
1.2 A, 30 V Step Down DC/DC Converter for Automotive Applications

No. EC-269-201022

OUTLINE

The R1245x is a Step-down DC/DC converter with internal N-channel high side Tr. That is developed with CMOS process technology. The ON resistance of the built-in high-side transistor is $0.35\ \Omega$ and the R1245x can provide the maximum 1.2 A output current. Each of the ICs consists of an oscillator, a PWM control circuit, a voltage reference unit, an error amplifier, a phase compensation circuit, a slope compensation circuit, a soft-start circuit, protection circuits, an internal voltage regulator, and a switch for bootstrap circuit. The ICs can make up a step-down DC/DC converter with an inductor, resistors, a diode, and capacitors. The R1245x is a current mode operating type DC/DC converter without an external current sense resistor, and realizes fast response and high efficiency. As an output capacitor, a ceramic type capacitor can be used with the R1245x. The options of the internal oscillator frequency are preset at 330 kHz for version A and B, 500 kHz for version C and D, 1000 kHz for version E and F, 2400 kHz for version G and H. As for protection, an Lx peak current limit circuit cycle by cycle, a thermal shutdown function and an under voltage lockout (UVLO) function are built in. Furthermore, there are two types for short protection, for A/C/E/G version, a latch protection function which makes the output latch off if the output voltage keeps lower than the set output voltage for a certain time after detecting current limit is built in, for B/D/F/H version, a fold-back protection function which changes the oscillator frequency slower after detecting short circuit or equivalent. As for the packages of the R1245x, HSOP-8E and DFN2020-8 are available.

FEATURES

- Input Voltage Range (Maximum Rating) 4.5 V to 30 V (32 V)
- Operating Temperature -40°C to 105°C
- Internal N-channel MOSFET Driver Typ. $R_{\text{ON}} = 0.35\ \Omega$
- Adjustable Output Voltage with External Resistor 0.8 V or more
- Feedback Voltage and Tolerance $0.8\ \text{V} \pm 1.0\%$
- Peak Current Limit Typ. 2.0 A
- UVLO Function Released Voltage Typ. 4.0 V
- Operating Frequency 330 kHz (A/B version), 500 kHz (C/D version),
1000 kHz (E/F version), 2400 kHz (G/H version)
- Fold-back Protected Frequency 170 kHz (B/D version), 250 kHz (F version),
400 kHz (H version)
- Latch Protection Delay Time Typ. 4 ms for A/C/E/G version
- Built-in Thermal Shutdown Circuit Typ. 160°C
- Ceramic Capacitors Recommended for Input and Output
- Stand-by Current Typ. $0\ \mu\text{A}$
- Packages HSOP-8E, DFN2020-8

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APPLICATIONS

- Power source for car accessories including car audio equipment, car navigation system, and ETC system.
- Power source for control units including EV inverter and charge control.

SELECTION GUIDE

In the R1245x, the package, type of short protection (Latch or Fold-back), and the oscillator frequency can be selected with the user's request.

Selection Guide

Product Name	Package	Quantity per Reel	Pb Free	Halogen Free
R1245S003*-E2-#E	HSOP-8E	1,000 pcs	Yes	Yes
R1245L003*-TR-AE	DFN2020-8	3,000 pcs	Yes	Yes

*: Designation of the oscillator frequency and the protection function option.

Symbol	Oscillator Frequency	Latch Protection	Fold-back Protection
A	330 kHz	✓	
B	330 kHz		✓
C	500 kHz	✓	
D	500 kHz		✓
E	1000 kHz	✓	
F	1000 kHz		✓
G	2400 kHz	✓	
H	2400 kHz		✓

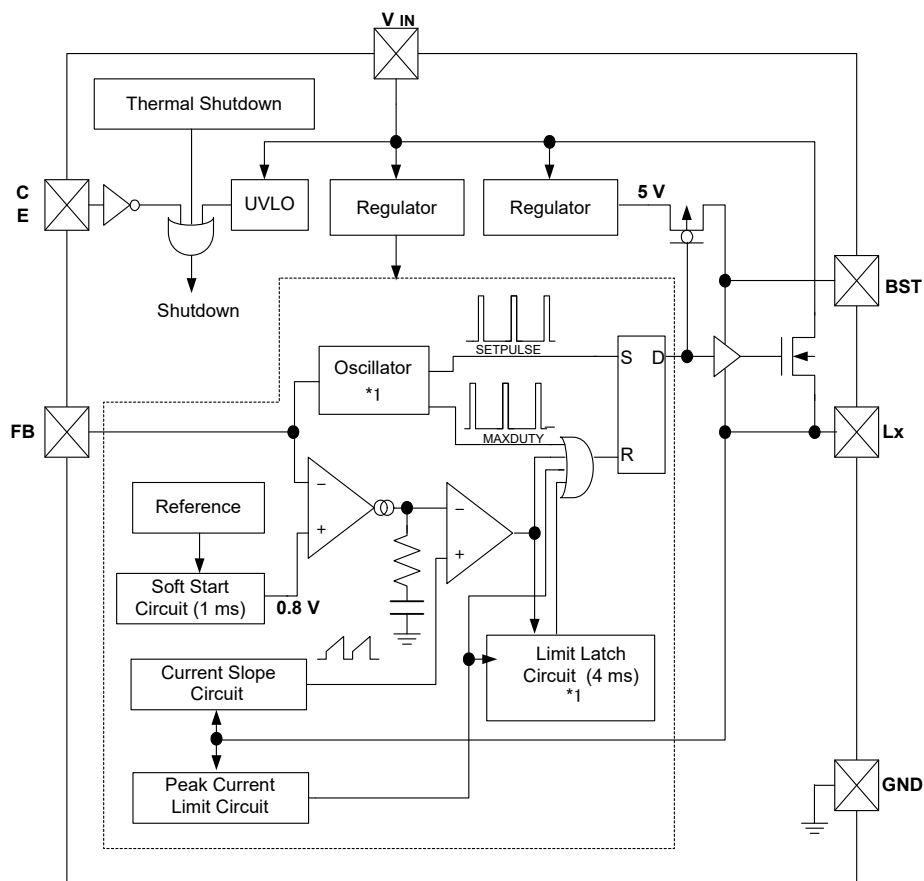
#: Designated Automotive Class Code

	Operating Temperature Range	Guaranteed Specs Temperature Range	Screening
A	-40°C to 105°C	25°C	High Temperature
J	-40°C to 105°C	-40°C to 105°C	High and low Temperature

Automotive class code (A, J) varies depending on the package and function.

Package	Function	Automotive Class Code	
		A	J
HSOP-8E	A, B, G, H	✓	✓
	C, D, E, F	✓	
DFN2020-8	A, B, C, D, E, F, G, H	✓	

BLOCK DIAGRAM



R1245x Block Diagram

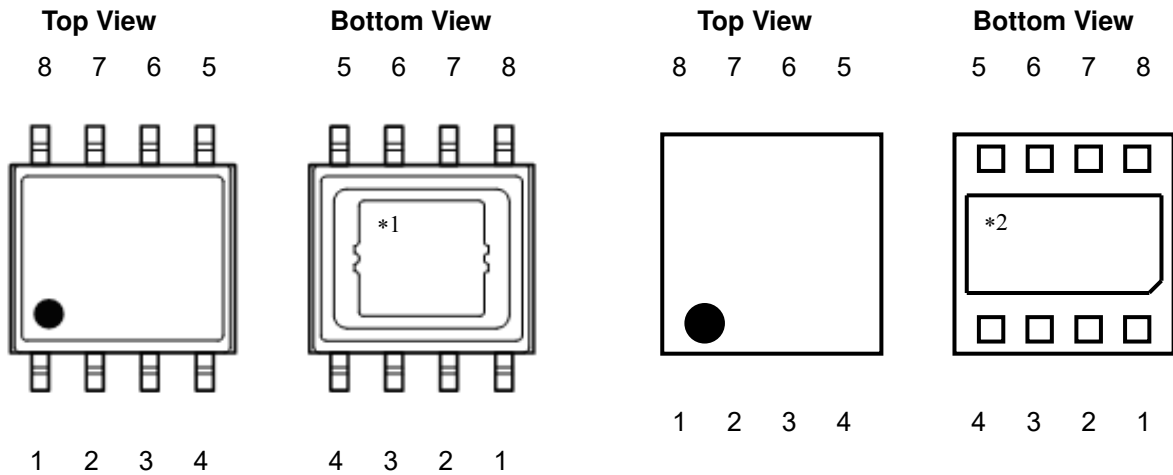
*1

Version	Oscillator Frequency	Short Protection Type
A	330 kHz	Latch
B	330 kHz	Fold-back
C	500 kHz	Latch
D	500 kHz	Fold-back
E	1000 kHz	Latch
F	1000 kHz	Fold-back
G	2400 kHz	Latch
H	2400 kHz	Fold-back

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PIN DESCRIPTIONS



SOP-8E Pin Configuration

DFN2020-8 Pin Configuration

R1245S Pin Description

Pin No.	Symbol	Description
1	Lx	Lx Switching Pin
2	VIN	Power Supply Pin
3	CE	Chip Enable Pin (Active with "H")
4	TEST	TEST pin (must be open for user side.)
5	GND* ¹	Ground Pin
6	FB	Feedback Pin
7	NC	No connection
8	BST	Bootstrap Pin

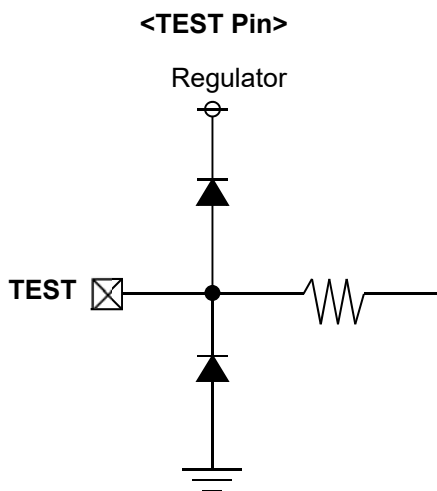
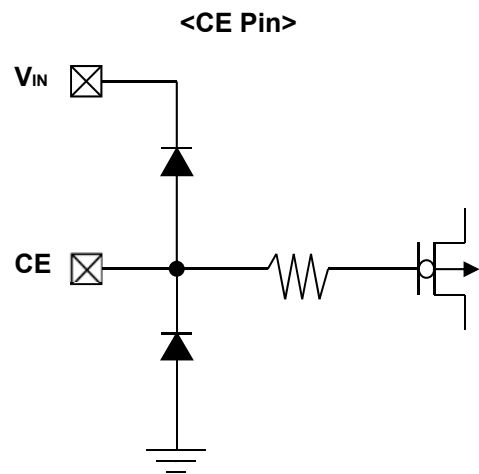
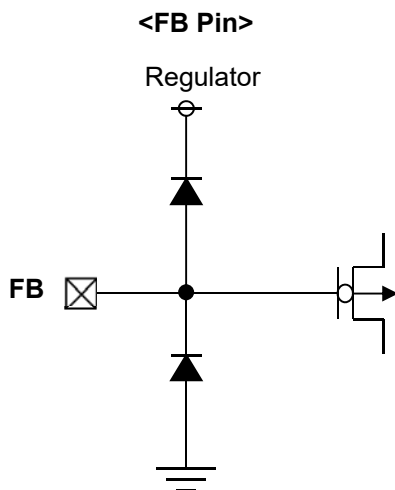
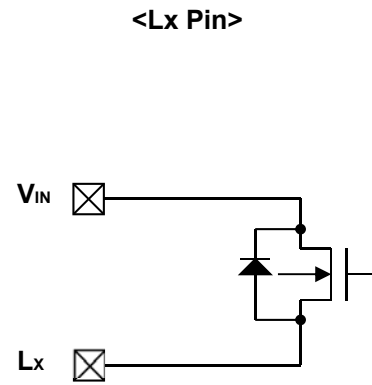
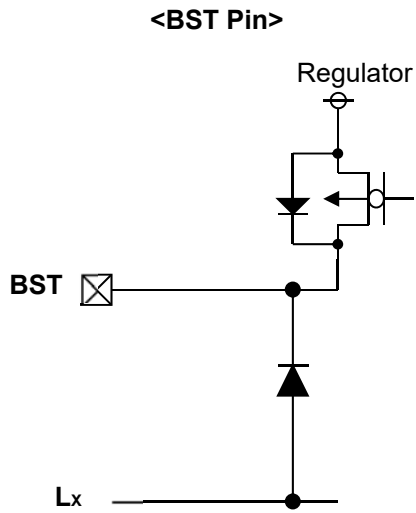
*¹ Connect the backside heat radiation tab to GND or same as GND level (recommendation). The tab is connected to the GND pin.

R1245L Pin Description

Pin No.	Symbol	Description
1	Lx	Lx Switching Pin
2	VIN	Power Supply Pin
3	VIN	Power Supply Pin
4	CE	Chip Enable Pin (Active with "H")
5	GND* ²	Ground Pin
6	FB	Feedback Pin
7	TEST	Test Pin (must be open for user side)
8	BST	Bootstrap Pin

*² Connect the backside heat radiation tab to GND or same as GND level (recommendation). The tab is connected to the GND pin.

INTERNAL EQUIVALENT CIRCUIT FOR EACH PIN



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ABSOLUTE MAXIMUM RATINGS

Absolute Maximum Ratings

(GND = 0 V)

Symbol	Item	Rating	Unit	
V _{IN}	Input Voltage	-0.3 to 32	V	
V _{BST}	BST Pin Voltage	V _{LX} - 0.3 to V _{LX} + 6	V	
V _{LX}	Lx Pin Voltage	-0.3 to V _{IN} + 0.3	V	
V _{CE}	CE Pin Input Voltage	-0.3 to V _{IN} + 0.3	V	
V _{FB}	Feedback Pin Voltage	-0.3 to 6	V	
P _D	Power Dissipation (HSOP-8E)* ¹	Ultra High Wattage Land Pattern	3600	mW
	Power Dissipation (DFN2020-8)* ¹	Standard Land Pattern	1100	
T _j	Junction Temperature	-40 to 150	°C	
T _{stg}	Storage Temperature Range	-55 to 150	°C	

*¹ Refer to *POWER DISSIPATION* for detailed information.

ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the lifetime and safety for both device and system using the device in the field. The functional operation at or over these absolute maximum ratings is not assured.

RECOMMENDED OPERATING CONDITIONS

Recommended Operating Conditions

Symbol	Item	Rating	Unit
V _{IN}	Input Voltage	4.5 to 30	V
T _a	Operating Temperature Range	-40 to 105	°C

RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such conditions by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

ELECTRICAL CHARACTERISTICS

$V_{IN} = 12\text{ V}$, unless otherwise noted.

The specifications surrounded by are guaranteed by design engineering at $-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$.

