entry 0, 0°) as well as full current (90°) within the step tables. This kind of stepping is avoided because it provides less torque and has a worse power dissipation in driver and motor.

Table 9. Fullstep/Half Step Lookup Table Values for Phase A/B Coil Currents

MicroPlyer Step Interpolator and Standstill Detection

For each active edge on STEP, MicroPlyer produces microsteps at 256x resolution. It interpolates the time in between the two step impulses at the step input based on the last step interval. This way, from 2 microsteps (128 microsteps to 256 microsteps interpolation) up to 256 microsteps (fullstep input to 256 microsteps) are driven for a single-step pulse.

MicroPlyer function is enabled by setting the *intpol* bit in the *CHOPCONF* register.

The step rate for the interpolated 2 microsteps to 256 microsteps is determined by measuring the time interval of the previous step period and dividing it into up to 256 equal parts. The maximum time between 2 microsteps corresponds to 2²⁰ (roughly one million system clock cycles), for an even distribution of 256 microsteps. At 16MHz system clock frequency, this results in a minimum step input frequency of 16Hz for MicroPlyer operation. A lower step rate causes the *STST* bit to be set, which indicates a standstill event. At that frequency, microsteps occur at a rate of (system clock frequency)/ 2^{16} ~ 256Hz. When a standstill is detected, the driver automatically switches the motor to holding current *IHOLD*.

Attention: MicroPlyer only works perfectly with a stable STEP frequency. Do not use the *dedge* option if the STEP signal does not have a 50% duty cycle!

Figure 8. MicroPlyer Microstep Interpolation with Rising STEP Frequency (Example: 16 to 256)

In the figure, the first STEP cycle is long enough to set the standstill bit *stst*. This bit is cleared on the next STEP active edge. Then, the external STEP frequency increases. After one cycle at the higher rate MicroPlyer adapts the interpolated microstep rate to the higher frequency. During the last cycle at the slower rate, MicroPlyer did not generate all 16 microsteps, so there is a small jump in motor angle between the first and second cycles at the higher rate.

StealthChop2

StealthChop2 is an extremely quiet mode of operation for stepper motors. It is based on a voltage mode PWM. In case of standstill and at low velocities, the motor is absolutely noiseless. Thus, StealthChop2-operated stepper motor applications are very suitable for indoor or home use. The motor operates absolutely free of vibration at low velocities. With StealthChop, the motor current is applied by driving a certain effective voltage into the coil, using a voltage mode PWM. With the enhanced StealthChop2, the driver automatically adapts to the application for best performance. No more configurations are required. Optional configuration allows for tuning the setting in special cases, or for setting initial values for the automatic adaptation algorithm. For high velocity drives, SpreadCycle should be considered in combination with StealthChop2.

Figure 9. Motor Coil Sine Wave Current with StealthChop (Measured with Current Probe)

Automatic Tuning

StealthChop2 integrates an automatic tuning (AT) procedure, which adapts the most important operating parameters to the motor automatically. This way, StealthChop2 allows high motor dynamics and supports powering down the motor to very low currents. Just two steps have to be taken into account for best results: Start with the motor in standstill, but powered with nominal run current (AT#1). Move the motor at a medium velocity, e.g., as part of a homing procedure (AT#2). The flowchart in the next figure shows the tuning procedure.

Table 10. Constraints and Requirements for StealthChop2 Autotuning AT#1 and AT#2

Hint:

Determine best conditions for automatic tuning with the evaluation board.

Use application-specific parameters for *PWM_GRAD* and *PWM_OFS* for initialization in firmware to provide initial tuning parameters.

Monitor *PWM_SCALE_AUTO* going down to zero during the constant velocity phase in AT#2 tuning. This indicates a successful tuning.

Attention:

Operating in StealthChop2 without proper tuning can lead to high motor currents during a deceleration ramp, especially with low resistive motors and fast deceleration settings. Follow the automatic tuning process and check optimum tuning conditions using the evaluation board. It is recommended to use an initial value for settings *PWM_OFS* and *PWM_GRAD* determined per motor type.

Modifying *GLOBALSCALER* or V_S voltage invalidates the result of the automatic tuning process. Motor current regulation cannot compensate significant changes until next AT#1 phase. Automatic tuning adapts to changed conditions whenever AT#1 and AT#2 conditions are fulfilled in the later operation.

Figure 10. StealthChop2 Automatic Tuning Procedure

StealthChop2 Options

In order to match the motor current to a certain level, the effective PWM voltage becomes scaled depending on the actual motor velocity. Several additional factors influence the required voltage level to drive the motor at the target current: The motor resistance, its back EMF (e.g., directly proportional to its velocity) as well as the actual level of the supply voltage. Two modes of PWM regulation are provided: The automatic tuning mode (AT) using current feedback (*pwm_autoscale* = 1, *pwm_autograd* = 1) and a feed forward velocity-controlled mode (*pwm_autoscale* = 0). The feed forward velocitycontrolled mode does not react to a change of the supply voltage or to events like a motor stall, but it provides very stable amplitude. It does not use nor require any means of current measurement. This is perfect when motor type and supply voltage are well known. Therefore, we recommend the automatic mode, unless current regulation is not satisfying in the given operating conditions.

It is recommended to use application-specific initial tuning parameters, fitting the motor type and supply voltage. Additionally, operate in automatic tuning mode in order to respond to parameter change, e.g., due to motor heat-up or change of supply voltage.

Non-automatic mode (*pwm_autoscale = 0*) should be taken into account only with well-known motor and operating conditions. In this case, careful programming via the interface is required. The operating parameters *PWM_GRAD* and *PWM_OFS* can be determined in automatic tuning mode initially.

The StealthChop2 PWM frequency can be chosen in four steps in order to adapt the frequency divider to the frequency of the clock source. A setting in the range of 20kHz–50kHz is good for most applications. It balances low current ripple and good higher velocity performance vs. dynamic power dissipation.

Table 11. Choice of PWM Frequency for StealthChop2 (Bold Font = Recommended)

StealthChop2 Current Regulator

In StealthChop2 voltage PWM mode, the autoscaling function (*pwm_autoscale* = 1, *pwm_auto_grad* = 1) regulates the motor current to the desired current setting. Automatic scaling is used as part of the AT process, and for subsequent tracking of changes within the motor parameters. The driver measures the motor current during the chopper on time and uses a proportional regulator to regulate *PWM_SCALE_AUTO* in order match the motor current to the target current. *PWM_REG* is the proportionality coefficient for this regulator. Basically, the proportionality coefficient should be as small as possible in order to get a stable and soft regulation behavior, but it must be large enough to allow the driver to quickly react to changes caused by variation of the motor target current (e.g., change of V_{RFF}). During initial tuning step AT#2, *PWM_REG* also compensates for the change of motor velocity. Therefore, a high acceleration during AT#2 requires a higher setting of *PWM_REG*. With careful selection of homing velocity and acceleration, a minimum setting of the regulation gradient often is sufficient (*PWM_REG* = 1). *PWM_REG* setting should be optimized for the fastest required acceleration and deceleration ramp (compare the following two figures).

Figure 11. StealthChop2: Good Setting for PWM_REG

Figure 12. StealthChop2: Too Small Setting for PWM_REG during AT#2

The quality of the setting *PWM_REG* in phase AT#2 and the finished automatic tuning procedure (or non-automatic settings for *PWM_OFS* and *PWM_GRAD*) can be examined when monitoring motor current during an acceleration phase as shown in the next figure.

Figure 13. Successfully Determined PWM_GRAD(_AUTO) and PWM_OFS(_AUTO)

Lower Current Limit

Depending on the setting of *pwm_meas_sd_enable,* the StealthChop2 current regulator principle imposes a lower limit for motor current regulation. As the coil current is measured during chopper on phase only (*pwm_meas_sd_enable* = 0), a minimum chopper duty cycle allowing coil current regulation is given by the blank time as set by *TBL* and by the chopper frequency setting. Therefore, the motor-specific minimum coil current in StealthChop2 autoscaling mode rises with the supply voltage and with the chopper frequency. A lower blanking time allows a lower current limit. It is important for the correct determination of *PWM_OFS_AUTO*, that in AT#1 the run current, *GLOBALSCALER,* and *IRUN* is well within the regulation range. Lower currents (e.g., for standstill power down) are automatically realized based on *PWM_OFS_AUTO* and *PWM_GRAD_AUTO* respectively based on *PWM_OFS* and *PWM_GRAD* with non-automatic current scaling. The freewheeling option allows going to zero motor current.

Lower motor coil current limit for StealthChop2 automatic tuning (*pwm_meas_sd_enable = 0)* :

$$
I_{\text{LowerLimit}} = t_{\text{BLANK}} \times f_{\text{PWM}} \times \frac{V_M}{R_{\text{COLL}}}
$$

With V_M the motor supply voltage and R_{COII} the motor coil resistance.