R1245x003x-AE Electrical Characteristics

($T_a = 25^{\circ}\text{C}$)

Symbol	Item	Conditions	Min.	Typ.	Max.	Unit	
I_{IN}	V_{IN} Consumption Current	$V_{IN} = 30\text{ V}$, $V_{FB} = 1.0\text{ V}$		0.5	1.80	mA	
V_{UVLO1}	UVLO Detect Voltage	Falling	3.55	V_{UVLO2} -0.2	V_{UVLO2} -0.05	V	
V_{UVLO2}	UVLO Released Voltage	Rising	3.75	4.0	4.25	V	
V_{FB}	VFB Voltage Tolerance	$T_a = 25^{\circ}\text{C}$	0.792	0.800	0.808	V	
		$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	0.781		0.819		
f_{osc}	Oscillator Frequency	Version A/B	$T_a = 25^{\circ}\text{C}$	300	330	360	kHz
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	280		380	
		Version C/D	$T_a = 25^{\circ}\text{C}$	450	500	550	
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	430		590	
		Version E/F	$T_a = 25^{\circ}\text{C}$	900	1000	1100	
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	870		1140	
		Version G/H	$T_a = 25^{\circ}\text{C}$	2200	2400	2600	
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	2150		2650	
f_{FLB}	Fold-back Frequency	Version B	$V_{FB} < 0.56\text{ V}$		170	kHz	
		Version D	$V_{FB} < 0.56\text{ V}$		170		
		Version F	$V_{FB} < 0.56\text{ V}$		250		
		Version H	$V_{FB} < 0.56\text{ V}$		400		
Maxduty	Oscillator Maximum Duty Cycle	Version A/B		91		%	
		Version C/D		91			
		Version E/F		86			
		Version G/H		74			
t_{start}	Soft-start Time	$V_{FB} = 0.72\text{ V}$		1.0		ms	
t_{DLY}	Delay Time for Latch Protection	Version A/G		4		ms	

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 $V_{IN} = 12\text{ V}$, unless otherwise noted.The specifications surrounded by are guaranteed by design engineering at $-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$.**R1245x003x-AE Electrical Characteristics**

(Ta = 25°C)

Symbol	Item	Conditions	Min.	Typ.	Max.	Unit
R_{LXH}	Lx High Side Switch ON Resistance	$V_{BST} - V_{LX} = 4.5\text{ V}$		0.35		Ω
I_{LXHOFF}	Lx High Side Switch Leakage Current	$V_{IN} = 30\text{ V}, V_{CE} = 0\text{ V}$		0	5.0	μA
I_{LIMLXH}	Lx High Side Switch Limited Current	$V_{BST} - V_{LX} = 4.5\text{ V}$	1.2	2.0		A
V_{CEL}	CE "L" Input Voltage	$V_{IN} = 30\text{ V}$			0.3	V
V_{CEH}	CE "H" Input Voltage	$V_{IN} = 30\text{ V}$	1.6			V
I_{FB}	VFB Input Current	$V_{IN} = 30\text{ V}, V_{FB} = 1.0\text{ V}$	-0.3	0	0.3	μA
I_{CEL}	CE "L" Input Current	$V_{IN} = 30\text{ V}, V_{CE} = 0\text{ V}$	-0.3	0	0.3	μA
I_{CEH}	CE "H" Input Current	$V_{IN} = 30\text{ V}, V_{CE} = 30\text{ V}$	-0.3	0	0.3	μA
Istandby	Standby Current	$V_{IN} = 30\text{ V}$		0	5.0	μA

All of units are tested and specified under load conditions such as $T_j \approx T_a = 25^{\circ}\text{C}$.

$V_{IN} = 12\text{ V}$, unless otherwise noted.

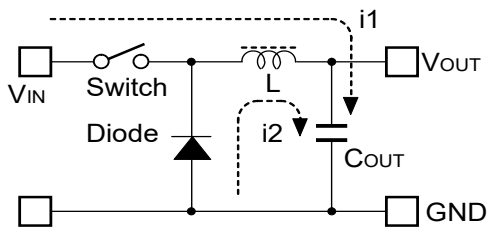
R1245x003x-JE Electrical Characteristics
 $(-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C})$

Symbol	Item	Conditions	Min.	Typ.	Max.	Unit	
I_{IN}	V_{IN} Consumption Current	$V_{IN} = 30\text{ V}$, $V_{FB} = 1.0\text{ V}$		0.5	1.80	mA	
V_{UVLO1}	UVLO Detect Voltage	Falling	3.55	V_{UVLO2} -0.2	V_{UVLO2} -0.05	V	
V_{UVLO2}	UVLO Released Voltage	Rising	3.75	4.0	4.25	V	
V_{FB}	VFB Voltage Tolerance	$T_a = 25^{\circ}\text{C}$	0.792	0.800	0.808	V	
		$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	0.781		0.819		
f_{OSC}	Oscillator Frequency	Version A/B	$T_a = 25^{\circ}\text{C}$	300	330	360	kHz
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	280		380	
		Version G/H	$T_a = 25^{\circ}\text{C}$	2200	2400	2600	
			$-40^{\circ}\text{C} \leq T_a \leq 105^{\circ}\text{C}$	2150		2650	
f_{FLB}	Fold-back Frequency	Version B	$V_{FB} < 0.56\text{ V}$		170	kHz	
		Version H	$V_{FB} < 0.56\text{ V}$		400		
Maxduty	Oscillator Maximum. Duty Cycle	Version A/B		91		%	
		Version G/H		74			
t_{start}	Soft-start Time	$V_{FB} = 0.72\text{ V}$		1.0		ms	
t_{DLY}	Delay Time for Latch Protection	Version A/G		4		ms	
R_{LXH}	Lx High Side Switch ON Resistance	$V_{BST} - V_{LX} = 4.5\text{ V}$		0.35		Ω	
I_{LXHOFF}	Lx High Side Switch Leakage Current	$V_{IN} = 30\text{ V}$, $V_{CE} = 0\text{ V}$		0	5.0	μA	
I_{LIMLXH}	Lx High Side Switch Limited Current	$V_{BST} - V_{LX} = 4.5\text{ V}$	1.2	2.0		A	
V_{CEL}	CE "L" Input Voltage	$V_{IN} = 30\text{ V}$			0.3	V	
V_{CEH}	CE "H" Input Voltage	$V_{IN} = 30\text{ V}$	1.6			V	
I_{FB}	VFB Input Current	$V_{IN} = 30\text{ V}$, $V_{FB} = 1.0\text{ V}$	-0.3	0	0.3	μA	
I_{CEL}	CE "L" Input Current	$V_{IN} = 30\text{ V}$, $V_{CE} = 0\text{ V}$	-0.3	0	0.3	μA	
I_{CEH}	CE "H" Input Current	$V_{IN} = 30\text{ V}$, $V_{CE} = 30\text{ V}$	-0.3	0	0.3	μA	
Istandby	Standby Current	$V_{IN} = 30\text{ V}$		0	5.0	μA	

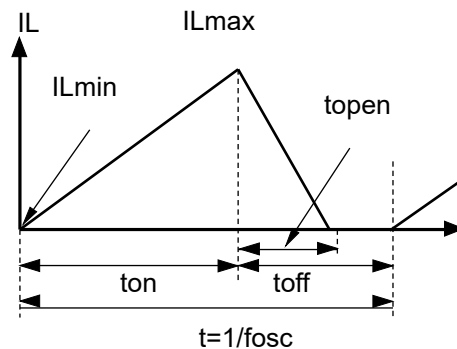
OPERATING DESCRIPTIONS

OPERATION OF THE BUCK CONVERTER AND THE OUTPUT CURRENT

The DC/DC converter charges energy in the inductor when the switch turns on, and discharges the energy from the inductor when the switch turns off and controls with less energy loss, so that a lower output voltage than the input voltage is obtained. Refer to the following figures.



Basic Circuit

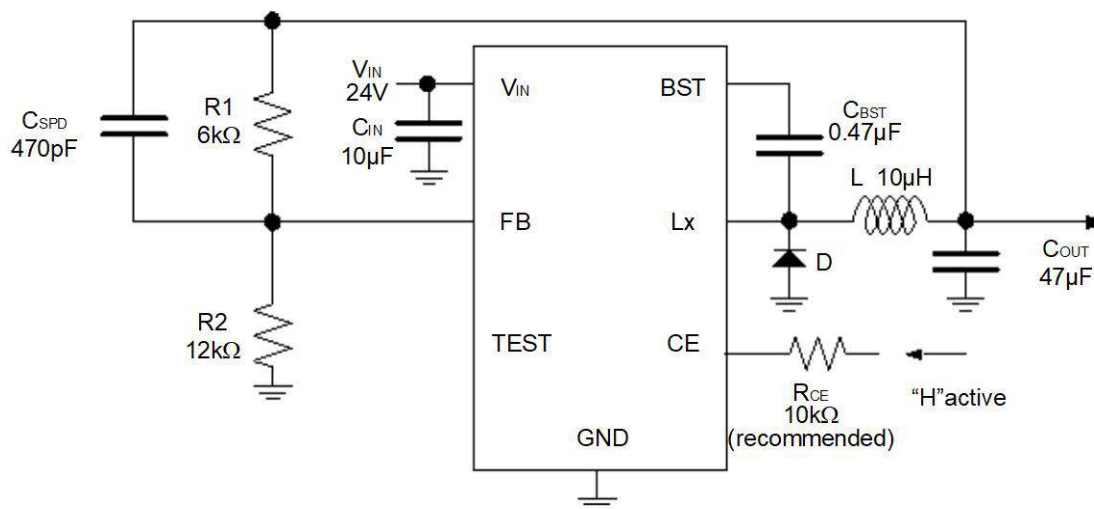
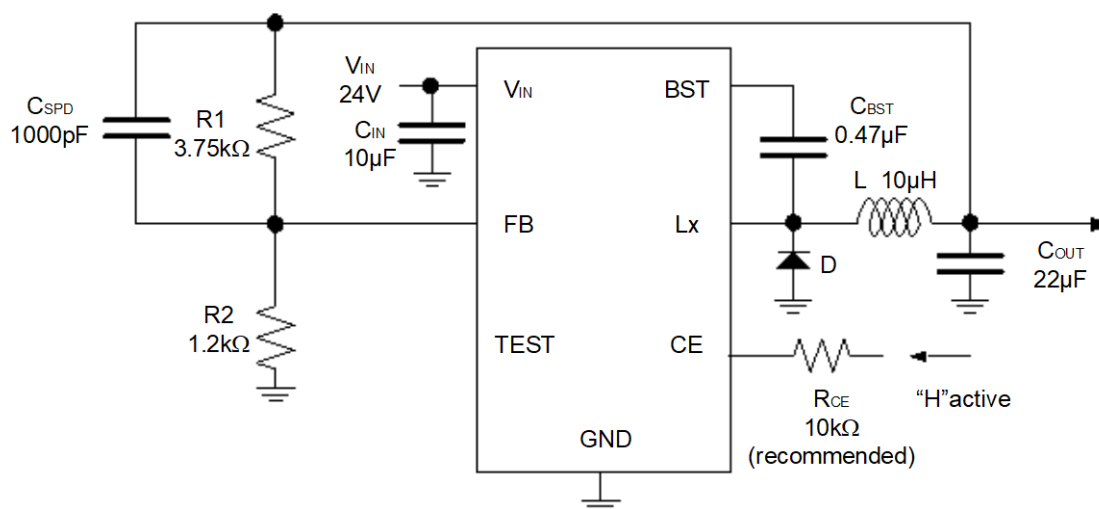


Current flowing through the Inductor

- Step 1: The switch turns on and current $I_L (= i_1)$ flows, and energy is charged into C_{OUT} . At this moment, I_L increases from $I_{Lmin} (= 0)$ to reach I_{Lmax} in proportion to the on-time period (t_{on}) of the switch.
- Step 2: When the switch turns off, the diode turns on in order to maintain I_L at I_{Lmax} , and current $I_L (= i_2)$ flows.
- Step 3: $I_L (= i_2)$ decreases gradually and reaches $I_L = I_{Lmin} = 0$ after a time period of t_{open} , and the diode turns off. This case is called as discontinuous mode. If the output current becomes large, next switching cycle starts before I_L becomes 0 and the diode turns off. In this case, I_L value increases from $I_{Lmin} (> 0)$, and this case is called continuous mode.

In the case of PWM control system, the output voltage is maintained by controlling the on-time period (t_{on}), with the oscillator frequency (f_{osc}) being maintained constant.

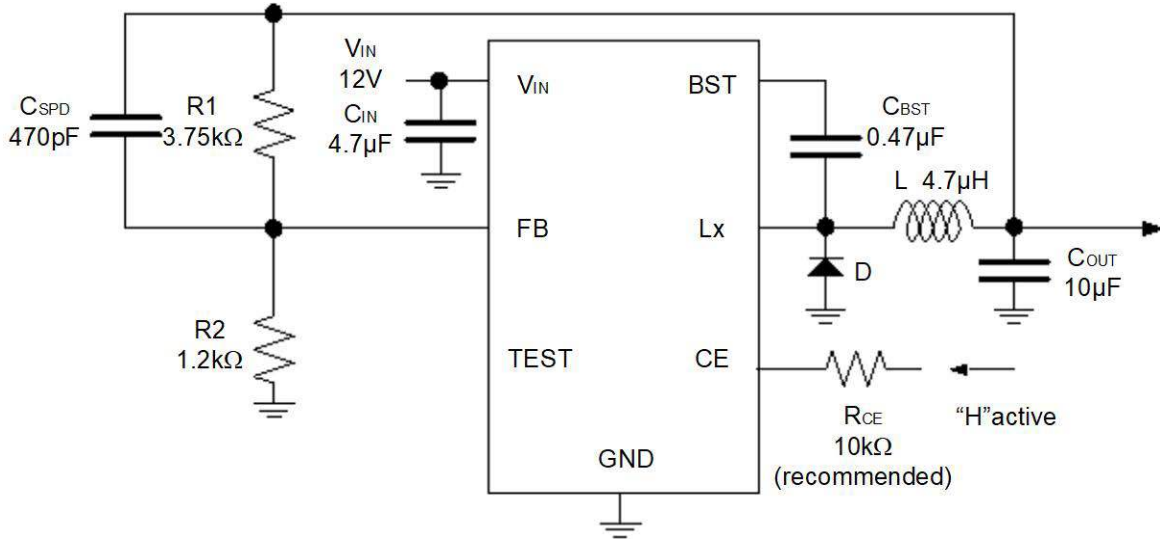
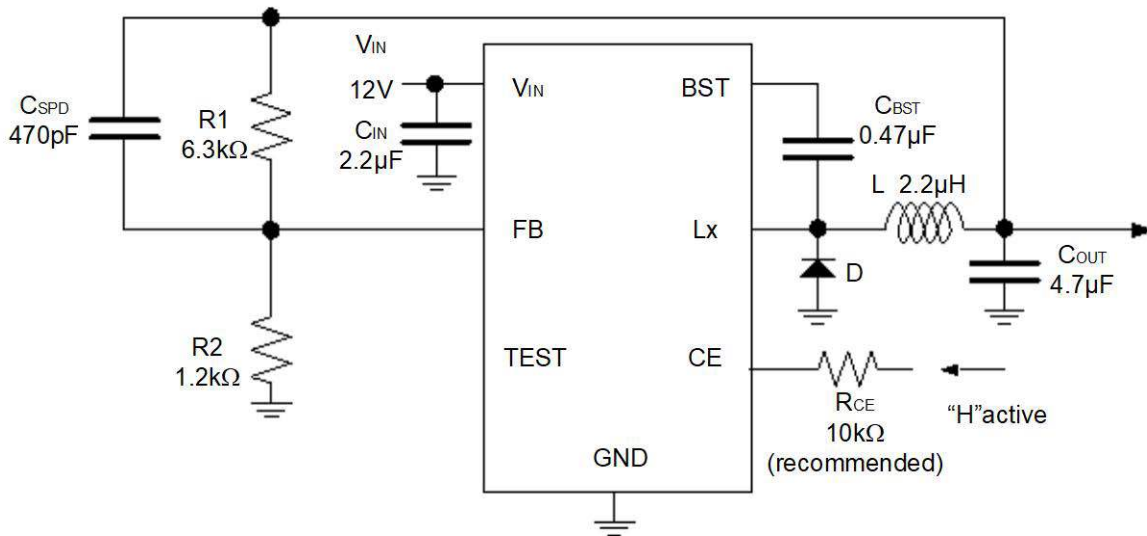
TYPICAL APPLICATION CIRCUIT

R1245x00xA/B Typical Application Circuit, 330 kHz, $V_{OUT} = 1.2\text{ V}$, $V_{IN} = 24\text{ V}$ R1245x00xC/D Typical Application Circuit, 500 kHz, $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 24\text{ V}$

*TEST pin must be open.

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**R1245x00xE/F Typical Application Circuit, 1000 kHz, $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$** **R1245x00xG/H Typical Application Circuit, 2400 kHz, $V_{OUT} = 5.0\text{ V}$, $V_{IN} = 12\text{ V}$**

*TEST pin must be open.

OUTPUT CURRENT AND SELECTION OF EXTERNAL COMPONENTS

The calculation method of output current and the relation between the output current and external components are as follows:

When the switch of Lx turns on:

(Wherein, the peak to peak value of the ripple current is described as I_{RP} , the ON resistance of the switch is described as R_{ONH} , and the diode forward voltage as V_F , and the DC resistance of the inductor is described as R_L , and on time of the switch is described as t_{on})

$$V_{IN} = V_{OUT} + (R_{ONH} + R_L) \times I_{OUT} + L \times I_{RP} / t_{on} \dots\dots\dots \text{Equation 1}$$

When the switch turns off (the diode turns on) as t_{off} :

$$L \times I_{RP} / t_{off} = V_F + V_{OUT} + R_L \times I_{OUT} \dots\dots\dots \text{Equation 2}$$

Put Equation 2 to Equation 1 and solve for ON duty of the switch, $t_{on} / (t_{off} + t_{on}) = D_{ON}$,

$$D_{ON} = (V_{OUT} + V_F + R_L \times I_{OUT}) / (V_{IN} + V_F - R_{ONH} \times I_{OUT}) \dots\dots\dots \text{Equation 3}$$

Ripple Current is as follows:

$$I_{RP} = (V_{IN} - V_{OUT} - R_{ONH} \times I_{OUT} - R_L \times I_{OUT}) \times D_{ON} / f_{osc} / L \dots\dots\dots \text{Equation 4}$$

wherein, peak current that flows through L, and the peak current I_{Lmax} is as follows:

$$I_{Lmax} = I_{OUT} + I_{RP} / 2 \dots\dots\dots \text{Equation 5}$$

As for the valley current I_{Lmin} ,

$$I_{Lmin} = I_{OUT} - I_{RP} / 2 \dots\dots\dots \text{Equation 6}$$

If $I_{Lmin} < 0$, the step-down DC/DC converter operation becomes current discontinuous mode.

Therefore the current condition of the current discontinuous mode, the next formula is true.

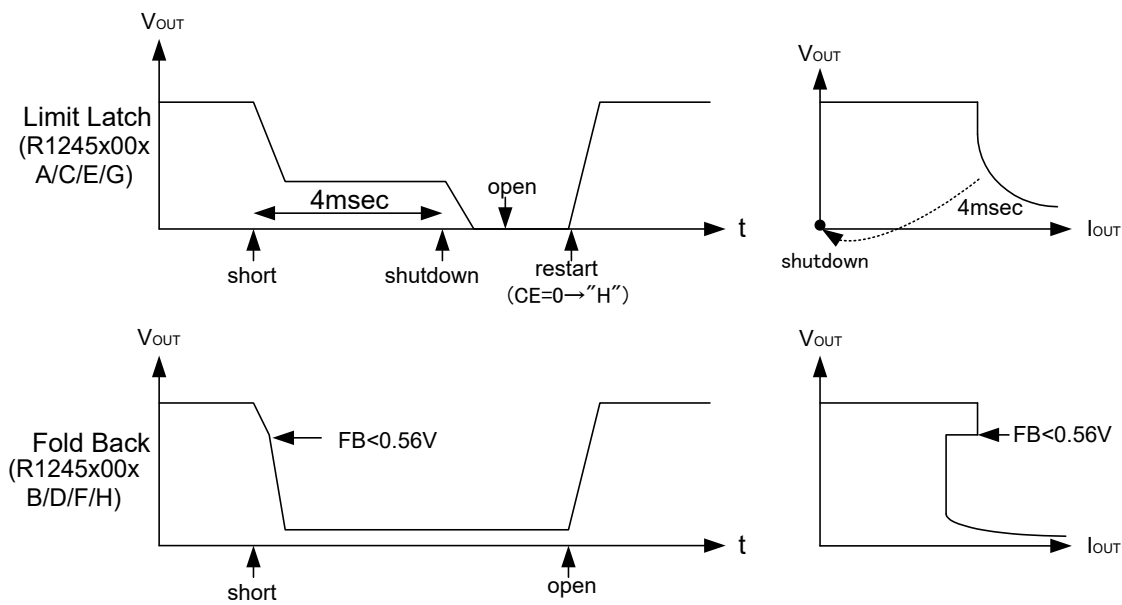
$$I_{OUT} < I_{RP} / 2 \dots\dots\dots \text{Equation 7}$$

Consider I_{Lmax} and I_{Lmin} , conditions of input and output and select external components.

Ripple Current and Lx current limit

The ripple current of the inductor may change according to the various reasons. In the R1245x, as an Lx current limit, Lx peak current limit is used. Therefore the upper limit of the inductor current is fixed.

The peak current limit is not the average current of the inductor (output current). If the ripple current is large, peak current becomes also large. The characteristic is used for the fold-back current limit of version B/D/F/H. In other words, the peak current limit is maintained and the switching frequency is reduced, as a result, the average current of the inductor is reduced. To release this condition, at 170 kHz for version B/D, at 250 kHz for version F, at 400 kHz for version H must not be beyond the peak current limit. In the Figure 1, the sequence of the Lx current limit function is described.

**Figure 1. Lx Limit Function Sequence**

Latch protection function for version A/C/E/G

The latch function works after detecting current limit and if the output voltage becomes low for a certain time, the output is latched off. Refer to the *TECHNICAL NOTES*.

Fold-back protection function for version B/D/F/H

If FB voltage becomes lower than approximately 0.56 V, the fold-back protection function limits the oscillator frequency to typically 170 kHz for version B/D, typically 250 kHz for version F, typically 400 kHz for version H. By reducing frequency, the ripple current increases. The R1245x has the peak current limit function, therefore as in the Equation 8, the Lx average current decreases by the increase of the ripple current.

$$I_{OUT} = I_{Lmax} + I_{RP} / 2 \dots\dots\dots \text{Equation 8}$$

If FB voltage becomes less than 0.56 V, the oscillator frequency is reduced. At heavy load, if the R1245x becomes into the fold-back protection mode, the situation may not be released by increase the ripple current. In terms of other notes on this protection function, refer to the *TECHNICAL NOTES*.

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MAXIMUM OUTPUT CURRENT

The output current of the R1245x is limited by the power dissipation P_D of the package and the maximum specification 1.2 A. The loss of the IC includes the switching loss, and it is difficult to estimate. To estimate the maximum output, using the efficiency data is one method.

By using the efficiency data, the loss including the external components can be calculated with the equation, $(100/\text{efficiency}(\%) - 1) \times (V_{OUT}(\text{V}) \times I_{OUT}(\text{A}))$. From this equation, by reducing the loss of external components, the loss of the IC can be estimated. The main loss of the external components is composed by the rectifier diode and DCR of the inductor. Supposed that the forward voltage of the diode is described as V_F , the loss of the diode can be described as follows:

$$(V_{IN}(\text{V}) - R_{ON}(\Omega) \times I_{OUT}(\text{A}) - V_{OUT}(\text{V}) - V_F(\text{V})) / V_{IN}(\text{V}) \times V_F(\text{V}) \times I_{OUT}(\text{A})$$

The loss by the DCR of the inductor can be calculated by the formula $DCR(\Omega) \times I_{OUT}^2(\text{A})$.

Thus,

$$\text{The loss of the IC} = (100 / \text{efficiency}(\%) - 1) \times (V_{OUT}(\text{V}) \times I_{OUT}(\text{A}) - (V_{IN}(\text{V}) - R_{ON}(\Omega) \times I_{OUT}(\text{A}) - V_{OUT}(\text{V}) - V_F(\text{V})) / V_{IN}(\text{V}) \times V_F(\text{V}) \times I_{OUT}(\text{A}) - DCR(\Omega) \times I_{OUT}^2(\text{A}))$$

The efficiency of the R1245x at $T_a = 25^\circ\text{C}$, $V_{IN} = 12\text{ V}$, $V_{OUT} = 3.3\text{ V}$, $I_{OUT} = 600\text{ mA}$ is approximately 89.5% for version A/B (Oscillator frequency 330 kHz). Supposed that the On resistance of the internal driver is $0.35\ \Omega$, the DCR of the inductor is $65\text{ m}\Omega$, the V_F of the rectifier diode is 0.3 V and applied to the formula above, The loss of the IC = $(100\% / 89.5\% - 1) \times (3.3\text{ V} \times 0.6\text{ A}) - (12\text{ V} - 0.35\ \Omega \times 0.6\text{ A} - 3.3\text{ V} - 0.3\text{ V}) / 12\text{ V} \times 0.3\text{ V} \times 0.6\text{ A} - 0.065\ \Omega \times 0.6^2\text{ A} = 86\text{ mW}$

The power dissipation P_D of the package is specified at $T_a = 25^\circ\text{C}$ based on the $T_{jmax} = 150^\circ\text{C}$. Thus the thermal resistance of the package $\theta_{ja} = (T_{jmax}(\text{ }^\circ\text{C}) - T_a(\text{ }^\circ\text{C})) / P_D(\text{ W})$, therefore the thermal resistance of the each available package is as follows:

$$\text{HSOP-8E: } (150^\circ\text{C} - 25^\circ\text{C}) / 3.6\text{ W} = 35^\circ\text{C/W}$$

$$\text{DFN2020-8: } (150^\circ\text{C} - 25^\circ\text{C}) / 1.1\text{ W} = 114^\circ\text{C/W}$$

Due to the loss of the IC is 86 mW for this example, therefore T_j increase of the each package is as follows:

$$\text{HSOP-8E: } 35^\circ\text{C/W} \times 86\text{ mW} = 3.01^\circ\text{C}$$

$$\text{DFN2020-8: } 114^\circ\text{C/W} \times 86\text{ mW} = 9.80^\circ\text{C}$$

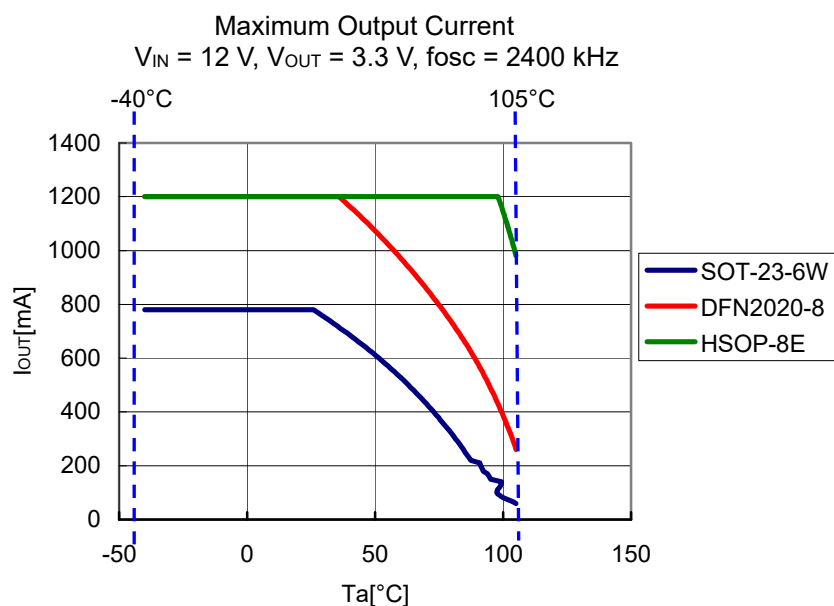
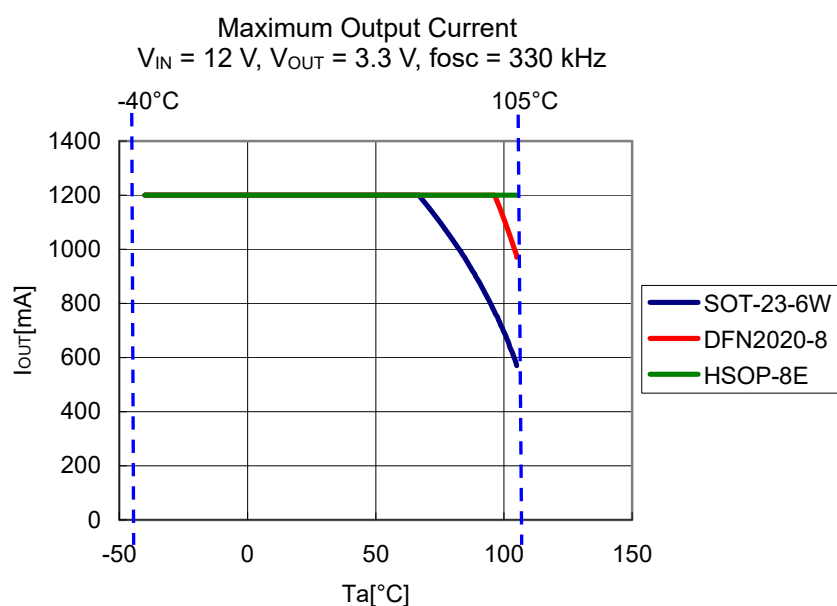
For all the packages, even if the ambient temperature is at 105°C , T_j can be suppressed less than 150°C . By the increase of the temperature, on resistance and switching loss increases, therefore, temperature margin is not enough, measure the efficiency at the actual maximum temperature and recalculation is necessary.

At the same condition, if the preset frequency is 2400 kHz, the efficiency will be down to approximately 81%. The result of the loss calculation is 310 mW, therefore the T_j increase of each package is as follows:

$$\text{HSOP-8E: } 35^\circ\text{C/W} \times 310\text{ mW} = 10.85^\circ\text{C}$$

$$\text{DFN2020-8: } 114^\circ\text{C/W} \times 310\text{ mW} = 35.34^\circ\text{C}$$

All packages can be used at the ambient temperature 105°C. However as for DFN2020-8 package, be sure to note the power dissipation when using at 2400 kHz since its temperature margin is not sufficient when $T_{jmax} = 150^{\circ}\text{C}$. The following graphs are the output current and estimated ambient temperature limit.



SHUTDOWN BY INPUT VOLTAGE CONTROL

If the set output voltage is more than UVLO detector threshold (Typ. 3.8 V) and on/off control is made by V_{IN} voltage-e.g. in the case of V_{IN} pin and CE pin are connected -, when the circuit is shutdown, the relation between input and output may be beyond the specified maximum duty cycle. If the ratio of input and output is beyond the maximum duty cycle, switching operation stops and the output voltage goes down, but depending on the V_{IN} decreasing speed, the ratio of V_{IN} and V_{OUT} could become equal or less than the maximum duty cycle, as a result, the output may be resumed and fluctuate. Further, if the input voltage goes down faster than the output voltage as shown in Figure 2, large reverse current may flow. In order to avoid the conditions above, or to maintain the input voltage being larger than the output voltage in the power off process, set CE signal "L" while the input voltage is enough larger than the output voltage, or add a discharge circuit.