ILowerLimit can be treated as a thumb value for the minimum nominal *IRUN* motor current setting. In case the lower current limit is not sufficient to reach the desired setting, the driver retries with a lower chopper frequency in step AT#1, only.

f_{PWM} is the chopper frequency as determined by setting *PWM_FREQ*. In AT#1, the driver tries a lower, (roughly half frequency), in case it cannot reach the current. The frequency remains active in standstill, while currentscale *CS* = *IRUN.* With automatic standstill reduction, this is a short moment.

Example: A motor has a coil resistance of 5Ω, the supply voltage is 24V. With *TBL* = %01 and *PWM_FREQ* = %00, $t_{\text{BI ANK}}$ is 24 clock cycles, f_{PWM} is 2/(1024 clock cycles):

$$
I_{\text{LowerLimit}} = 24t_{\text{CLK}} \times \frac{2}{1024t_{\text{CLK}}} \times \frac{24V}{5\Omega} = \frac{24}{512} \times \frac{24V}{5\Omega} = 225 \text{mA}
$$

This means the motor target current for automatic tuning must be 225mA or more, taking into account all relevant settings. This lower current limit also applies for modification of the motor current via the *GLOBALSCALER*.

Attention:

For automatic tuning, a lower coil current limit applies.

IRUN ≥ 8: Current settings for *IRUN* below 8 do not work with automatic tuning.

ILOWERLIMIT: Depending on the setting of bit *pwm_meas_sd_enable (in register PWM_CONF[22])* for automatic tuning, a lower coil current limit applies.The motor current in automatic tuning phase AT#1 must exceed this lower limit. Calculate ILOWERLIMIT or measure it using a current probe. Setting the motor run-current or hold-current below the lower current limit during operation by modifying *IRUN* and *IHOLD* is possible after successful automatic tuning. The lower current limit also limits the capability of the driver to respond to changes of *GLOBALSCALER*.

The lower current limit also limits the capability of the driver to respond to changes of *GLOBALSCALER*.

To overcome the lower limit set *pwm_meas_sd_enable* = 1. This will allow the IC to additionally measure coil current in the slow decay phase.

Velocity-Based Scaling

Velocity-based scaling scales the StealthChop2 amplitude based on the time between every two steps, e.g., based on *TSTEP*, measured in clock cycles. This concept basically does not require a current measurement, because no regulation loop is necessary. A pure velocity-based scaling is available via programming, only, when setting *pwm_autoscale* = 0. The basic idea is to have a linear approximation of the voltage required to drive the target current into the motor. The stepper motor has a certain coil resistance and thus needs a certain voltage amplitude to yield a target current based on the basic formula I = U/R. With R being the coil resistance, U the supply voltage scaled by the PWM value, the current I results. The initial value for *PWM_OFS* can be calculated:

$$
PWM_OFS = \frac{374 \times R_{COL} \times I_{COL}}{V_M}
$$

With V_M the motor supply voltage and I_{COLL} the target RMS current

The effective PWM voltage U_{PWM} (1/SQRT(2) x peak value) results considering the 8-bit resolution and 248 sine wave peak for the actual PWM amplitude shown as *PWM_SCALE*:

$$
UPWM = V_M \times \frac{PWM_SCALE}{256} \times \frac{248}{256} \times \frac{1}{\sqrt{2}} = V_M \times \frac{PWM_SCALE}{374}
$$

With rising motor velocity, the motor generates an increasing back EMF voltage. The back EMF voltage is proportional to the motor velocity. It reduces the PWM voltage effective at the coil resistance and thus current decreases. The TMC2240 provides a second velocity dependent factor (*PWM_GRAD*) to compensate for this. The overall effective PWM amplitude (*PWM_SCALE_SUM*) in this mode automatically is calculated in dependence of the microstep frequency as:

$$
PWM_SCALE_SUM = PWM_OFS + PWM_GRAD \times 256 \times \frac{f_{STEP}}{f_{CLK}}
$$

With f_{STEP} being the microstep frequency for 256 microstep resolution equivalent and $f_{\text{CI K}}$ the clock frequency supplied to the driver or the actual internal frequency.

As a first approximation, the back EMF subtracts from the supply voltage and thus the effective current amplitude decreases. This way, a first approximation for *PWM_GRAD* setting can be calculated:

$$
PWM_GRAD = C_{BEMF} \left[\frac{\frac{V}{rad}}{s} \right] \times 2\pi \times \frac{f_{clk} \times 1.46}{V_M \times MSPR}
$$

C_{BFMF} is the back EMF constant of the motor in Volts per radian/second.

MSPR is the number of microsteps per rotation related to 1/256 microstep resolution, e.g., 51200 = 256 microsteps multiplied by 200 fullsteps for a 1.8° motor.

Figure 14. Velocity-Based PWM Scaling (pwm_autoscale = 0)

The values for *PWM_OFS* and *PWM_GRAD* can easily be optimized by tracing the motor current with a current probe on the oscilloscope. Alternatively, automatic tuning determines these values and they can be read out from *PWM_OFS_AUTO* and *PWM_GRAD_AUTO*.

Understanding the back EMF constant of a motor: The back EMF constant is the voltage a motor generates when turned with a certain velocity. Often motor datasheets do not specify this value, as it can be deducted from motor torque and coil current rating. Within SI units, the numeric value of the back EMF constant CBEMF has the same numeric value as the numeric value of the torque constant. For example, a motor with a torque constant of 1 Nm/A would have a C_{BFMF} of 1V/rad/s. Turning such a motor with 1rps (1rps = 1 revolution per second = 6.28 rad/s) generates a back EMF voltage of 6.28V. Thus, the back EMF constant can be calculated as:

$$
C_{\text{BEMF}}\left|\frac{V}{\frac{\text{rad}}{\text{s}}}\right| = \frac{\text{HoldingTorque[Nm]}}{2 \times I_{\text{COLNOM}}[A]}
$$

I_{COILNOM} is the motor's rated phase current for the specified holding torque.

HoldingTorque is the motor specific holding torque, e.g., the torque reached at $l_{\rm COII}$ NOM on both coils. The torque unit is [Nm] where 1Nm = 100Ncm = 1000mNm.

The voltage is valid as RMS voltage per coil, thus the nominal current is multiplied by 2 in this formula, since the nominal current assumes a fullstep position, with two coils operating.

Combining StealthChop2 and SpreadCycle

For applications requiring high velocity motion, SpreadCycle may bring more stable operation in the upper velocity range. To combine no-noise operation with highest dynamic performance, the TMC2240 allows combining StealthChop2 and SpreadCycle based on a velocity threshold. With this, StealthChop2 is only active at low velocities.

Figure 15. TPWMTHRS for Optional Switching to SpreadCycle

 As a first step, both chopper principles should be parameterized and optimized individually. In a next step, a transfer velocity has to be fixed. For example, StealthChop2 operation is used for precise low speed positioning, while SpreadCycle shall be used for highly dynamic motion. *TPWMTHRS* determines the transition velocity. Read out *TSTEP* when moving at the desired velocity and program the resulting value to *TPWMTHRS*. Use a low transfer velocity to avoid a jerk at the switching point.

Jerkless switching to SpreadCycle: A jerk occurs when switching at higher velocities, because the back-EMF of the motor (which rises with the velocity) causes a phase shift of up to 90° between motor voltage and motor current. So when switching at higher velocities between voltage PWM and current PWM mode, this jerk will occur with increased intensity. A high jerk may even produce a temporary overcurrent condition (depending on the motor coil resistance). At low velocities (e.g., 1 to a few 10RPM), it can be completely neglected for most motors. Therefore, consider the jerk when switching the driver between SpreadCycle and StealthChop2. With automatic switching controlled by *TPWMTHRS*, the driver can automatically eliminate the jerk by using StallGuard4 to determine the phase shift. It will apply the same phase shift to SpreadCycle until the velocity falls back below the switching threshold. Set flag *SG4_THRS*.sg_angle_offset to enable this function.

Set *TPWMTHRS* zero if you want to work with StealthChop2 only.

When enabling the StealthChop2 mode the first time using automatic current regulation, the motor must be at standstill

in order to allow a proper current regulation. When the drive switches to StealthChop2 at a higher velocity, StealthChop2 logic stores the last current regulation setting until the motor returns to a lower velocity again. This way, the regulation has a known starting point when returning to a lower velocity, where StealthChop2 becomes re-enabled. Therefore, neither the velocity threshold nor the supply voltage must be considerably changed during the phase while the chopper is switched to a different mode because otherwise, the motor might lose steps or the instantaneous current might be too high or too low.

A motor stall or a sudden change in the motor velocity may lead to the driver detecting a short circuit or to a state of automatic current regulation, from which it cannot recover. Clear the error flags and restart the motor from zero velocity to recover from this situation.