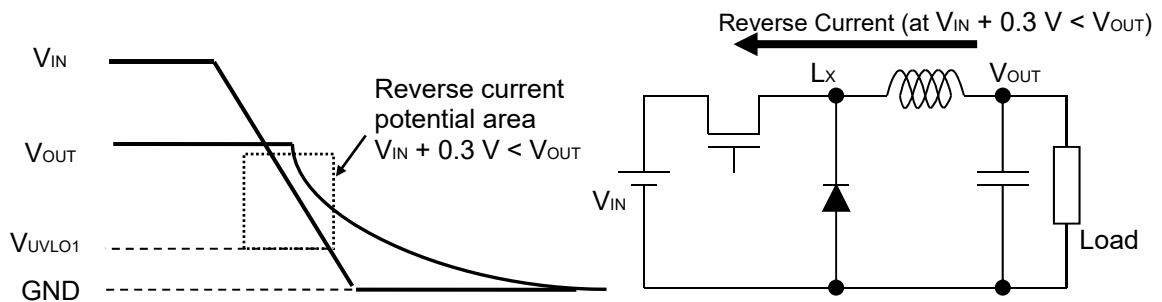


Figure 2. Conditions for Reverse Current Generation at Shutdown by Input Voltage Control

TECHNICAL NOTES

- External components must be connected as close as possible to the ICs and make wiring as short as possible. Especially, the capacitor connected in between V_{IN} pin and GND must be wiring the shortest. If their impedance is high, internal voltage of the IC may shift by the switching current, and the operating may be unstable. Make the power supply and GND lines sufficient. In the wiring of the power supply, GND, L_x , V_{OUT} and the inductor, large current by switching may flow. To avoid the bad influence, the wiring between the resistance, “ R_{UP} ” for setting the output voltage and loading, and the wiring between the inductor and loading must be separated.
- The ceramic capacitors have low ESR (Equivalent Series Resistance) and recommended for the ICs. The recommendation of C_{IN} capacitor between V_{IN} and GND is 10 μ F or more for A/B/C/D version, 4.7 μ F or more for E/F version, and 2.2 μ F or more for G/H version. Verify the bias dependence and the temperature characteristics of the ceramic capacitors. Recommendation conditions are written based on the case which the recommendation parts are used with the R1245x.
- The R1245x is designed with the recommendation inductance value and ceramic capacitor value and phase compensation has been made. If the inductance value is large, due to the lack of current sensing amount of the current mode, unstable operation may result. On the contrary, if the inductance value is small, the current sensing amount may increase too much, low frequency oscillation may occur when the on duty ratio is beyond 50%. Not only that, if the inductance value is small, according to the increase of the load current, the peak current of the switching may increase, as a result, the current may reach the current limit value and the current limit may work.
- As for the diode, use the Schottky diode with small capacitance between terminals. The reference characteristic of the capacitance between terminals is around 100 pF or less at 10 V. If the capacitance between terminals is large, excess switching current may flow and the operation of the IC may be unstable. If the capacitance between terminals of the Schottky diode is beyond 100 pF at 10 V or unknown, verify the load regulation, line regulation, and the load transient response.
- Output voltage can be set by adjustment of the values of R1 and R2. The equation of setting the output voltage is $V_{OUT} = V_{FB} \times (R1 + R2)/R2$. If the values of R1 and R2 are large, the impedance of FB pin increases, and pickup the noise may result. The recommendation value range of R2 is approximately between 1.0 k Ω to 16 k Ω . If the operation may be unstable, reduce the impedance of FB pin.
- For the CE pin, as an ESD protection element, a diode to V_{IN} pin is formed internal of the IC. If CE pin voltage may become higher than V_{IN} pin voltage, to prevent flowing large current from CE pin to V_{IN} pin, connect 10 k Ω or more resistor between CE and V_{IN} pin.
- Connect the backside heat radiation tab to the GND. As for multi-layered boards, to make better power dissipation, putting some thermal vias on the thermal tab in the land pattern and radiation of the heat to another layer is effective.
- After the soft-start operation, the latch function is enabled for version A/C/E/G. The latch protection starts the internal counter when the internal current limit protection circuit detects the current limit. When the internal counter counts up to the latch timer limit, typically 4 ms, the output is latched off. To reset the latch function, make the CE pin “L”, or make V_{IN} pin voltage lower than UVLO detector threshold. Then in the case that the output voltage or FB voltage becomes setting voltage within the latch timer preset time, counter is initialized. If the slew rate of the power supply is too slow and after the soft-start time, the output voltage does not reach the set output voltage even if the latch timer preset time is over, the latch function may work unexpectedly.

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- After the soft-start operation, fold-back protection function is enabled for version B/D/F/H. The fold-back function will limit the oscillator frequency if the FB pin voltage becomes lower than typically 0.56 V. For B/D version, the oscillator frequency will be reduced typically into 170 kHz, for F version, into 250 kHz, for H version, into 400 kHz.
- If the slew rate of the power supply is too slow, and even after the soft-start time, the output voltage is still less than 70% of the set output voltage, or FB pin voltage is less than typically 0.56 V, then this function may work unexpectedly.
- The performance of power circuit using this IC largely depends on external components. Selection of external components is very important, especially, do not exceed each rating value (voltage/current/power).

Recommended Values for Each Output Voltage

R1245x003A/B: 330 kHz

V _{OUT} (V)	0.8 to 1.2	1.2 to 2.5	2.5 to 5.0	5.0 ≤
R1 (R _{UP}) (kΩ)	= (V _{OUT} / 0.8-1) × R2			
R2 (R _{BOT}) (kΩ)	16	12	1.20	1.20
C _{SPD} (pF)	open	470	2200	1000
C _{OUT} (μF)	47	47	22	22
L (μH)	4.7	10	15	33

R1245x00xC/D: 500 kHz

V _{OUT} (V)	0.8 to 1.2	1.2 to 1.5	1.5 to 2.0	2.0 to 5.0	5.0 to 12.0	12.0 ≤
R1 (R _{UP}) (kΩ)	= (V _{OUT} / 0.8-1) × R2					
R2 (R _{BOT}) (kΩ)	16	16	16	1.2	1.2	1.2
C _{SPD} (pF)	open	100	100	1000	1000	470
C _{OUT} (μF)	100	100	22	22	22	22
L (μH)	4.7	4.7	10	10	15	15

R1245x00xE/F: 1000 kHz

V _{OUT} (V)	0.8 to 1.0	1.0 to 1.2	1.2 to 1.5	1.5 to 2.5	2.5 to 5.0	5.0 ≤
R1 (R _{UP}) (kΩ)	= (V _{OUT} / 0.8-1) × R2					
R2 (R _{BOT}) (kΩ)	16	16	16	16	1.2	1.2
C _{SPD} (pF)	open	100	100	100	470	470
C _{OUT} (μF)	100	100	47	22	10	10
L (μH)	2.2	2.2	2.2	2.2	4.7	10

R1245x003G/H: 2400 kHz

V _{OUT} (V)	1.5 to 1.8	1.8 to 2.5	2.5 to 5.0	5.0 ≤
R1 (R _{UP}) (kΩ)	= (V _{OUT} / 0.8-1) × R2			
R2 (R _{BOT}) (kΩ)	16	12	1.2	1.2
C _{SPD} (pF)	100	100	470	470
C _{OUT} (μF)	10	10	4.7	4.7
L (μH)	1.0	1.5	2.2	4.7

Divider Resistors Values and Possible Setting Range of Input /Output

V _{OUT} [V]	R1 (R _{UP}) [kΩ]	R2 (R _{BOT}) [kΩ]	Input Voltage Range [V]			
			Ver. AB	Ver. CD	Ver. EF	Ver. GH
0.8	0	open	4.5 to 20	4.5 to 13.5	4.5 to 7	-
	0	16				
1	4	16	4.5 to 25.5	4.5 to 17	4.5 to 8.5	-
1.2	8	16	4.5 to 30	4.5 to 20	4.5 to 10	-
	6	12				
1.5	10.5	12	4.5 to 30	4.5 to 25	4.5 to 12.5	4.5 to 5.5
	14	16				
1.8	20	16	4.5 to 30	4.5 to 30	4.5 to 15	4.5 to 6.5
	15	12				
2	24	16	4.5 to 30	4.5 to 30	4.5 to 17	4.5 to 7
	1.8	1.2				
2.5	34	16	4.5 to 30	4.5 to 30	4.5 to 21	4.5 to 9
	25.5	12				
	2.55	1.2				
3.3	3.75	1.2	4.5 to 30	4.5 to 30	4.5 to 27.5	4.5 to 12
5	6.3	1.2	5.5 to 30	5.5 to 30	6 to 30	7 to 18.5
6	7.8	1.2	6.5 to 30	6.5 to 30	7 to 30	8 to 20
9	12.3	1.2	10 to 30	10 to 30	11 to 30	12 to 30
12	16.8	1.2	13 to 30	13 to 30	14 to 30	16 to 30
15	21.3	1.2	16.5 to 30	16.5 to 30	17 to 30	20 to 30
24	34.8	1.2	26.5 to 30	26.5 to 30	27.5 to 30	30

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Recommended External Components Examples (Considering all the range)

Symbol	Condition	Value	Parts Name	MFR
C _{IN}	50 V/X5R	10 μ F	UMK325BJ106MM-P	TAIYO YUDEN
	50 V/ X5R	10 μ F	CGA6P3X7S1H106K	TDK
	50 V/X7R	4.7 μ F	GRM31CR71H475KA12L	muRata
	50 V/X7R	2.2 μ F	GRM31CR71H225KA88L	muRata
C _{OUT}	50 V/X5R	10 μ F	UMK325BJ106MM-P	TAIYO YUDEN
	50 V/ X5R	10 μ F	CGA6P3X7S1H106K	TDK
	50 V/X7R	10 μ F	KTS500B106M55N0T00	Nippon Chemi-Con
	50 V/X7R	4.7 μ F	GRM31CR71H475KA12L	muRata
	25 V/X7R	10 μ F	GRM31CR71E106K	muRata
	10 V/X7R	22 μ F	GRM31CR71A226M	muRata
	16 V/B	47 μ F	GRM32EB31C476KE15	muRata
	10 V/X7R	47 μ F	GRM32ER71A476KE15 NOTE: The value of C _{OUT} depends upon the set output voltage.	muRata
C _{BST}	16 V/X7R	0.47 μ F	EMK212B7474KD-T	TAIYO YUDEN
L	1.8 A	10 μ H	SLF6045T-100M1R6-3PF	TDK
	1.65 A	4.7 μ H	SLF7045T-4R7M2R0-PF	TDK
	1.7 A	4.7 μ H	NR4018T4R7M	TAIYO YUDEN
	2.4 A	4.7 μ H	NR6020T4R7N	TAIYO YUDEN
	1.9 A	10 μ H	NR6028T100M	TAIYO YUDEN
	2.3 A	15 μ H	NR6045T150M	TAIYO YUDEN
	1.9 A	22 μ H	NR6045T220M	TAIYO YUDEN
	1.9 A	33 μ H	NR8040T330M	TAIYO YUDEN
	1.7 A	2.2 μ H	VLCF4020T-2R2N1R7	TDK
	1.65 A	2.2 μ H	NR4012T2R2M	TAIYO YUDEN
	1.8 A	1.5 μ H	NR3015T1R5N	TAIYO YUDEN
	1.8 A	1.0 μ H	NR4010T1R0N	TAIYO YUDEN
Diode	30 V/2.0 A	0.37 V	CMS06	TOSHIBA
	40 V/2.0 A	0.55 V	CMS11	TOSHIBA
R _{CE}	The Up Diode is connected between the CE pin and the V _{IN} pin as the ESD protection element. If there is the possibility that the voltage of the CE pin becomes higher than the voltage of the V _{IN} pin, it is recommended to connect the 10 k Ω resistance with the CE pin for preventing a large current flows into the V _{IN} pin from the CE pin.			

APPLICATION INFORMATION

TO IMPROVE THE PERFORMANCE

The R1245 can make its performance better, adding components as shown below.

Cspd: Speed up capacitor

Cspd has two roles, one is to improve the stability, and the other is to improve the transient speed. The transfer function from V_{OUT} (-which is made of Cspd and feedback resistors, R1(Rup) and R2(Rbot)) to FB will make a forward bump by low frequency zero and high frequency pole, and improve the stability of feedback loop. Cspd can improve the gain and make the transient speed fast at high frequency.

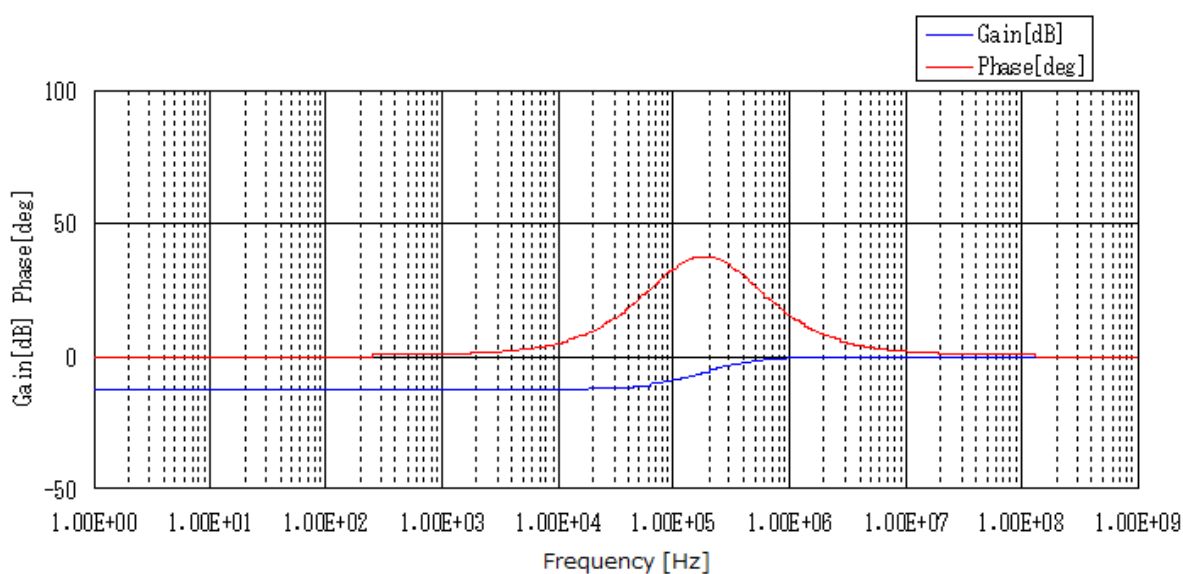


Figure 3. Transfer function BODE plot from V_{OUT} to FB (R1=3.75k Ω , R2=1.2k Ω , Cspd=470pF)

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To improve the stability

If the resistance values of the R1 and R2 have to be changed, make the value of $R1 \cdot C_{spd}$ be constant.

(For example, with the R1245x00xA/B and making $V_{OUT}=1.2V$, if $R1=0.6k\Omega$, $R2=1.2k\Omega$ are used, $C_{spd}=4700pF$. By making the values of R1 and R2 increase, the impedance of FB pin also increases, as a result, the influence by noise must be cared. To avoid this, recommendation value range of R2 is from 1.0k Ω to 16k Ω . If the operation becomes unstable by increasing the impedance, choose low resistance value.

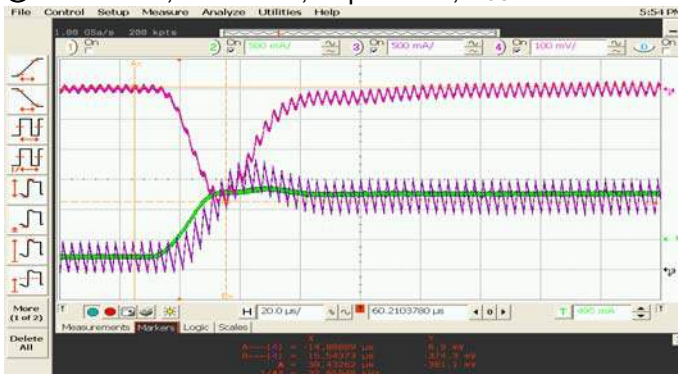
If C_{OUT} and L are necessary to be changed, or unusual voltage setting is necessary, the C_{spd} value must be adjusted. The instruction of the adjustment is as follows:

1. Without C_{spd} , measure the output under-shoot amount by load transient response.
2. Further, with using a small value C_{spd} , measure the output under-shoot amount by load transient response. The appropriate initial value is about 1/10 of the recommendation C_{spd} value. If C_{spd} is too small, the under-shoot amount is almost same as the one without C_{spd} . If the value of C_{spd} is changed bigger gradually, the under-shoot amount will be less. Supposed that this new good C_{spd} as C_{spd1} , and continue to make it bigger, and finally, the under-shoot amount becomes unchanged, at this point, supposed that the maximum C_{spd} as C_{spd2} .
3. Select an appropriate value according to the formula, $C_{spd}=\sqrt{C_{spd1} \cdot C_{spd2}}$.

To improve the transient response speed

If the stability is enough, (for example, in the case that C_{OUT} is big enough), make C_{spd} value bigger. The stability will be same, but the gain at high frequency will be large, and improve the transient response speed. However, if C_{spd} value is set C_{spd2} value or more, the result will not be improved, not only that, due to the high gain at high frequency, compared with the result without C_{spd} , the stability will be worse.

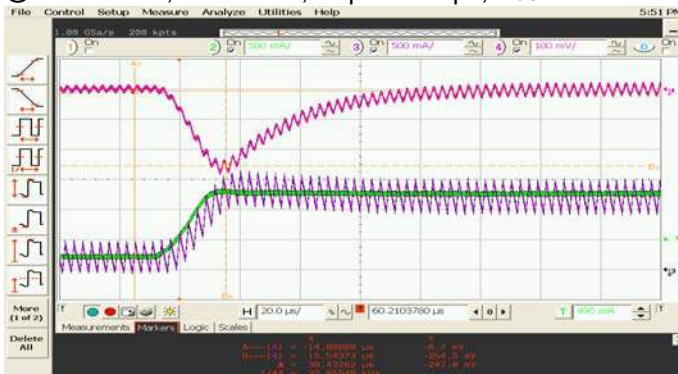
① $R_1=3.75k\Omega$, $R_2=1.2k\Omega$, Cspd: none, $V_{OUT}=3.3V$



Vout
ILx
Iout

Due to no Cspd, the stability is not good enough, and under-shoot amount is big during the load transient.

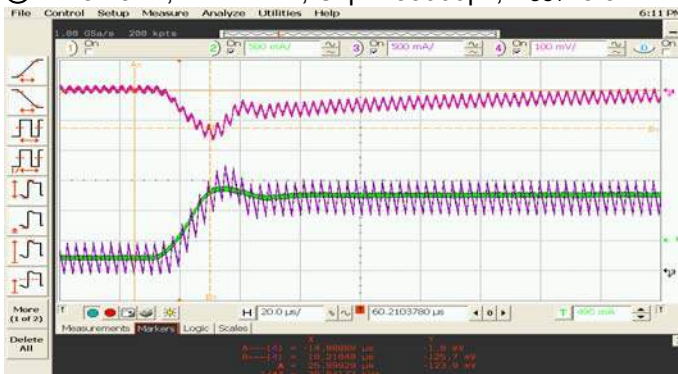
② $R_1=3.75k\Omega$, $R_2=1.2k\Omega$, Cspd=2200pF, $V_{OUT}=3.3V$



Vout
ILx
Iout

Cspd value is appropriate, and stability and response speed is adjusted properly.

③ $R_1=3.75k\Omega$, $R_2=1.2k\Omega$, Cspd=33000pF, $V_{OUT}=3.3V$



Vout
ILx
Iout

Cspd value is too big, the response speed is fast, but the stability decreases slightly.

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Rspd: Noise reduction filter for speed up capacitor

Cspd can improve the high frequency characteristics due to its differential function. In other words, the high frequency component is passed through without change, therefore the spike noise of V_{OUT} is transferred to FB pin as it is. If the spike noise is too big, by its noise of FB pin, the output voltage may be changed especially at heavy load. To avoid this situation, by setting an Rspd which inserts in series in Cspd and making a pole at high frequency, filtering is possible and effective. The appropriate value range of Rspd is from 10Ω to 30Ω . If the resistance value is too big, the effect of Cspd is cancelled by the lowering pole at high frequency by Rspd. By removing FB pin noise, using low R1 and R2 resistance value.

VOLTAGE BETWEEN Lx PIN AND BST PIN

In the boot-strap style switching regulator, when the Lx pin voltage becomes lower than the regulator which supplies BST voltage, C_{BST} is charged.

By this charge, while the Lx pin voltage is "H", high side switch can be turned on continuously. Therefore, if Lx pin voltage does not become lower than the BST voltage supply regulator, switching may be abnormal. In the R1245, the output voltage of the BST voltage supply regulator is set at 5V. The abnormal switching may be caused by the following conditions:

• **$V_{OUT} > 5V$, the difference between V_{IN} and V_{OUT} is small, inductor current is discontinuous by light load**

When the inductor current is continuous, or load current is big enough even if the discontinuous mode, the forward current of the diode will make Lx pin voltage down and C_{BST} is charged, but at light load, Lx pin voltage does not become low enough against the BST voltage supply regulator output(5V). The voltage of C_{BST} is not high enough and drive capability will be down. (Figure 4-①) Due to the lack of the drive capability, V_{OUT} cannot be maintained, and under-shoot happens to V_{OUT} , Lx pin voltage may become lower than the BST voltage supply regulator output (5V), but the error amplifier operation may be abnormal. When the charge of C_{BST} is recovered and normal switching starts, V_{OUT} becomes back to set output voltage. However, after recovering the V_{OUT} , to recover the error amplifier's operation, some response time is necessary, during this response time, V_{OUT} may be over-shoot. (Figure 4-②) As a result, Lx pin voltage cannot be low enough against the BST voltage supply regulator output voltage (5V), under-shoot and over-shoot may be repeated. (Figure 5)

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Abnormal waveforms are shown in the next figures. Figure 4: V_{IN} voltage start-up is slower than the soft-start time Figure 5: The voltage difference between input and output is small and load current is small
In both cases, the voltage between Lx pin and BST pin is not enough.

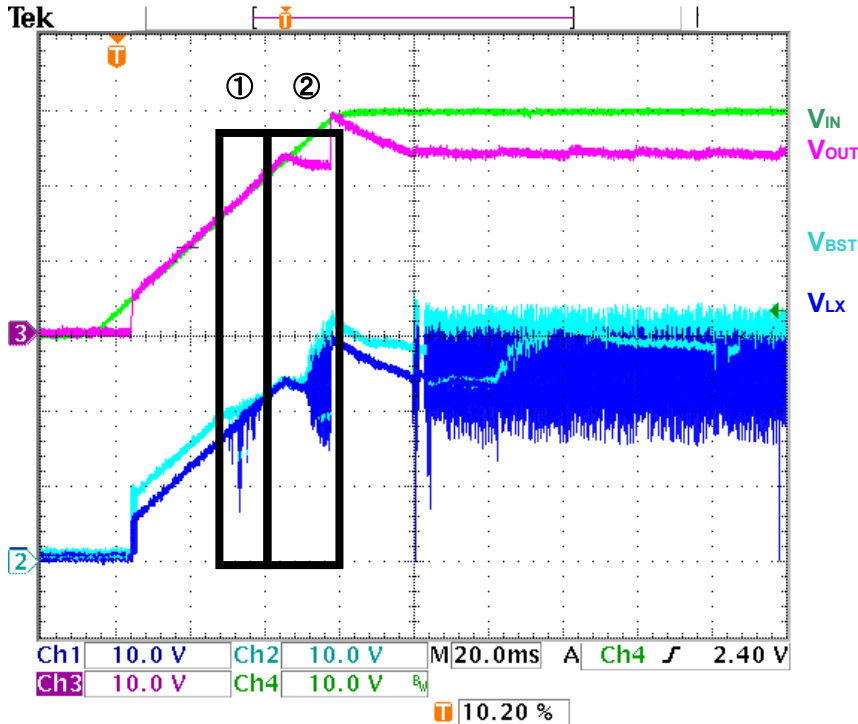


Figure 4. V_{IN} slow start-up (R1245S003A: $V_{IN}=30V$, $V_{OUT}=24V$, $I_{OUT}=0mA$)

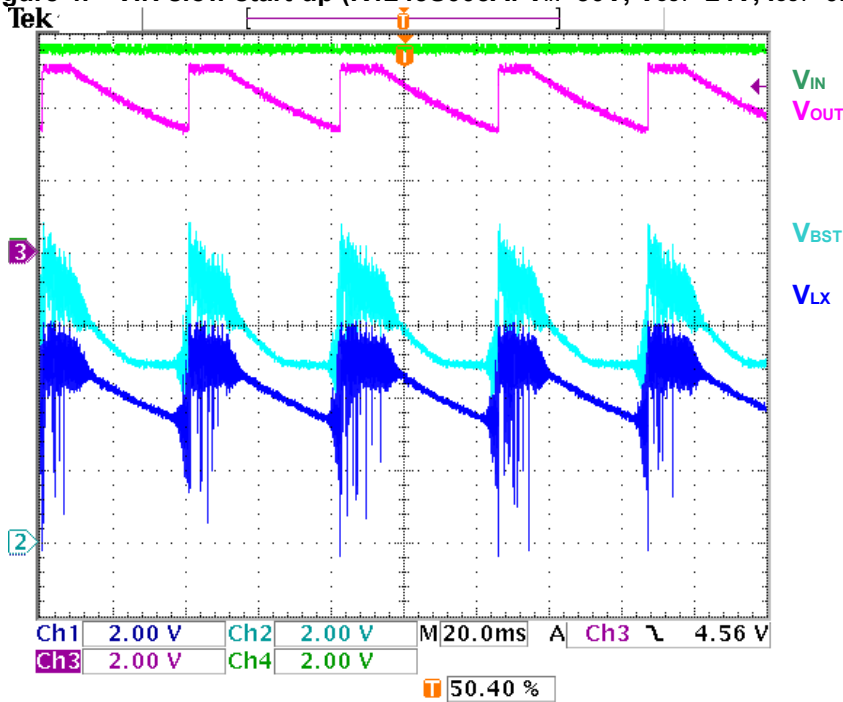


Figure 5. The voltage difference between input and output is small (R1245S003A $V_{IN}=5.5V$, $V_{OUT}=5V$, $I_{OUT}=500\mu A$)

To avoid these situations, please refer to the countermeasures shown below:

- If start-up with $V_{OUT}>5V$ is necessary, avoid the extremely low load, and start up should be done by CE pin control after V_{IN} becomes high enough.
- If $V_{OUT}>5V$ at low load operation is necessary, make the inductance value bigger and assure the "L" time of Lx .
- If start-up with $V_{IN}=CE$ is necessary, avoid very slow V_{IN} setting and low load current condition.

During the output overshoot while the normal transient response, even the no-switching condition happens, the operation keeps normal. Other than that, low load condition with $V_{OUT}<5V$ is also normal condition for the device.

MINIMUM ON TIME

The minimum On time of the R1245 is Typ.110ns. 110ns derives from the current sense circuit delay time and stability.

The R1245 has adopted current mode control without an external sense resistance. Instead of the external sense resistance, the on resistance of the N-channel driver: R_{ON} is used. $V_{IN}-V_{LX}=I_{LX}\times R_{ON}$, therefore I_{LX} (inductor current) can be sensed. I_{LX} can be sensed during the on time of the N-channel driver, ($L_x="H"$), if L_x switching surge is sensed just after turning on, the operation may be abnormal, therefore, just after turning on the N-channel driver, sensing is stopped for a short period and avoid the error by the switching surge.

Therefore, during this sensing delay time, current mode control and current limit cannot operate properly.

Figure 6. X-axis: On time, Y-axis: Current limit

By this current sense delay time, 110ns or less, current limit circuit has also delay time, and detecting current increases drastically. This delay time includes the signal delay time from the current sense circuit to the driver.

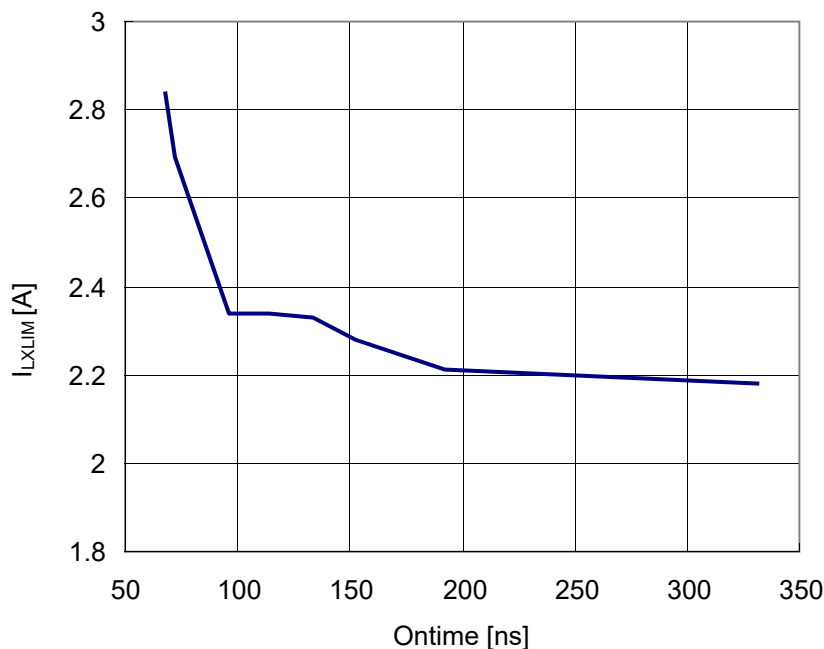


Figure 6. On time and Lx current limit, Lx pin current peak value I_{LXLIM}

This could be applied to the current mode control. Therefore, 110ns or less, current mode control does not work correctly, and operation becomes like a low stability voltage control mode.

Thus, if the condition of switching on time of the R1245 becomes less than 110ns, stability and current limit detecting accuracy are deteriorated. The higher the switching frequency and the input voltage, the higher current limit detecting threshold is and output and GND short must be cared. Under such conditions, the stability must be assured by the external components, and over current protection other than the IC is necessary. (ex. Using a fuse with the IC.)

INPUT VOLTAGE TRANSIENT

In the R1245, if the voltage between input and output is small and max. duty condition, or if the input voltage changes from lower than the set output voltage to high voltage rapidly, depending on the setting frequency of the R1245, output voltage may be over-shoot to input voltage.

Figure 7: Output response of the input voltage from 5V to 15V rapidly. External voltages: General recommendation values on datasheet, load 20Ω resistance, or 250mA load current.

In the high switching frequency type, the response speed is excellent, therefore, input transient characteristic is good, and over-shoot is suppressed. If input voltage rapid change must be considered, choose the high frequency type.