Start the motor from standstill when switching on StealthChop2 the first time and keep it stopped for at least 128 chopper periods to allow StealthChop2 to do initial standstill current control.

Flags in StealthChop2

As StealthChop2 uses voltage mode driving, status flags based on current measurement respond slower, respectively the driver reacts delayed to sudden changes of back EMF, like on a motor stall.

A motor stall, or abrupt stop of the motion during operation in StealthChop2 can lead to an overcurrent condition. Depending on the previous motor velocity, and on the coil resistance of the motor, it significantly increases motor current for a time of several 10ms. With low velocities, where the back EMF is just a fraction of the supply voltage, there is no danger of triggering the short detection.

Tune the low side driver overcurrent detection to safely trigger upon motor stall, when using StealthChop2. This avoids high peak current draw from the power supply.

Open Load Flags

In StealthChop2 mode the status information is different compared to the cycle-by-cycle regulated SpreadCycle mode.

The flags OLA and OLB indicate that the current regulation is reaching the nominal current on both coils.

- A flickering OLA or OLB can result from too big differences in the motor coils.
- An interrupted motor coil leads to a continuously active open load flag for the coil.
- One or both flags are active, if the current regulation did not succeed in scaling up to the full target current within the last few fullsteps (because no motor is attached or a high velocity exceeds the PWM limit).

If desired, do an on-demand open load test using the SpreadCycle chopper as it delivers the safest result. With StealthChop2, *PWM_SCALE_SUM* can be checked to detect the correct coil resistance.

PWM_SCALE_SUM Informs about the Motor State

Information about the motor state is available with automatic scaling by reading out *PWM_SCALE_SUM*. As this parameter reflects the actual voltage required to drive the target current into the motor, it depends on several factors: motor load, coil resistance, supply voltage, and current setting. Therefore, an evaluation of the *PWM_SCALE_SUM* value allows checking the motor operation point. When reaching the limit (1023), the current regulator cannot sustain the full motor current, e.g., due to a drop in supply voltage.

Freewheeling and Passive Braking

StealthChop2 provides different options for motor standstill. These options can be enabled by setting the standstill current *IHOLD* to zero and choosing the desired option using the *FREEWHEEL* setting. The desired option becomes enabled after a time period specified by *TPOWERDOWN* and *IHOLDDELAY*. Current regulation becomes frozen once the motor target current is at zero current in order to ensure a quick startup. With the freewheeling options, both freewheeling and passive braking can be realized. Passive braking is an effective eddy current motor braking, which consumes a minimum of energy because no active current is driven into the coils. However, passive braking will allow slow turning of the motor when a continuous torque is applied.

Operate the motor within your application when exploring StealthChop2. Motor performance often is better with a mechanical load because it prevents the motor from stalling due to mechanical oscillations which can occur without load.

Parameters Controlling StealthChop2

The following table contains all parameters related to the StealthChop2 chopper mode.

Table 12. Parameters Controlling StealthChop2

Table 12. Parameters Controlling StealthChop2 (continued)

SpreadCycle and Classic Chopper

While StealthChop2 is a voltage mode PWM controlled chopper, SpreadCycle is a cycle-by-cycle current control. Therefore, it can react extremely fast to changes in motor velocity or motor load. The currents through both motor coils are controlled using choppers. The choppers work independently of each other. In the following figure, the different chopper phases are shown.

Figure 16. Typical Chopper Decay Phases

Although the current could be regulated using only on phases and fast decay phases, insertion of the slow decay phase is important to reduce electrical losses and current ripple in the motor. The duration of the slow decay phase is specified in a control parameter and sets an upper limit on the chopper frequency. The current comparator measures coil current during phases when the current flows through exactly one lowside transistor, but not during the slow decay phase. The slow decay phase is terminated by a timer. The on phase is terminated by the comparator when the current through the coil reaches the target current. The fast decay phase may be terminated by either the comparator or another timer.

When the coil current is switched, spikes in the $R_{DS(ON)}$ -based current measurement occur due to charging and discharging parasitic capacitance. During this time, typically one or two microseconds, the current cannot be measured. Blanking is the time when the input to the comparator is masked to block these spikes.

There are two cycle-by-cycle chopper modes available: a new high-performance chopper algorithm called SpreadCycle

and a proven constant off-time chopper mode. The constant off-time mode cycles through three phases: on, fast decay, and slow decay. The SpreadCycle mode cycles through four phases: on, slow decay, fast decay, and a second slow decay.

The chopper frequency is an important parameter for a chopped motor driver. A too low frequency might generate audible noise. A higher frequency reduces current ripple in the motor, but with a too high frequency magnetic losses may rise. Also power dissipation in the driver rises with increasing frequency due to the increased influence of switching slopes causing dynamic dissipation. Therefore, a compromise needs to be found. Most motors are optimally working in a frequency range of 16kHz to 30kHz. The chopper frequency is influenced by a number of parameter settings as well as by the motor inductivity and supply voltage.

Hint: A chopper frequency in the range of 25kHz to 40kHz gives a good result for most motors when using SpreadCycle. A higher frequency leads to increased switching losses.

Table 13. Parameters Controlling SpreadCycle and Classic Constant Off Time Chopper

SpreadCycle Chopper

The SpreadCycle (patented) chopper algorithm is a precise and simple to use chopper mode which automatically determines the optimum length for the fast-decay phase. The SpreadCycle will provide superior microstepping quality even with default settings. Several parameters are available to optimize the chopper to the application.

Each chopper cycle comprises an on phase, a slow decay phase, a fast decay phase and a second slow decay phase. The two slow decay phases and the two blank times per chopper cycle put an upper limit to the chopper frequency. The slow decay phases typically make up for about 30%–70% of the chopper cycle in standstill and are important for low motor and driver power dissipation.

Example calculation of a starting value for the slow decay time *TOFF*:

- Target Chopper frequency: 25kHz (Assumption: Two slow decay cycles make up for 50% of overall chopper cycle time.)
- t_{OFF} = 1 / 25kHz × 50 / 100 × 1 / 2 = 10 µ *s*
- For the *TOFF* setting this means: TOFF = $(t_{\text{OFF}} \times f_{\text{CLK}} 12)$ / 32
- With 12MHz clock this results in TOFF = 3.4, which would require a setting of TOFF = 3 or 4
- With 16MHz clock this results in TOFF = 4.6, which would require a setting of TOFF = 4 or 5

Hint: Highest motor velocities sometimes benefit from setting TOFF to 1 or 2 and a short TBL of 1 or 0.

The hysteresis start setting forces the driver to introduce a minimum amount of current ripple into the motor coils. The current ripple must be higher than the current ripple which is caused by resistive losses in the motor in order to give best

microstepping results. This will allow the chopper to precisely regulate the current for both rising and falling target current. The time required to introduce the current ripple into the motor coil also reduces the chopper frequency. Therefore, a higher hysteresis setting will lead to a lower chopper frequency. The motor inductance limits the ability of the chopper to follow a changing motor current. Further the duration of the on phase and the fast decay must be longer than the blanking time, because the current comparator is disabled during blanking.

It is easiest to find the best setting by starting from a low hysteresis setting (e.g., *HSTRT* = 0, *HEND* = 0) and increasing *HSTRT*, until the motor runs smoothly at low velocity settings. This can best be checked when measuring the motor current with a current probe. Checking the sine wave shape near the zero transition will show a small ledge between both half waves in case the hysteresis setting is too small. At medium velocities (e.g., 100 fullsteps to 400 fullsteps per second), a too low hysteresis setting will lead to increased humming and vibration of the motor. A too high hysteresis setting will lead to reduced chopper frequency and increased chopper noise but will not yield any benefit for the wave shape.

As experiments show, the setting is quite independent of the motor because higher current motors typically also have a lower coil resistance. Therefore choosing a low to medium default value for the hysteresis (for example, effective hysteresis = 4) normally fits most applications. The setting can be optimized by experimenting with the motor: A too low setting will result in reduced microstep accuracy, while a too high setting will lead to more chopper noise and motor power dissipation. When the fast decay time becomes slightly longer than the blanking time, the setting is optimum. You can reduce the off-time setting if this is hard to reach.

The hysteresis principle could in some cases lead to the chopper frequency becoming too low, e.g., when the coil resistance is high when compared to the supply voltage. This is avoided by splitting the hysteresis setting into a start setting (*HSTRT + HEND*) and an end setting (*HEND*). An automatic hysteresis decrementer (HDEC) interpolates between both settings, by decrementing the hysteresis value stepwise each 16 system clocks. At the beginning of each chopper cycle, the hysteresis begins with a value which is the sum of the start and the end values (*HSTRT* + *HEND*), and decrements during the cycle, until either the chopper cycle ends or the hysteresis end value (*HEND*) is reached. This way, the chopper frequency is stabilized at high amplitudes and low supply voltage situations, if the frequency gets too low. This avoids the frequency from reaching the audible range.