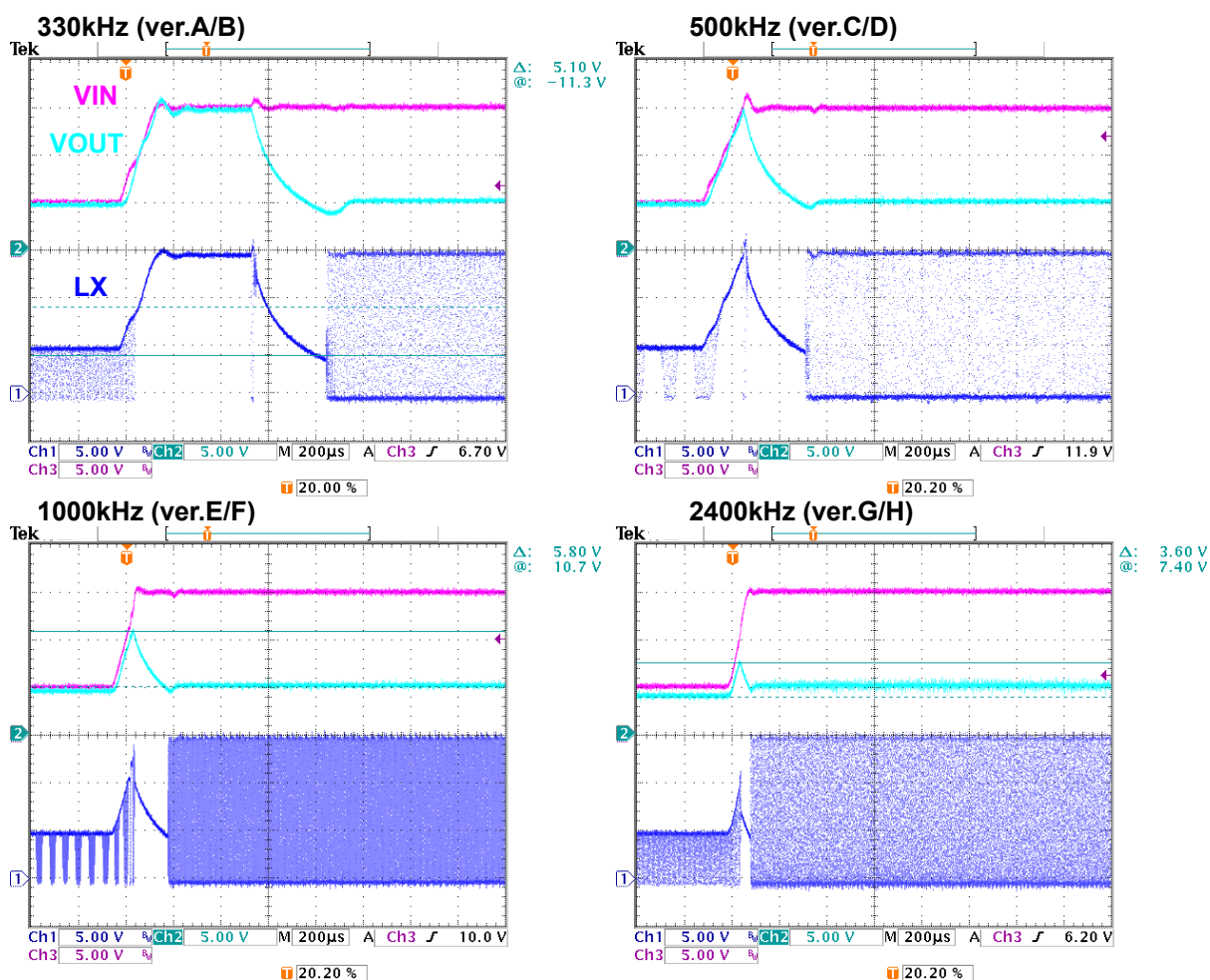


Figure 7. Input transient response from low difference voltage between input and output to high voltage

If the difference between input and output is large, then over-shoot will not happen. In the Figure 8, Other than the start VIN, the conditions are same as Figure 7. VIN is changed from 8V to 18V, 330kHz type, input transient response. Frequency is the lowest, but there is no over-shoot.

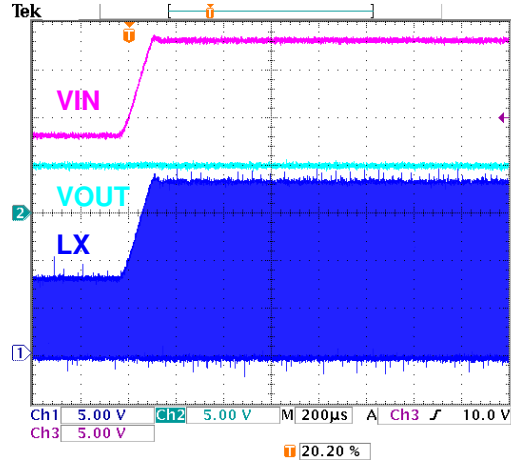


Figure 8. Input transient response from the big difference between input and output

To improve the situation shown in Figure 7, as shown in Figure 9, by using a zener diode, ZD and resistance, when the VIN decreases, CE pin is set at "L" and make the IC standby, over-shoot will be suppressed. Because, when the VIN goes up again and IC becomes active, soft-start function will work. If the input voltage, VIN goes down, Before the set output voltage V_{SET} against VIN ratio, (V_{SET}/VIN) becomes more than the max. duty, CE voltage must be "L". Consider this ratio and choose ZD voltage, or under the ZD, the voltage made by divider resistors must be forced to CE.

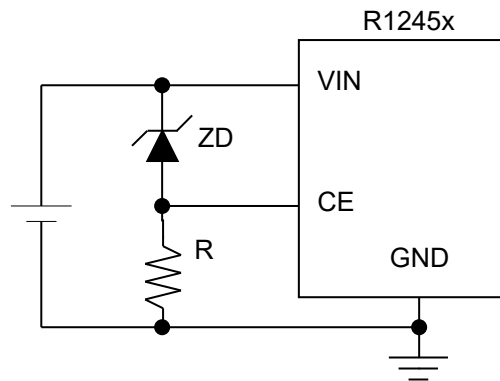


Figure 9. Low input voltage countermeasure circuit with using ZD

THE NOTE OF LAYOUT PATTERN

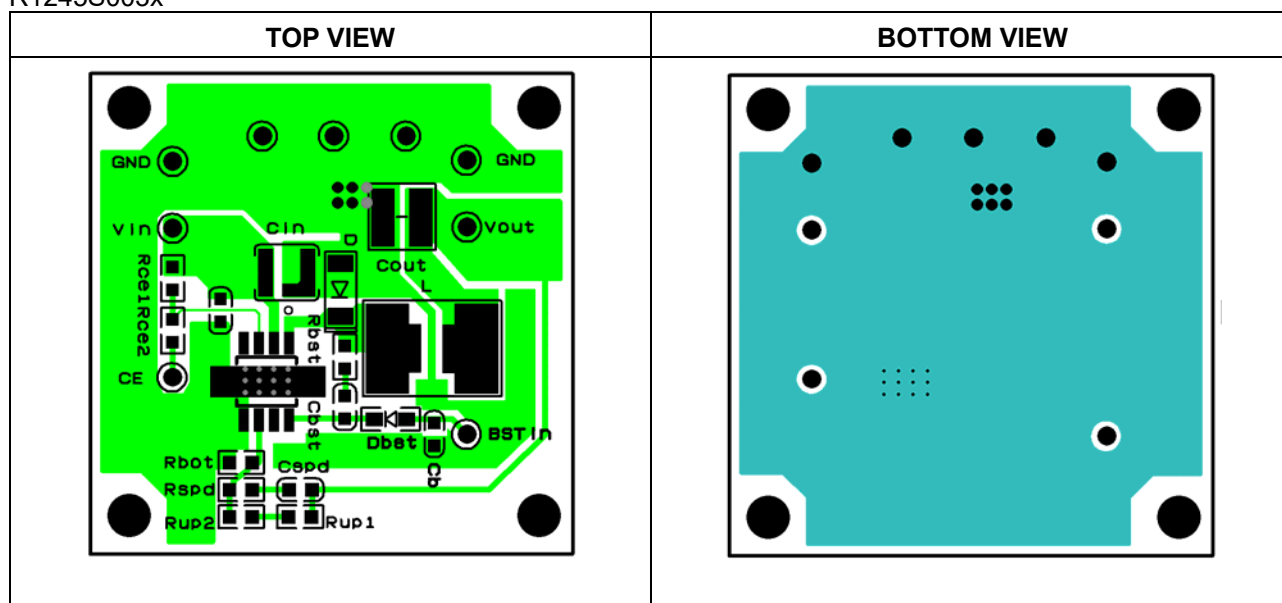
1. The wire of Power line (V_{IN} , GND) should be broad to minimize the parasitic inductance. The Bypass capacitor (C_{IN}) must be connected as close as possible in between $V_{IN} - GND$.
2. The wire between Lx pin and the inductor as short as possible to minimize the parasitic inductance.

This evaluation board is designed for the product evaluation board. Therefore large inductors or diodes can be set and the large space of Lx area has been secured. The evaluation board, R1245L003x (2400 kHz) with the reduced mounting area including external components, is available due to the small package of R1245L003G/H and the low recommended constant numbers including inductors.

3. The ripple current flows through the output capacitor. If the GND side of the output capacitor is connected very close to GND pin of the IC, the noise might have a bad impact on the IC. Therefore, the GND side of the output capacitor is better to connect to the outside of the GND of the C_{IN} , or connect to the GND plain layer.
4. R_{up} , R_{bot} , C_{spd} , and R_{spd} should be mounted on the position as close as possible to the FB pin, and away from the inductor and BST pin.
5. The feed-back must be made as close as possible from the Output capacitor (C_{OUT}).

PCB LAYOUT

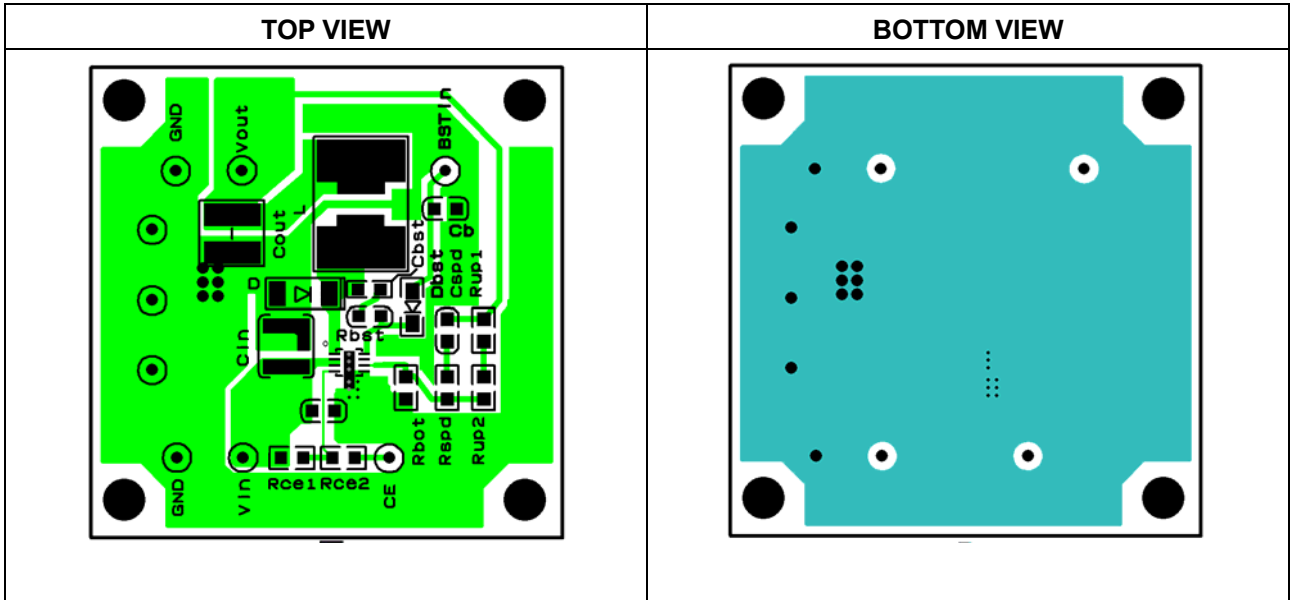
R1245S003x



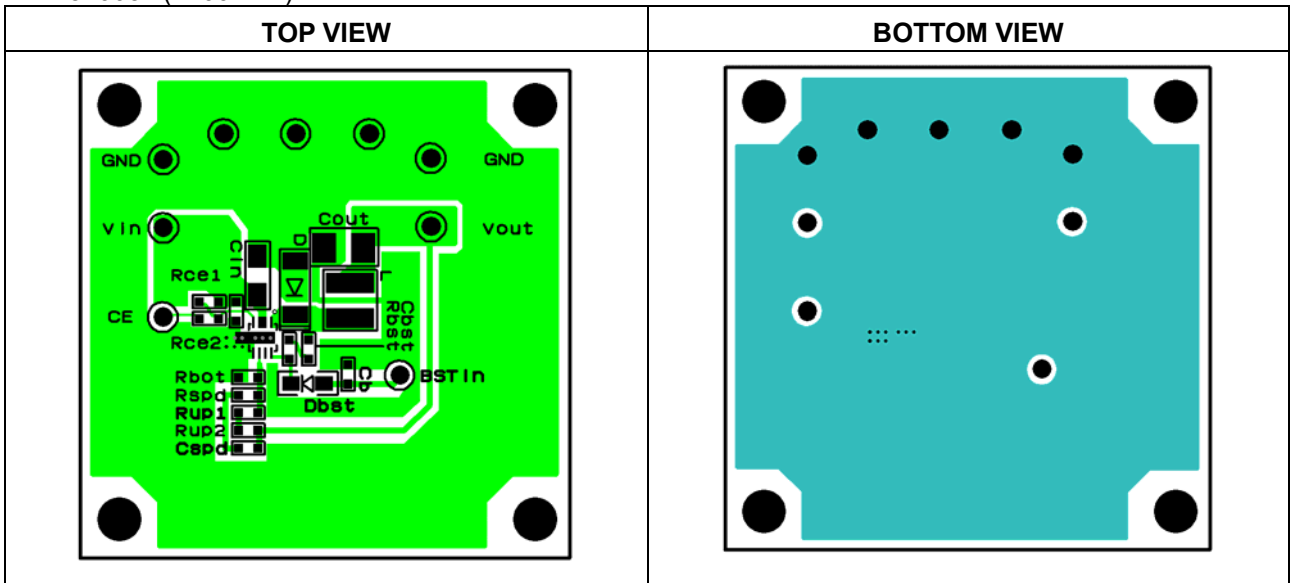
R1245x

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R1245L003x



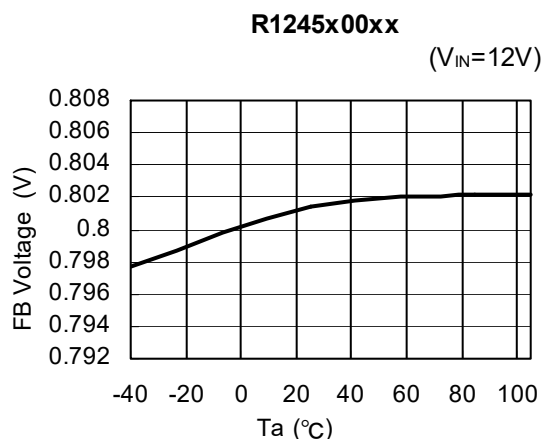
R1245L003x (2400 kHz)



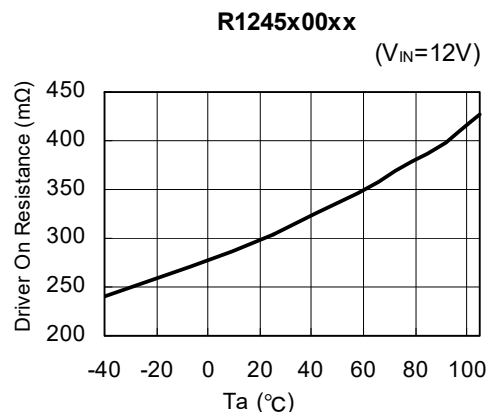
TYPICAL CHARACTERISTICS

Note: Typical Characteristics are intended to be used as reference data; they are not guaranteed.

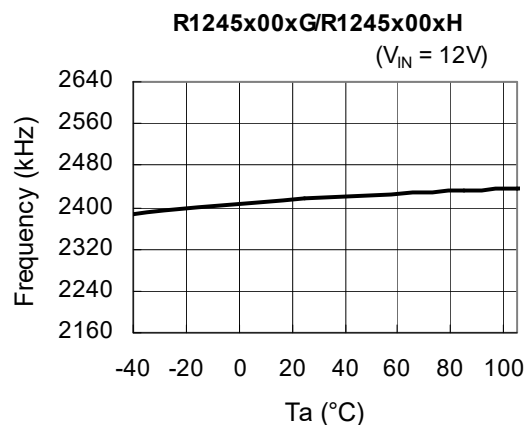
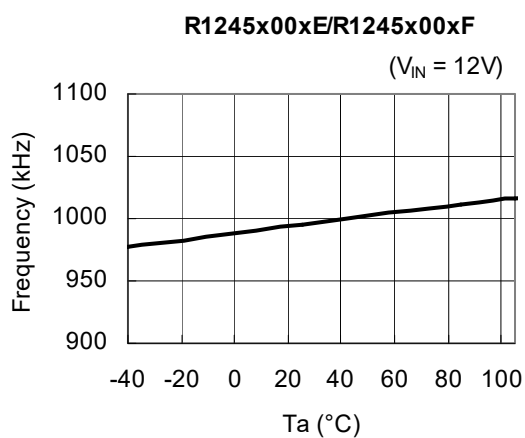
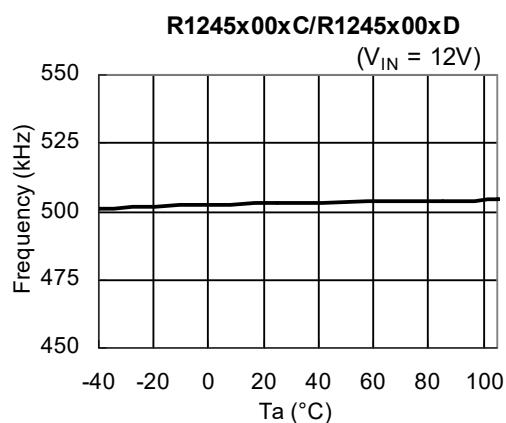
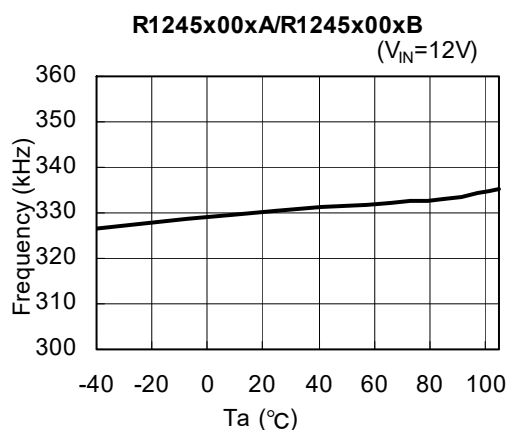
1) FB voltage vs. Temperature



2) Driver On resistance vs. Temperature



3) Oscillator frequency vs. Temperature

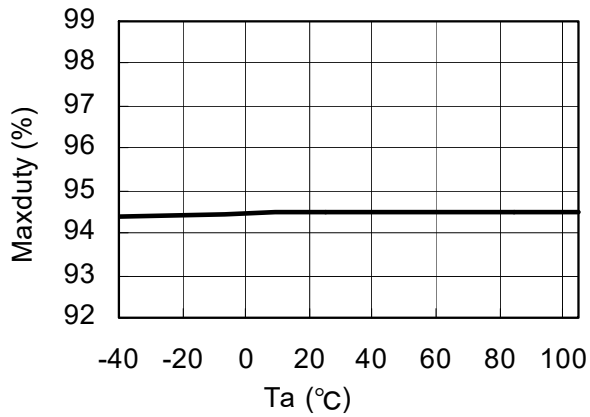


R1245x

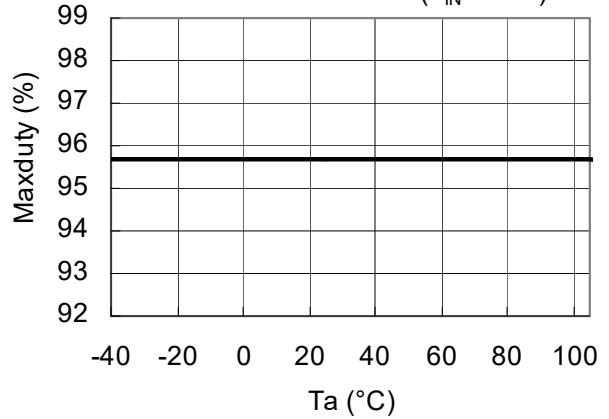
No. EC-269-201022

4) Maximum duty cycle vs. Temperature

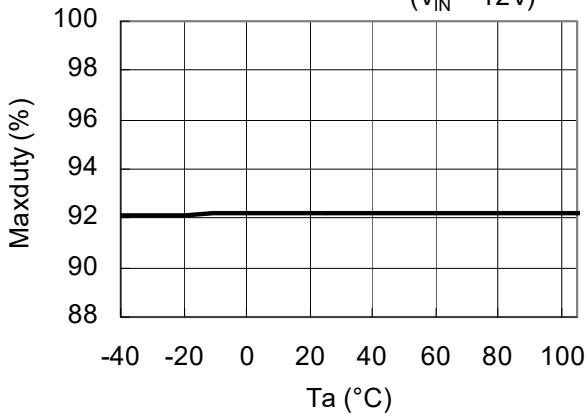
R1245x00xA/R1245x00xB
($V_{IN}=12V$)



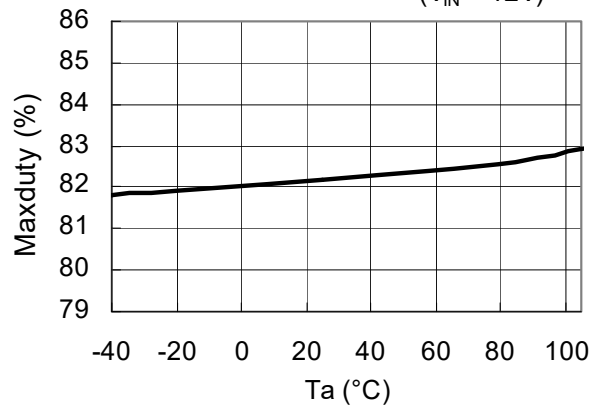
R1245x00xC/R1245x00xD
($V_{IN} = 12V$)



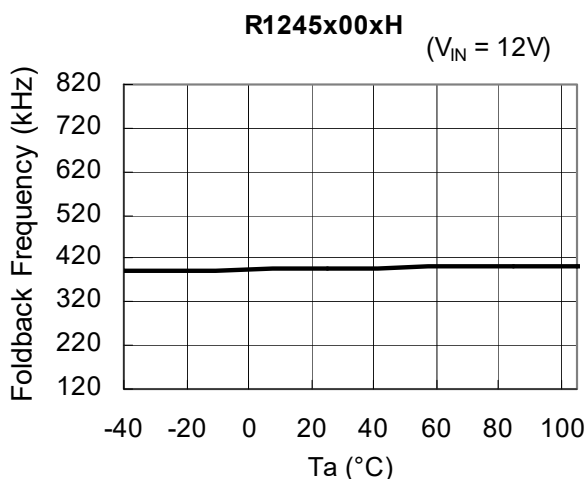
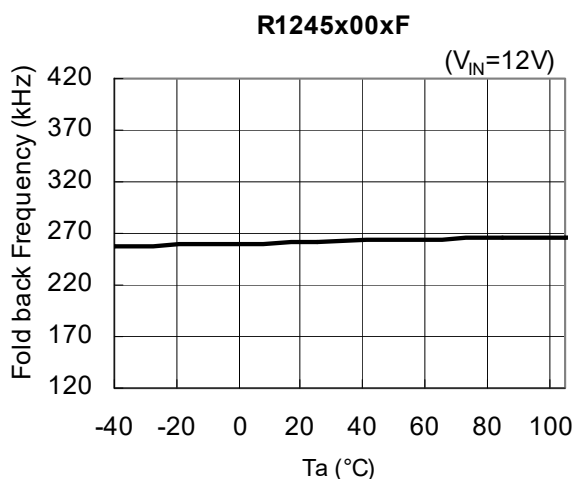
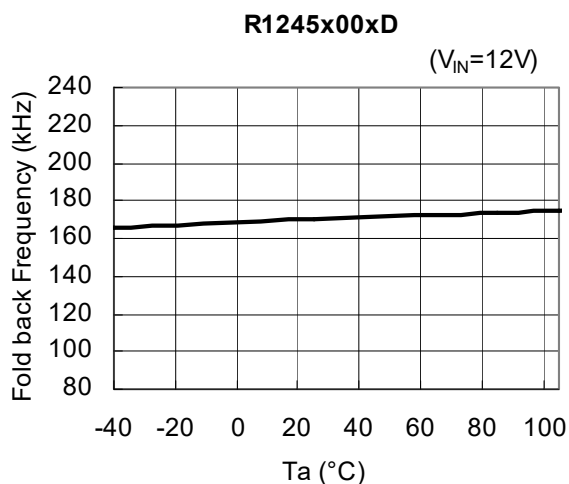
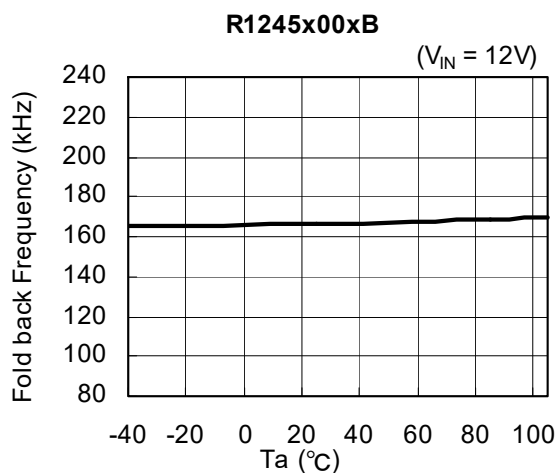
R1245x00xE/R1245x00xF
($V_{IN} = 12V$)



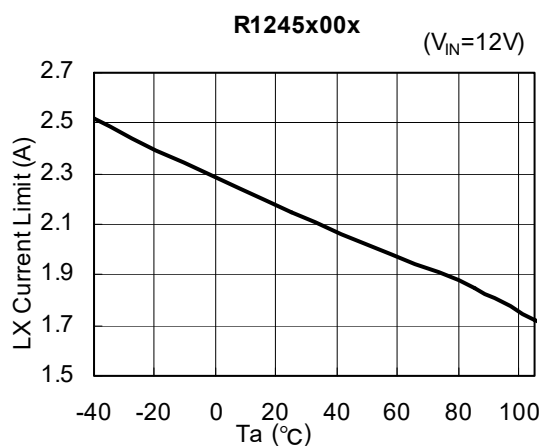
R1245x00xG/R1245x00xH
($V_{IN} = 12V$)



5) Fold-back frequency vs. Temperature

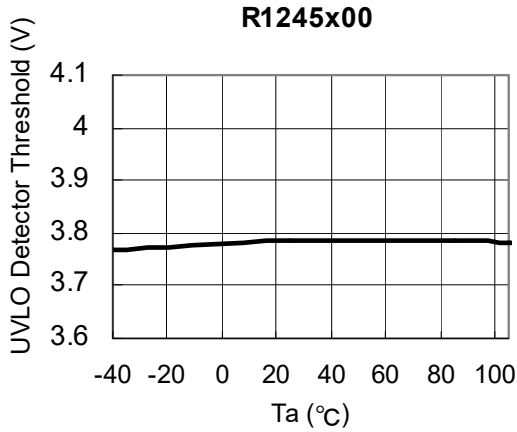
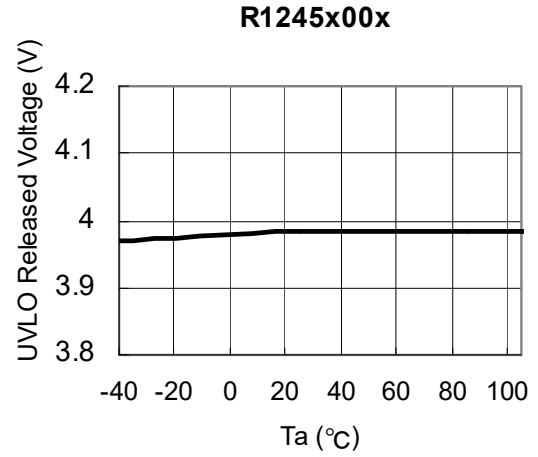
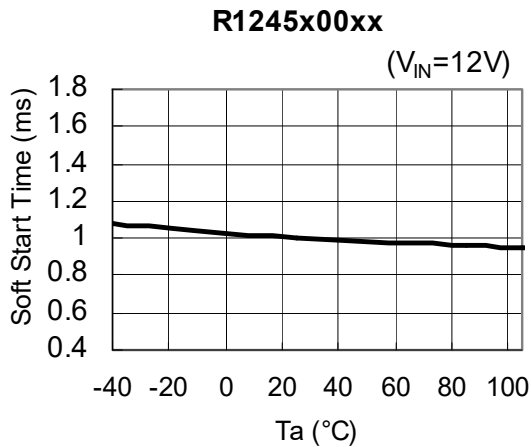
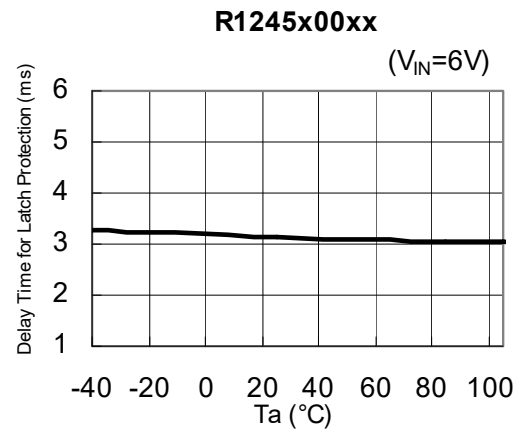
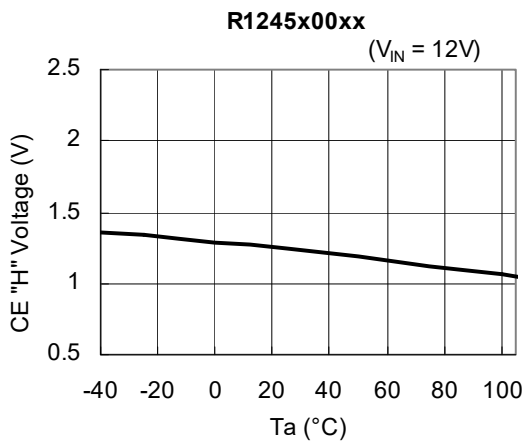
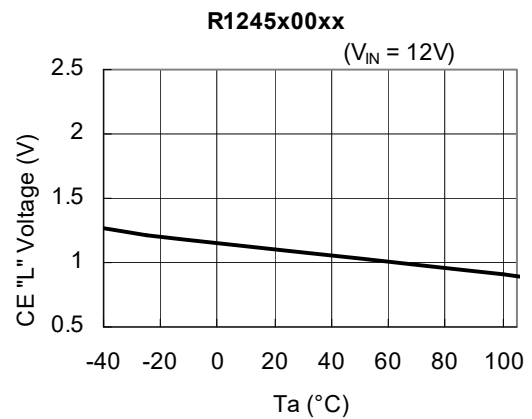


6) High side switch current limit vs. Temperature



R1245x

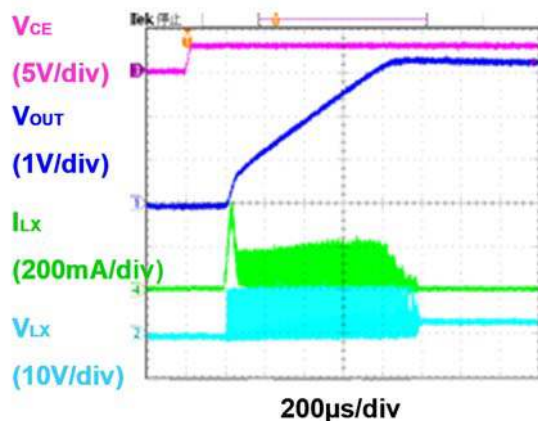
No. EC-269-201022

7) UVLO detector threshold vs. Temperature**8) UVLO released voltage vs. Temperature****9) Soft-start time vs. Temperature****10) Timer latch delay vs. Temperature****11) CE "H" Input voltage vs. Temperature****12) CE "L" Input voltage vs. Temperature**