Figure 17. SpreadCycle Chopper Scheme Showing Coil Current during a Chopper Cycle

Table 14. SpreadCycle Mode Parameters

Table 14. SpreadCycle Mode Parameters (continued)

Even at HSTRT = 0 and HEND = 0, the TMC2240 sets a minimum hysteresis via analog circuitry.

Example:

A hysteresis of 4 has been chosen. You might decide to not use hysteresis decrement. In this case set:

In order to take advantage of the variable hysteresis, we can set most of the value to the HSTRT, e.g., 4, and the remaining 1 to hysteresis end. The resulting configuration register values are as follows:

Classic Constant Off-Time Chopper

The classic constant off-time chopper is an alternative to SpreadCycle. Perfectly tuned, it also gives good results. In combination with RDSon current sensing without external sense resistors, this chopper mode can bring a benefit with regard to audible high-pitch chopper noise.

The classic constant off-time chopper uses a fixed-time fast decay following each on phase. While the duration of the on phase is determined by the chopper comparator, the fast decay time needs to be long enough for the driver to follow the falling slope of the sine wave, but it should not be so long that it causes excess motor current ripple and power dissipation. This can be tuned using an oscilloscope or evaluating motor smoothness at different velocities. A good starting value is a fast decay time setting similar to the slow decay time setting.

Figure 18. Classic Constant Off-Time Chopper with Offset Showing Coil Current

After tuning the fast decay time, the offset should be tuned for a smooth zero crossing. This is necessary because the fast decay phase makes the absolute value of the motor current lower than the target current (see figures below). If the zero offset is too low, the motor stands still for a short moment during current zero crossing. If it is set too high, it makes a larger microstep. Typically, a positive offset setting is required for smoothest operation.

Figure 19. Zero Crossing with Classic Chopper and Correction Using Sine Wave Offset

Table 15. Parameters Controlling Constant Off-Time Chopper Mode

Integrated Current Sense

A non-dissipative Current Sensing is integrated. This feature eliminates the bulky external power resistors which are normally required for this function. The ICS results in a dramatic space and power saving compared with mainstream applications based on external sense resistor.

Setting the Motor Current

Table 16. Parameters Controlling the Motor Current

Table 16. Parameters Controlling the Motor Current (continued)

Setting the Full-Scale Current Range

The full-scale current is selected with an external reference resistor and 2 bits in the DRV_CONF register.

Three different full-scale current ranges can be configured to adapt to different motor sizes and applications.

This is needed to benefit from a best possible current control resolution.

Therefore, connect a resistor from I_{REF} to GND to set the full-scale chopping current I_{FS} .

Bits 1..0 in DRV_CONF register define the typical ON resistance of the driver stage and further control the full-scale range based on the external resistor.

The equation below shows the full-scale current as a function of the R_{REF} shunt resistor connected to pin I_{REF} and the DRV CONF register bit setting.

The proportionality constant K_{IFS} depends on the selected full-scale range setting (DRV_CONF register bits 1..0). The external resistor R_{REF} can range between 12kΩ and 60kΩ.

 I_{FS} = $K_{IFS}(KV)$ / $R_{REF}(k\Omega)$

Table 17. IFS Full-Scale Range Settings (Example for RREF = 12kΩ)

Velocity-Based Mode Control

The TMC2240 allows the configuration of different chopper modes and modes of operation for optimum motor control. Depending on the motor load, the different modes can be optimized for lowest noise & high precision, highest dynamics,

or maximum torque at highest velocity. Some of the features like CoolStep or StallGuard2 are useful in a limited velocity range. A number of velocity thresholds allow combining the different modes of operation within an application requiring a wide velocity range.

Figure 20. Choice of Velocity-Dependent Modes

The figure shows all available thresholds and the required ordering. VPWMTHRS, VHIGH, and VCOOLTHRS are determined by the settings *TPWMTHRS*, *THIGH,* and *TCOOLTHRS.* The velocity is described by the time interval *TSTEP* between each two step pulses. This allows determination of the velocity when an external step source is used. *TSTEP* always becomes normalized to 256 microsteps. This way, the thresholds do not have to be adapted when the microstep resolution is changed. The thresholds represent the same motor velocity, independent of the microstep settings. *TSTEP* becomes compared to these threshold values. A hysteresis of 1/16 *TSTEP* resp. 1/32 *TSTEP* is applied to avoid continuous toggling of the comparison results when a jitter in the *TSTEP* measurement occurs. The upper switching velocity is higher by 1/16, resp. 1/32 of the value set as threshold. The motor current can be programmed to a run and a hold level, dependent on the standstill flag *stst*.

Using automatic velocity thresholds allows tuning the application for different velocity ranges. Features like CoolStep will integrate completely transparently in your setup. This way, once parameterized, they do not require any activation or

deactivation via software.

Table 18. Velocity-Based Mode Control Parameters

StallGuard2 Load Measurement

To fit different motor control schemes, the TMC2240 offers two types of StallGuard2 sensorless load detection schemes, covering the two basic chopper modes. StallGuard2 works in SpreadCycle operation, while StallGuard4 is optimized for StealthChop2 operation.

StallGuard2 provides an accurate measurement of the load on the motor. It can be used for stall detection as well as other uses at loads below those which stall the motor, such as CoolStep load-adaptive current reduction. The StallGuard2 measurement value changes linearly over a wide range of load, velocity, and current settings. At maximum motor load,

the value goes to zero or near to zero. This corresponds to a load angle of 90° between the magnetic field of the coils and magnets in the rotor. This also is the most energy-efficient point of operation for the motor.

Hint: In order to use StallGuard2 and CoolStep, the StallGuard2 sensitivity should first be tuned using the SGT setting!

Figure 21. Function Principle of StallGuard2

Table 19. StallGuard2-Related Parameters

Table 19. StallGuard2-Related Parameters (continued)

StallGuard2 Update Rate and Filter

The StallGuard2 measurement value *SG_RESULT* is updated with each fullstep of the motor. This is enough to safely detect a stall because a stall always means the loss of four fullsteps. In a practical application, especially when using CoolStep, a more precise measurement might be more important than an update for each fullstep because the mechanical load never changes instantaneously from one step to the next. For these applications, the *sfilt* bit enables a filtering function over four load measurements. The filter should always be enabled when high-precision measurement is required. It compensates for variations in motor construction, for example due to misalignment of the phase A to phase B magnets. The filter should be disabled when rapid response to increasing load is required and for best results of sensorless homing using StallGuard.

Detecting a Motor Stall

For best stall detection, work without StallGuard2 filtering (*sfilt* = 0). To safely detect a motor stall the stall threshold must be determined using a specific *SGT* setting. Therefore, the maximum load needs to be determined, which the motor can drive without stalling. At the same time, monitor the *SG_RESULT* value at this load, e.g., some value within the range 0 to 100. The stall threshold should be a value safely within the operating limits, to allow for parameter stray. The response at an *SGT* setting at or near 0 gives some idea on the quality of the signal: Check the *SG_RESULT* value without load and with maximum load. They should show a difference of at least 100 or a few 100, which shall be largely compared to the offset. If you set the *SGT* value in a way, that a reading of 0 occurs at maximum motor load, the stall can be automatically detected to issue a motor stop. In the moment of the step resulting in a step loss, the lowest reading will be visible. After the step loss, the motor will vibrate and show a higher *SG_RESULT* reading.

Homing with StallGuard2

The homing of a linear drive requires moving the motor into the direction of a hard stop. As StallGuard2 needs a certain velocity to work (as set by TCOOLTHRS), make sure that the start point is far enough away from the hard stop to provide the distance required for the acceleration phase. After setting up SGT, start a motion into the direction of the hard stop and configure *diag0_stall* or *diag1_stall* to indicate the stall condition to the external controller using one of the diagnostic outputs. Once a stall is detected, the controller stops the motor. The stop condition also is indicated by the flag STALLGUARD in DRV_STATUS.

Limits of StallGuard2 Operation

StallGuard2 does not operate reliably at extreme motor velocities: Very low motor velocities (for many motors, less than 1Rps) generate a low back EMF and make the measurement unstable and dependent on environment conditions (temperature, etc.). The automatic tuning procedure described above will compensate for this. Other conditions will also lead to extreme settings of *SGT* and poor response of the measurement value *SG_RESULT* to the motor load.

Very high motor velocities, in which the full sinusoidal current is not driven into the motor coils also leads to poor response. These velocities are typically characterized by the motor back EMF reaching the supply voltage.

StallGuard4 Load Measurement

StallGuard4 is developed for operation in conjunction with StealthChop2. It provides an accurate measurement of the load on the motor and can be used for stall detection, load estimation as well as CoolStep load-adaptive current reduction. The StallGuard4 measurement value changes linearly over a wide range of load, velocity, and current settings, as shown in the next figure. When approaching maximum motor load, the value goes down to a motor-specific lower value. This corresponds to a load angle of 90° between the magnetic field of the coils and magnets in the rotor. This also is the most energy-efficient point of operation for the motor.

In order to use StallGuard4, check the sensitivity of the motor at border conditions.

Figure 22. StallGuard4 Mode of Operation

Table 20. StallGuard4-Related Parameters

Table 20. StallGuard4-Related Parameters (continued)

StallGuard4 vs. StallGuard2

StallGuard4 is optimized for operation with StealthChop2, and its predecessor StallGuard2 works with

SpreadCycle. The function is similar: Both deliver a load value, going from a high value at low load, to a low value at high load. While StallGuard2 becomes tuned to show a "0"-reading for stall detection, StallGuard4 uses a comparison-value to trigger stall detection, rather than shifting the measurement result by applying an offset.

Tuning StallGuard4

The StallGuard4 value *SG4_RESULT* is affected by motor-specific characteristics and application-specific demands on load, coil current, and velocity. Therefore, the easiest way to tune the StallGuard4 threshold *SG4_THRS* for a specific motor type and operating conditions is interactive tuning in the actual application.

The initial procedure for tuning StallGuard *SG4_THRS* is as follows:

- 1. Operate the motor at the normal operation velocity for your application and monitor *SG4_RESULT*.
- 2. Apply slowly increasing mechanical load to the motor. Check the lowest value of *SG4_RESULT* before the motor stalls. Use this value as starting value for *SG4_THRS* (apply half of the value).
- 3. Now, monitor the StallGuard output signal via DIAG output (configure properly, also set *TCOOLTHRS* to match the lower velocity limit for operation) and stop the motor when a pulse is seen on the respective output. Make sure, that the motor is safely stopped whenever it is stalled. Increase *SG4_THRS* if the motor becomes stopped before a stall occurs.
- 4. The optimum setting is reached when a stall is safely detected and leads to a pulse at DIAG in the moment where the stall occurs. *SG4_THRS* in most cases can be tuned for a certain motion velocity or a velocity range. Make sure, that the setting works reliable in a certain range (e.g., 80% to 120% of desired velocity) and also under extreme motor conditions (lowest and highest applicable temperature).

DIAG is pulsed by StallGuard, when *SG4_RESULT* falls below *SG4_THRS*. It is only enabled in StealthChop2 mode, and when *TCOOLTHRS* ≥ *TSTEP* > *TPWMTHRS.*

The external motion controller should react to a single pulse by stopping the motor if desired. Set *TCOOLTHRS* to match the lower velocity threshold where StallGuard delivers a good result.

SG4_RESULT measurement has a high resolution, and there are a few ways to enhance its accuracy, as described in the following sections.

StallGuard4 Update Rate

The StallGuard4 measurement value *SG4_RESULT* is updated with each fullstep of the motor. This is enough to safely detect a stall because a stall always means the loss of four fullsteps.

StallGuard4 provides two options for measurement:

1. *sg4* filt en = 0: A single measurement, updated after each fullstep, and valid for each one fullstep. This measurement allows quickest reaction to load variations, as *SG4_RESULT* becomes fully updated with each zero transmission of a coil voltage. Therefore, it is optimum for stall detection with a hard obstacle.

2. *sg4_filt_en* = 1: In this mode, four individual signals become generated: *SG4_IND_0* upon falling 0-transition of the cosine wave (coil A); *SG4_IND_1* upon rising 0-transition of the co-sine wave; *SG4_IND_2* upon falling 0-transition of the sine wave (coil B); *SG4_IND_3* upon rising 0-transition of the sine wave. The actual value for *SG4_RESULT* is the

mean value of all four measurements, becoming updated once each fullstep. With this, each fullstep has an influence of 25% only, on the overall result. This mode is perfect for detection of soft obstacles, or for usage of CoolStep on imprecise motors. In filtered mode, sensitivity to a sudden load increase (hard motor blockage) is reduced.

Detecting a Motor Stall

To safely detect a motor stall, the stall threshold must be determined using a specific *SG4_THRS* setting and a specific motor velocity or velocity range. Further, the motor current setting has a certain influence and should not be modified, once optimum values are determined. Therefore, the maximum load needs to be determined the motor can drive without stalling. At the same time, monitor *SG4_RESULT* at this load. The stall threshold should be a value safely within the operating limits, to allow for parameter stray. More refined evaluation may also react to a change of *SG4_RESULT* rather than comparing to a fixed threshold. This will rule out certain effects which influence the absolute value.

Limits of StallGuard4 Operation

StallGuard4 does not operate reliably at extreme motor velocities: Very low motor velocities (for many motors, less than 1Rps) generate a low back EMF and make the measurement unstable and dependent on environment conditions (temperature, etc.). Other conditions will also lead to a poor response of the measurement value *SG4_RESULT* to the motor load. Very high motor velocities, in which the full sinusoidal current is not driven into the motor coils also leads to poor response. These velocities are typically characterized by the motor back EMF exceeding the supply voltage.

CoolStep Operation

CoolStep is an automatic smart energy optimization for stepper motors based on the motor mechanical load, making them "green." Depending on the actual chopper mode, CoolStep automatically uses StallGuard4 load measurement result in StealthChop2, or StallGuard2 in SpreadCycle. However, the tuning has to be done for either one or the other. A single tuning does not cover all operating points.

Setting Up for CoolStep

CoolStep is controlled by several parameters, but two are critical for understanding how it works:

Table 21. CoolStep Critical Parameters

The figure below shows the operating regions of CoolStep:

- The black line represents the *SG_RESULT* measurement value.
- The blue line represents the mechanical load applied to the motor.
- The red line represents the current into the motor coils.

When the load increases, *SG_RESULT* falls below *SEMIN*, and CoolStep increases the current. When the load decreases, *SG_RESULT* rises above (*SEMIN* + *SEMAX* + 1) x 32, and the current is reduced.

Figure 23. CoolStep Adapts Motor Current to the Load

Table 22. CoolStep Additional Parameters and Status Information

Tuning CoolStep

Before tuning CoolStep in conjunction with SpreadCycle, first tune the StallGuard2 threshold level *SGT*, which affects the range of the load measurement value *SG_RESULT*. CoolStep uses *SG_RESULT* to operate the motor near the optimum

load angle of +90°. In conjunction with StealthChop2, CoolStep uses *SG4_RESULT*. In this mode, the leveling is done via *SEMIN*.

The current increment speed is specified in *SEUP*, and the current decrement speed is specified in *SEDN*. They can be tuned separately because they are triggered by different events that may need different responses. The encodings for these parameters allow the coil currents to be increased much more quickly than decreased, because crossing the lower threshold is a more serious event that may require a faster response. If the response is too slow, the motor may stall. In contrast, a slow response to crossing the upper threshold does not risk anything more serious than missing an opportunity to save power.

CoolStep operates between limits controlled by the current scale parameter *IRUN* and the *seimin* bit.

Response Time

For fast response to increasing motor load, use a high current increment step *SEUP*. If the motor load changes slowly, a lower current increment step can be used to avoid motor oscillations. If the filter controlled by *sfilt* is enabled, the measurement rate and regulation speed are cut by a factor of four.

Advice: The most common and most beneficial use is to adapt CoolStep for operation at the typical system target operation velocity and to set the velocity thresholds according. As acceleration and decelerations normally shall be quick, they will require the full motor current, while they have only a small contribution to overall power consumption due to their short duration.

Low Velocity and Standby Operation

As CoolStep is not able to measure the motor load in standstill and at very low RPM, a lower velocity threshold is provided in the driver. It should be set to an application specific default value. Below this threshold the normal current setting via *IRUN* respectively *IHOLD* is valid. An upper threshold is provided by the *VHIGH* setting. Both thresholds can be set as a result of the StallGuard2 tuning process.

Diagnostic Outputs

Operation with an external motion controller often requires quick reaction to certain states of the stepper motor driver. Therefore, the DIAG outputs supply a configurable set of different real time information complementing the STEP/DIR interface.

Both, the information available at DIAG0 and DIAG1 can be selected as well as the type of output (low active open drain – default setting, or high active push-pull). In order to determine a reset of the driver, DIAG0 always shows a power-on reset condition by pulling low during a reset condition. The figure below shows the available signals and control bits.

Figure 24. DIAG0 and DIAG1 Output Options

The stall output signal allows StallGuard to be handled by the external motion controller like a stop switch.

Depending on the chopper mode, it becomes activated whenever the StallGuard value *SG_RESULT* reaches zero, respectively when *SG4_RESULT* falls below *SG4_THRS*, and at the same time the velocity condition is fulfilled (*TSTEP* ≤ *TCOOLTHRS*).

Chopper on-state shows the on-state of both coil choppers (alternating) when working in SpreadCycle or constant off time in order to determine the duty cycle.

The index output signals the microstep counter zero position to allow the application to reference the drive to a certain current pattern.The duration of the index pulse corresponds to the duration of the microstep. When working without interpolation at less than 256 microsteps, the index time goes down to two CLK clock cycles. The index output signals the positive zero transition of the coil B microstep wave.

Figure 25. Index Signal at Positive Zero Transition of the Coil B Microstep Wave

Sine Wave Lookup Table

The TMC2240 provides a programmable look-up table for storing the microstep current wave. As a default, the table is pre-programmed with a sine wave, which is a good starting point for most stepper motors. Reprogramming the table to a motor specific wave allows drastically improved microstepping especially with low-cost motors. The user benefits are:

- Microstepping extremely improved with low cost motors
- $Motor runs smooth and quiet$
- Torque reduced mechanical resonances yields improved torque
- Low frequency motor noise reduced by adapting the sine & cosine wave shift for the actual motor's manufacturing tolerance

Microstep Table

In order to minimize required memory and the amount of data to be programmed, only a quarter of the wave becomes stored. The internal microstep table maps the microstep wave from 0° to 90°. It becomes symmetrically extended to 360°. When reading out the table the 10-bit microstep counter *MSCNT* addresses the fully extended wave table. The table is stored in an incremental fashion, using each one bit per entry. Therefore only 256 bits (*ofs00* to *ofs255*) are required to store the quarter wave. These bits are mapped to eight 32 bit registers. Each *ofs* bit controls the addition of an inclination *Wx* or *Wx*+1 when advancing one step in the table. When *Wx* is 0, a 1 bit in the table at the actual microstep position means "add one" when advancing to the next microstep. As the wave can have a higher inclination than 1, the base inclinations *Wx* can be programmed to -1, 0, 1, or 2 using up to four flexible programmable segments within the quarter wave. This way even a negative inclination can be realized. The four inclination segments are controlled by the position registers *X1* to *X3*. Inclination segment 0 goes from microstep position 0 to *X1*-1 and its base inclination is controlled by *W0*, segment 1 goes from *X1* to *X2*-1 with its base inclination controlled by *W1*, etc.

When modifying the wave, care must be taken to ensure a smooth and symmetrical zero transition when the quarter wave becomes expanded to a full wave. The maximum resulting swing of the wave should be adjusted to a range of -248 to 248, in order to give the best possible resolution while leaving headroom for the hysteresis based chopper to add an offset.

Figure 26. LUT Programming Example

When the microstep sequencer advances within the table, it calculates the actual current values for the motor coils with each microstep and stores them to the registers *CUR_A* and *CUR_B*. However, the incremental coding requires an absolute initialization, especially when the microstep table becomes modified. Therefore, *CUR_A* and *CUR_B* become initialized whenever *MSCNT* passes zero.

Matching the phase shift to the motor:

Two registers control the starting values of the tables.

- As the starting value at zero is not necessarily 0 (it might be 1 or 2), it can be programmed into the starting point register *START_SIN*.
- In the same way, the start of the second wave for the second motor coil needs to be stored in *START_SIN90*. This register stores the resulting table entry for a phase shift of 90° for a two-phase motor. To adapt for motor tolerances, the phase shift can be modified from 90° (256 microsteps) to anywhere between 45° and 135°, by adding a microstep offset in the range of -127 to +127 (register *OFFSET_SIN90*). Motor tolerance will require moderate adaptations of a few, to a few 10 steps, maximum. The required correction offset can be found out using StallGuard4 individual values *SG4_IND* and trimming the offset, until both coils give a symmetrical result.

Figure 27. Shifting the Cosine Wave via OFFSET_SIN90

The default table is a good base for realizing an own table. This is an initialization example for the reset default microstep table:

MSLUT[0] = %10101010101010101011010101010100 = 0xAAAAB554 *MSLUT[1]* = %01001010100101010101010010101010 = 0x4A9554AA *MSLUT[2]* = %00100100010010010010100100101001 = 0x24492929 *MSLUT[3]* = %00010000000100000100001000100010 = 0x10104222 *MSLUT[4]* = %11111011111111111111111111111111 = 0xFBFFFFFF *MSLUT[5]* = %10110101101110110111011101111101 = 0xB5BB777D *MSLUT[6]* = %01001001001010010101010101010110 = 0x49295556

MSLUT[7] = %00000000010000000100001000100010 = 0x00404222

MSLUTSEL = 0xFFFF8056: *X1* = 128, *X2* = 255, *X3* = 255 *W3* = %01, *W2* = %01, *W1* = %01, *W0* = %10

MSLUTSTART = 0x00F70000:

START_SIN_0 = 0, *START_SIN90* = 247

To optimize the motor phase shift, run the motor at a medium velocity in StealthChop2 and set *sg4_filt_en* = 1. Adapt the phase offset to match the StallGuard4 results for phase A (*SG4_IND_0*+*SG4_IND_1*) to phase B (*SG4_IND_2*+*SG4_IND_3*).

If phase A value is > phase B value, increment *OFFSET_SIN90*, otherwise decrement. Repeat until best match is found.

Be sure to enter the correct value for *START_SIN90*. For an offset of -10 to +9 use *START_SIN90 =* 247; up to -17 or +17 use *START_SIN90 =* 246. *START_SIN* is always 0.

ABN Incremental Encoder Interface

The TMC2240 is equipped with an incremental encoder interface for ABN encoders. The encoder gives positions via digital incremental quadrature signals (usually named A and B) and an index signal (usually named N for null, Z for zero, or I for index).

N Signal

The N signal can be used to clear the position counter or to take a snapshot. To continuously monitor the N channel and trigger clearing of the encoder position or latching of the position, where the N channel event has been detected, set the flag *clr_cont*. Alternatively, it is possible to react to the next encoder N channel event only, and automatically disable the clearing or latching of the encoder position after the first N signal event (flag *clr_once*). This might be desired because the encoder gives this signal once for each revolution.

Some encoders require a validation of the N signal by a certain configuration of A and B polarity. This can be controlled by *pol_A* and *pol_B* flags in the *ENCMODE* register. For example, when both *pol_A* and *pol_B* are set, an active N-event is only accepted during a high polarity of both, A and B channel.

For clearing the encoder position *ENC_POS* with the next active N event set *clr_enc_x* = 1 and *clr_once* = 1 or *clr_cont* $= 1.$

Figure 28. Outline of ABN Signals of an Incremental Encoder

The Encoder Constant *ENC_CONST*

The encoder constant *ENC_CONST* is added to or subtracted from the encoder counter on each polarity change of the quadrature signals AB of the incremental encoder. The encoder constant *ENC_CONST* represents a signed fixed point number (16.16) to facilitate the generic adaption between motors and encoders. In decimal mode, the lower 16 bits represent a number between 0 and 9999. For stepper motors equipped with incremental encoders the fixed number representation allows very comfortable parameterization. Additionally, mechanical gearing can easily be taken into account. Negating the sign of *ENC_CONST* allows inversion of the counting direction to match motor and encoder direction.

Examples:

- Encoder factor of 1.0: *ENC* CONST = 0x0001.0x0000 = FACTOR.FRACTION
- Encoder factor of -1.0: *ENC_CONST* = 0xFFFF.0x0000. This is the two's complement of 0x00010000. It equals (2^16-(FACTOR+1)).(2^16-FRACTION)
- Decimal mode encoder factor $25.6: 00025.6000 = 0x0019.0x1770 = FACTOR.DECIMALS (DECIMALS = first 4)$ digits of fraction)
- Decimal mode encoder factor -25.6: $(2^{A}16-(25+1))$.(10000-6000) = (2^16 26).(4000) = 0xFFE6.0x0FA0.
	- A negative encoder constant is calculated using the following equation: (2^16-(FACTOR+1)).(10000-DECIMALS)

The Encoder Counter *X_ENC*

The encoder counter *X_ENC* holds the current encoder position ready for read out. Different modes concerning handling of the signals A, B, and N take into account active low and active high signals found with different types of encoders. For more details, see the Register Map.

The Register *ENC_STATUS*

The register *ENC_STATUS* holds the status concerning the event of an encoder clear upon an N channel signals. The

register *ENC_LATCH* stores the actual encoder position on an N signal event.

Checking for encoder latched event

Option 1: Check ENC_LATCH for change. It starts up with 0, and will show the encoder count where the N-event occurred, after starting motion for the first time. For consecutive rotations, it will show increased / decreased values and thus always changes.

Option 2: Check for the interrupt output active, and read the flag only following active interrupt output.

Please do not use the *ENC_STATUS* event flag for active, high-frequent polling, as in the event of a parallel read event and encoder N event, the flag will be cleared at the same moment, and will be missed.

Setting the Encoder to Match Motor Resolution

Encoder example settings for motor parameters: USC = 256 microsteps, 200 fullstep motor

Factor = FSC x USC/encoder resolution

Table 23. Encoder Example Settings for a 200 Fullstep Motor with 256 Microsteps

Example:

The encoder constant register shall be programmed to 51.2 in decimal mode. Therefore, set

ENC_CONST = $51 \times 2^{16} + 0.2 \times 10000$

Reset, Disable/Stop and Power Down

Emergency Stop

The driver provides a negative active enable pin DRV_ENN to safely switch off all power MOSFETs. This allows putting the motor into freewheeling. Further, it is a safe hardware function whenever an emergency stop not coupled to software is required. Some applications may require the driver to be put into a state with active holding current or with a passive braking mode. This is possible by programming the pin ENCA to act as a step disable function. Set GCONF flag *stop_enable* to activate this option. Whenever ENCA becomes pulled high and as long as it stays high, the motor will stop abruptly and go to the power down state, as configured via *IHOLD*, *IHOLD_DELAY* and StealthChop2 standstill options.

External Reset and Sleep Mode

The reset and sleep mode are controlled with the SLEEPN pin.

A short pulse on SLEEPN with a duration >30µs results in a chip reset (also visible at the diagnostics outputs).

Very short pulses <30µs are filtered out and will not have an effect on operation.

If SLEEPN is kept at GND, the IC goes into low-power standby state (sleep mode). All internal supplies are switched off.

In both cases reset and standby all internal register values and configurations are cleared and set to their defaults and power bridges are off.

After power-up or leaving sleep mode and reset condition the registers need to be re-configured.

While reconfiguring the IC it is advised to still hold the bridge drivers disabled with DRV_ENN. Do not use during high motor velocity as energy fed back from the motor might damage the chip! If not used connect to V_S or V_{CC} IO (this is a high voltage pin).

Restart the Stepper Motor Without Position Loss

A self-locking drive allows switching off the motor completely without loss of position. Locking can result from mechanical friction and from the stepper motor cogging torque. Most stepper motors have a cogging torque in the range of a few percent of their nominal torque, which also will contribute to the motor locking in a certain position. Due to their construction, most motors lock at a fullstep position. A full step position is characterized by the position yielded with both coils at identical absolute current. With n-times microstepping, fullstep positions are reached each n steps. The first fullstep position is reached when exactly n/2 steps are done following a driver power-up. The internal

microstep counter shows 128, 384, 640, or 896 when a fullstep position is reached.

The motor will pull into the same step after power up, as long as the rotor position and electrical position differ by up to +-2 fullsteps, given that no external force pulls the motor into a certain direction. An offset of maximum one fullstep is safest.

When powering up the driver, all registers become reset to zero. This also affects the internal position counter. Thus, the position counter will restart from 0 after power up. With the enable pin fixed at "1", the motor current will pull the motor to this (halfstep) position. With this, several options to keep track of the motor position result:

Table 24. Methods for Position Recovery

Protections and Driver Diagnostics

The TMC2240 drivers supply a complete set of diagnostic and protection capabilities, like short to GND protection and undervoltage detection. A detection of an open load condition allows testing if a motor coil connection is interrupted. See the *DRV_STATUS* register table for details.

Besides the status flags the TMC2240 allows measurement and read out of the chip temperature as well as feedback on the motor phase winding temperature.

For improved system reliability and overall circuit protection the TMC2240 contains an overvoltage comparator and a trigger output OV to control external switches in terms of excessive supply voltage increase.

Overcurrent Protection

An overcurrent protection (OCP) protects the device against short circuits to the rails (supply voltage and ground) and between the outputs (OUT1A, OUT2A, OUT1B, OUT2B).

The OCP threshold depends on the selected full-scale current range or see the Electrical Characteristics table for the respective threshold values.

The full scale range is selected with the *CURRENT_RANGE* parameter in *DRV_CONF* register.

If the output current is greater than the OCP threshold for longer than the deglitch time (blanking time), then an OCP event is detected.

When an OCP event is detected, the H-bridge is immediately disabled.

The short protection is trying 3 times before a fault flag (*s2ga*, *s2gb*, *s2vsa*, *s2vsb* in *DRV_STATUS* register) is set and the bridge becomes continuously disabled.

The device is still alive and allows for configuration and status read out.

To re-enable the power bridge DRV_ENN pin must be cycled.

Another option is to disable the power bridge with *TOFF* = 0 in *CHOPCONF* and re-enable the bridges with *TOFF > 0.*

Thermal Protection and Shutdown

The TMC2240 has an internal thermal protection.

If the die temperature exceeds 165°C (typical value), a fault indication a fault flag (*ot* in *DRV_STATUS*) is raised and the driver is three-stated until the junction temperature drops below ca. 145°C (typical value). After that, the driver is reenabled.

In addition, the TMC2240 supports ADC-based configurable thermal pre-warning levels. This can be configured in register *OTW_OV_VTH* using parameter *OVERTEMPPREWARNING_VTH*. The ADC senses the chip average temperature, while the driver stages may be at a much higher temperature. This is only to specify that TMC2240 can go in thermal shutdown and the pre-warning may not be asserted, even if it is set at a low temperature.

Heat is mainly generated by the motor driver stages, and, at increased voltage, by the internal voltage regulator. Most critical situations, where the driver MOSFETs could be overheated, are avoided when enabling the short to GND protection. For many applications, the overtemperature pre-warning will indicate an abnormal operation situation and can be used to initiate user warning or power reduction measures like motor current reduction. The thermal shutdown is just an emergency measure and temperature rising to the shutdown level should be prevented by design.

Temperature Measurement

The TMC2240 offers functions to measure the internal chip temperature as well as the motor temperature.

These diagnostic functions can be helpful in applications to monitor the chip or PCB temperature and the motor temperature development over time to increase system robustness or gather additional information for predictive maintenance.

Chip Temperature Measurement

Besides the overtemperature pre-warning and overtemperature flags the chip temperature itself can be determined using the *ADC_TEMP* parameter in the *ADC_TEMP* register.

The final temperature in degree Celsius can be calculated using the following formula:

ADC_TEMP = 7.7 × TEMP + 2038

TEMP[° C] = <u>ADC_TEMP − 2038</u>

Motor Temperature Measurement

PWM_SCALE register shows the actual duty cycle in StealthChop2 operation. For a given motor current, the duty cycle depends on the phase resistance of the motor.

As the phase resistance is temperature dependent, *PWM_SCALE* can be used to estimate the actual motor temperature and monitor changes in the motor temperature over time.

This measurement is preferably done during motor standstill or slow movements.

Typically, the motor temperature does not change quickly.

Overvoltage Protection and Pin OV

A stepper motor application can generate significant overvoltage, especially when the motor becomes quickly decelerated from a high velocity, or when the motor stalls.

This voltage becomes fed back to the supply rails by the driver output stage.

For typical NEMA17 or larger motors, and also for smaller motors with sufficient flywheel mass, the energy fed back can be substantial, so that the power capacitors and circuit consumption will not be sufficient to keep the supply within its limits.

To protect the driver as well as connected circuitry, the TMC2240 has an overvoltage detection and protection mechanism.

The OV output allows attaching an NPN or MOSFET with a power resistor (brake resistor) to dump the excess energy into the resistor.

The transistor will chop with approximately 3kHz to 4kHz (depending on the clock frequency) to keep the supply within the limits.

The supply voltage is permanently monitored with the internal ADC.

The upper level for the supply voltage for a given application can be configured in register *OTW_OV_VTH* using parameter *OVERVOLTAGE_VTH.*

The actual ADC value for the supply voltage can be read via register *ADC_VSUPPLY_AIN* as parameter *ADC_VSUPPLY.*

The OV output pin shows the actual state of the overvoltage monitor.

As soon as and as long as *ADC_VSUPPLY* becomes greater or equal to *OVERVOLTAGE_VTH* the OV output pin changes to three-state/'Z'.

The OV output pin is an open-drain pin. The following diagram shows an example brake chopper circuit.

Figure 29. Brake Chopper Circuit Example

Short to GND Protection

The TMC2240 power stages are protected against a short circuit condition by an additional measurement of the current flowing through the high-side MOSFETs. This is important, as most short circuit conditions result from a motor cable insulation defect, e.g. when touching the conducting parts connected to the system ground. The short detection is protected against spurious triggering, e.g., by ESD discharges, by retrying three times before switching off the motor.

Once a short condition is safely detected, the corresponding driver bridge becomes switched off, and the *s2ga* or *s2gb* flag becomes set. In order to restart the motor, the user must intervene by disabling and re-enabling the driver. It should be noted, that the short to GND protection cannot protect the system and the power stages for all possible short events,

as a short event is rather undefined and a complex network of external components may be involved. Therefore, shortcircuits should basically be avoided.

Open Load Diagnostics

Interrupted cables are a common cause for systems failing, e.g., when connectors are not firmly plugged. The TMC2240 detects open load conditions by checking, if it can reach the desired motor coil current. This way, also undervoltage conditions, high motor velocity settings or short and overtemperature conditions may cause triggering of the open load flag, and inform the user, that motor torque may suffer. In motor stand still, open load cannot be measured, as the coils might eventually have zero current.

To safely detect an interrupted coil connection, operate in SpreadCyle, and check the open load flags following a motion of minimum four times the selected microstep resolution into a single direction using low or nominal motor velocity operation, only. However, the *ola* and *olb* flags have just informative character and do not cause any action of the driver.

Undervoltage Lockout Protection

The TMC2240 features a UVLO protection for V_M , V_{CC} _{IO}, and the charge pump.

UVLO condition on V_M is triggered below 4.15V (max).

UVLO condition on $V_{CC~IO}$ is triggered below 1.95V (max).

UVLO condition on the charge pump is triggered in case of an error condition of the charge pump, e.g., due to a wrong capacitor value.

A VM UVLO condition can be read from register *GSTAT* as flag *vm_uvlo.* This flag is a write-clear flag. It must be actively set to 1 to clear it. The UVLO condition is also shown at the DIAG0 pin depending on the configured pin settings.

During a V_{CC-IO} UVLO, no communication with the IC is possible. DIAG0 pin will be active low (open drain).

ESD Protection

The chip has internal ESD protection on every pin.

The TMC2240 motor phase output pins are protected up to 8KV HBM in the application when using a bypass capacitor of at least 1uF on the positive voltage supply (V_M Pin).

Anyhow, this is no protection against hot plugging of a motor.

Clock Oscillator and Clock Input

Using the Internal Clock

Directly tie the CLK input pin to GND close to the IC if the internal clock oscillator is to be used.

Using an External Clock

When an external clock is available, a frequency of 12MHz to 20MHz is recommended for optimum performance.

The duty cycle of the clock signal is uncritical, as long as minimum high or low input time for the pin is satisfied (see *Electrical Characteristics*).

Up to 20MHz can be used, when the clock duty cycle is 50%.

Make sure, that the clock source supplies clean CMOS output logic levels and steep slopes when using a high clock frequency.

The external clock input is enabled as soon as an external clock is provided at the CLK pin.

Reading out bit *ext_clk* in register *IOIN* gives feedback on which clock source is currently in use (1 = external clock).

In case the external clock fails or is switched off, the internal clocks takes over seamlessly and automatically to prevent the driver from damage.

General Register Mapping and Register Information

This section gives some general information on the register map.

Details on all registers and their content are given in the register map section.

- All registers become reset to 0 upon power up, unless otherwise noted.
- Add 0x80 to the address Addr for write accesses!

Table 25. Overview of Register Map

Register Map

TMC2240

Register Details

GCONF (0x0)

Global Configuration Flags

GSTAT (0x1)

Global Status Flags

(Re-Write with '1' bit to clear respective flags)

IFCNT (0x2)

Interface transmission counter.

This register becomes incremented with each successful UART interface write access. It can be read out to check the serial transmission for lost data. Read accesses do not change the content. Disabled in SPI operation. The counter wraps around from 255 to 0.

SLAVECONF (0x3)

IOIN (0x4)

Reads the state of all input pins available and returns IC revision in highest byte

DRV_CONF (0xA)

GLOBAL SCALER (0xB)

IHOLD_IRUN (0x10)

Test Reg

TPOWERDOWN (0x11)

TSTEP (0x12)

TPWMTHRS (0x13)

TCOOLTHRS (0x14)

THIGH (0x15)

DIRECT_MODE (0x2D)

ENCMODE (0x38)

X_ENC (0x39)

ENC_CONST (0x3A)

ENC_STATUS (0x3B)

Encoder status information

corresponding position.

ENC_LATCH (0x3C)

ADC_VSUPPLY_AIN (0x50)

ADC_TEMP (0x51)

OTW_OV_VTH (0x52)

MSLUT_0 (0x60)

MSLUT_1 (0x61)

Microstep table entries 32…63

MSLUT_2 (0x62)

Microstep table entries 64…95

MSLUT_3 (0x63)

Microstep table entries 96…127

MSLUT_4 (0x64)

Microstep table entries 128…159

MSLUT_5 (0x65)

Microstep table entries 160…191

MSLUT_6 (0x66)

Microstep table entries 192…223

MSLUT_7 (0x67)

Microstep table entries 224…255

MSLUTSEL (0x68)

MSLUTSTART (0x69)

Start values are transferred to the microstep registers *CUR_A* and *CUR_B*, whenever the reference position *MSCNT*=0 is passed.

MSCNT (0x6A)

MSCURACT (0x6B)

CHOPCONF (0x6C)

COOLCONF (0x6D)

DRV_STATUS (0x6F)

PWMCONF (0x70)

PWM_SCALE (0x71)

Results of StealthChop2 amplitude regulator. These values can be used to monitor automatic PWM amplitude scaling (255=max. voltage).

PWM_AUTO (0x72)

These automatically generated values can be read out in order to determine a default / power up setting for *PWM_GRAD* and *PWM_OFS*.

SG4_THRS (0x74)

SG4_RESULT (0x75)

SG4_IND (0x76)

TMC2240 36V 2ARMS⁺ Smart Integrated Stepper Driver with S/D and SPI

Typical Application Circuits

Standard Application Circuit

The standard application circuit uses a minimum set of additional components. Use low ESR capacitors for filtering the power supply. The capacitors need to cope with the current ripple cause by chopper operation. A minimum capacity of 100µF near the driver is recommended for best performance. Current ripple in the supply capacitors also depends on the power supply internal resistance and cable length. VCC IO must be supplied from an external source, e.g., a low drop 3.3V regulator.

Place all filter capacitors as close as possible to the related IC pins. Use a solid common GND for all GND connections. Connect VDD1V8 filtering capacitor directly to VDD1V8 pin. Low ESR electrolytic capacitors are recommended for VS filtering.

Figure 30. Standard Application Circuit

High Motor Current

When operating at a high motor current, the driver power dissipation due to MOSFET switch on-resistance significantly heats up the driver. This power dissipation will heat up the PCB cooling infrastructure also, if operated at an increased duty cycle. This in turn leads to a further increase of driver temperature. An increase of temperature by about 100°C increases MOSFET resistance by roughly 50%. This is a typical behavior of MOSFET switches. Therefore, under high duty cycle, high load conditions, thermal characteristics have to be carefully taken into account, especially when increased environment temperatures are to be supported. Refer the thermal characteristics and the layout examples as well.

As a thumb rule, thermal properties of the PCB design may become critical at or above 1.5A RMS motor current for increased periods of time. Keep in mind that the resistive power dissipation raises with the square of the motor current. On the other hand, this means that a small reduction of motor current significantly saves heat dissipation and energy.

Typical Application Circuits (continued)

Driver Protection and EME Circuitry

Some applications have to cope with ESD events caused by motor operation or external influence. Despite ESD circuitry within the driver chips, ESD events occurring during operation can cause a reset or even a destruction of the motor driver, depending on their energy. Especially plastic housings and belt drive systems tend to cause ESD events of several kV. It is best practice to avoid ESD events by attaching all conductive parts, especially the motors themselves to PCB ground, or to apply electrically conductive plastic parts. In addition, the driver can be protected up to a certain degree against ESD events or live plugging / pulling the motor, which also causes high voltages and high currents into the motor connector terminals.

A simple scheme uses capacitors at the driver outputs to reduce the dV/dt caused by ESD events. Larger capacitors will bring more benefit concerning ESD suppression, but cause additional current flow in each chopper cycle, and thus increase driver power dissipation, especially at high supply voltages. The values shown are example values – they might be varied between 100pF and 1nF. The capacitors also dampen high frequency noise injected from digital parts of the application PCB circuitry and thus reduce electromagnetic emission.

Figure 31. Simple ESD Enhancement

A more elaborate scheme uses LC filters to de-couple the driver outputs from the motor connector. Varistors V1 and V2 in between of the coil terminals eliminate coil overvoltage caused by live plugging. Optionally protect all outputs by a varistor (V1A, V1B, V2A, V2B) against ESD voltage. Fit the varistors to the supply voltage rating. The SMD inductivities will conduct full motor coil current and need to be selected accordingly.

Typical Application Circuits (continued)

Figure 32. Elaborate Motor Output Protection

Ordering Information

** Future product—contact factory for availability.*

+ Denotes a lead(Pb)-free/RoHS-compliant package.

T Denotes tape-and-reel.

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Revision History

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