13) Soft-start waveform

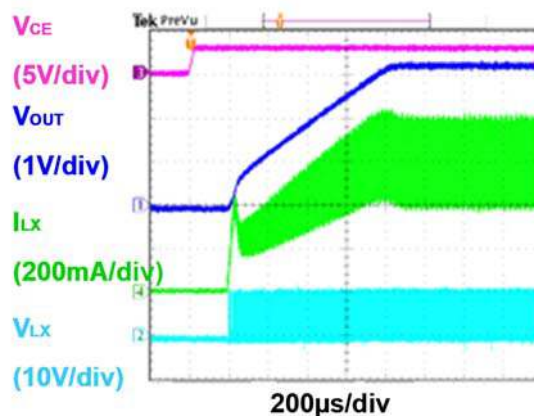
R1245x00xA/R1245x00xB

$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 0\text{ mA}$, $T_a = 25^\circ\text{C}$



R1245x00xA/R1245x00xB

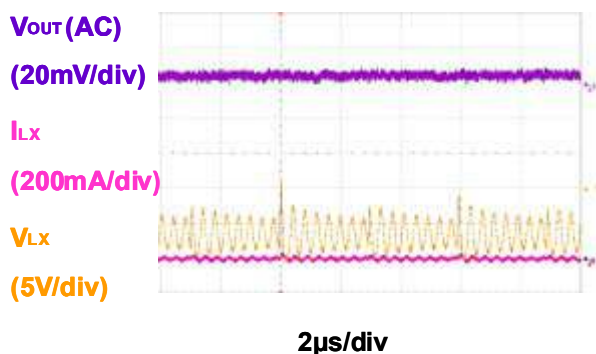
$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600\text{ mA}$, $T_a = 25^\circ\text{C}$



14) Switching operation waveform

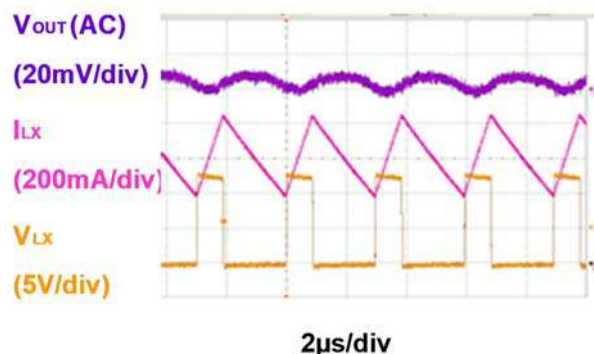
R1245x00xA/R1245x00xB

$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 0\text{ mA}$, $T_a = 25^\circ\text{C}$



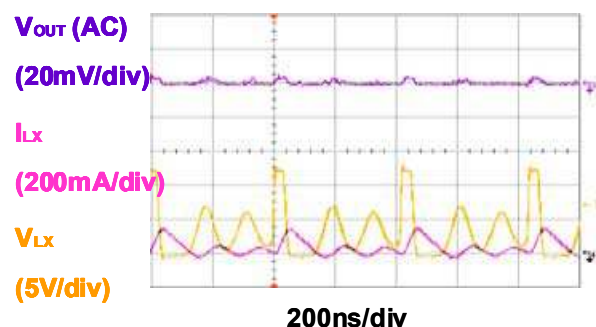
R1245x00xA/R1245x00xB

$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600\text{ mA}$, $T_a = 25^\circ\text{C}$



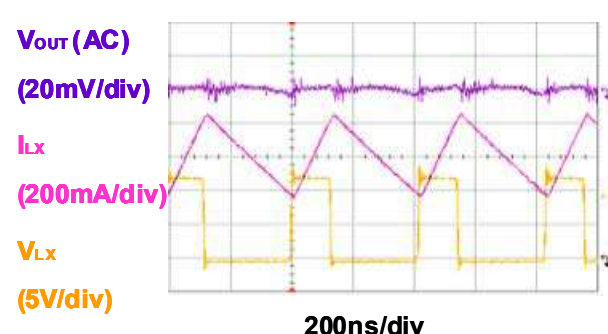
R1245x00xG/R1245x00xH

$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 20\text{ mA}$, $T_a = 25^\circ\text{C}$



R1245x00xG/R1245x00xH

$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600\text{ mA}$, $T_a = 25^\circ\text{C}$



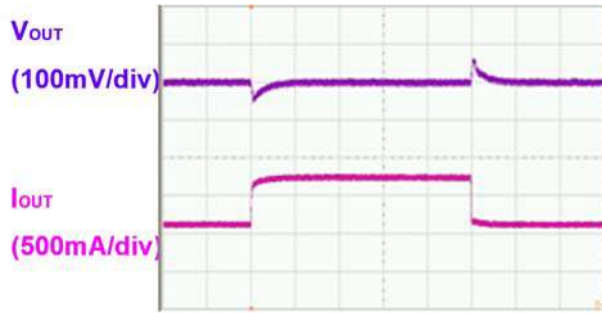
R1245x

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15) Load transient response waveform

R1245x00xA/R1245x00xB

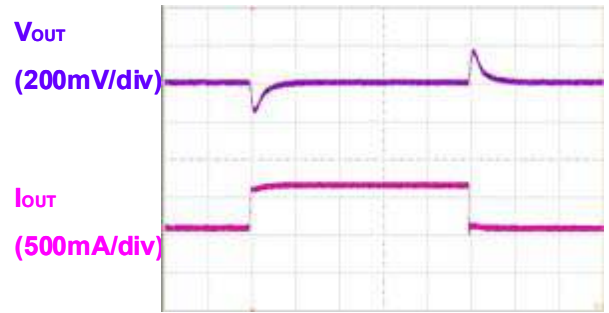
$V_{OUT} = 0.8\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600 \leftrightarrow 1200\text{ mA}$, $T_a = 25^\circ\text{C}$



100 μ s/div

R1245x00XA/R1245x00xB

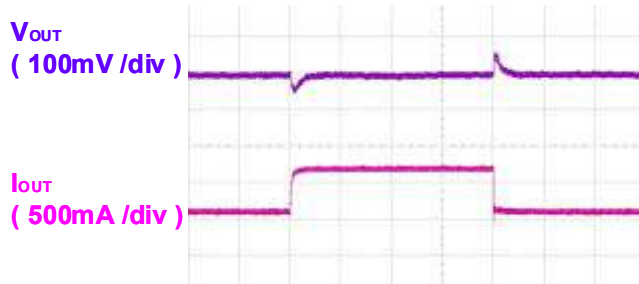
$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600 \leftrightarrow 1200\text{ mA}$, $T_a = 25^\circ\text{C}$



100 μ s/div

R1245x00xG/R1245x00xH

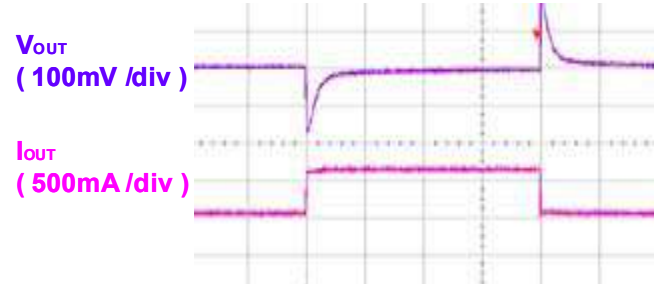
$V_{OUT} = 1.5\text{ V}$, $V_{IN} = 4.5\text{ V}$, $I_{OUT} = 600 \leftrightarrow 1200\text{ mA}$, $T_a = 25^\circ\text{C}$



50us/div

R1245x00xG/R1245x00xH

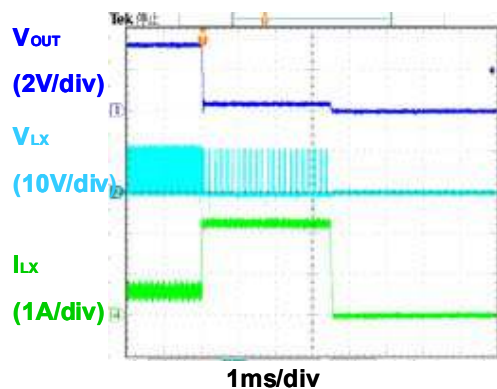
$V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $I_{OUT} = 600 \leftrightarrow 1200\text{ mA}$, $T_a = 25^\circ\text{C}$



50us/div

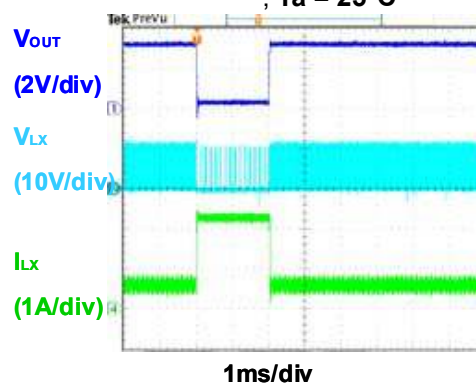
16) Limit latch operation waveform

R1245x00xA

 $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $R_{OUT} = 5.5\ \Omega \rightarrow 0.05\ \Omega$, $T_a = 25^\circ\text{C}$ 

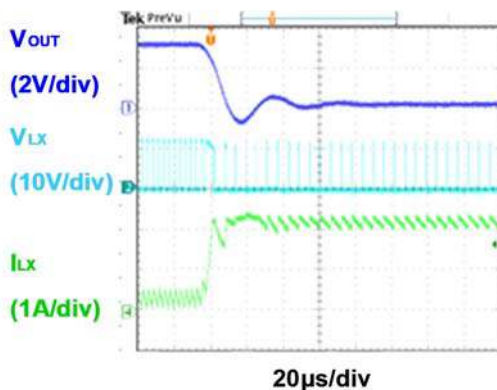
17) Released waveform from limit latch

R1245x00xA

 $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $R_{OUT} = 5.5\ \Omega \rightarrow 0.05\ \Omega \rightarrow 5.5\ \Omega$, $T_a = 25^\circ\text{C}$ 

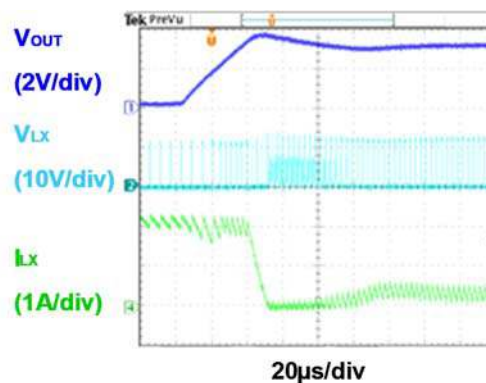
18) Fold-back operation waveform

R1245x00xB

 $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $R_{OUT} = 5.5\ \Omega \rightarrow 0.05\ \Omega$, $T_a = 25^\circ\text{C}$ 

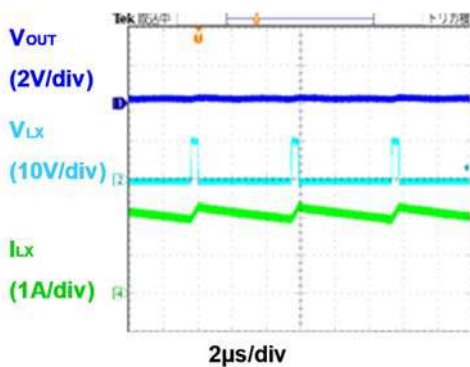
19) Released waveform from fold-back

R1245x00xB

 $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $R_{OUT} = 5.5\ \Omega \rightarrow 0.05\ \Omega \rightarrow 5.5\ \Omega$, $T_a = 25^\circ\text{C}$ 

20) Switching waveform at fold-back operation

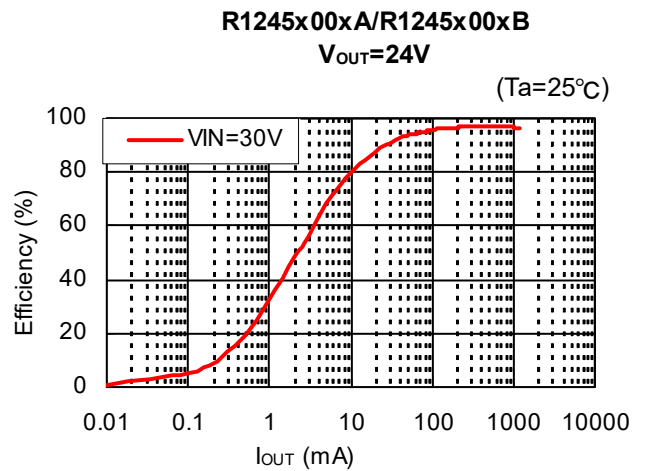
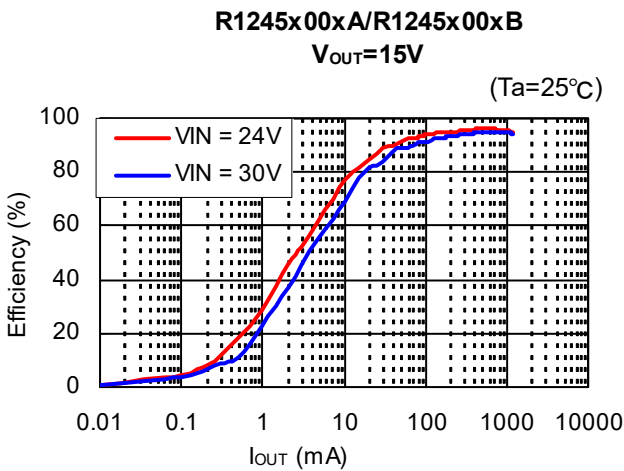
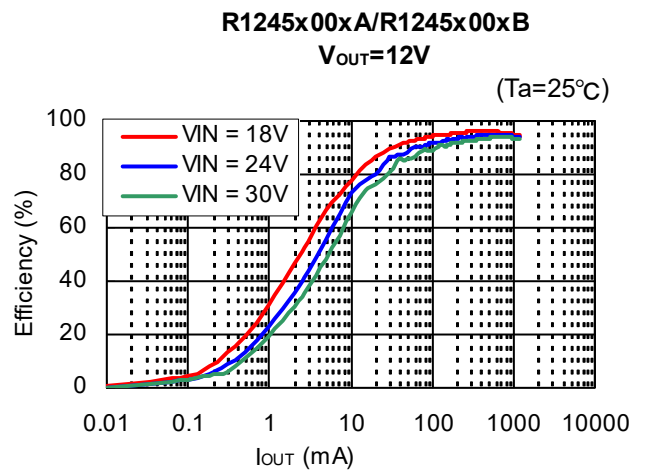
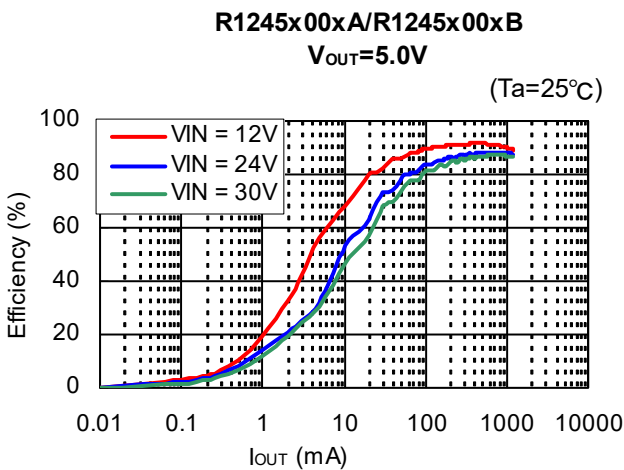
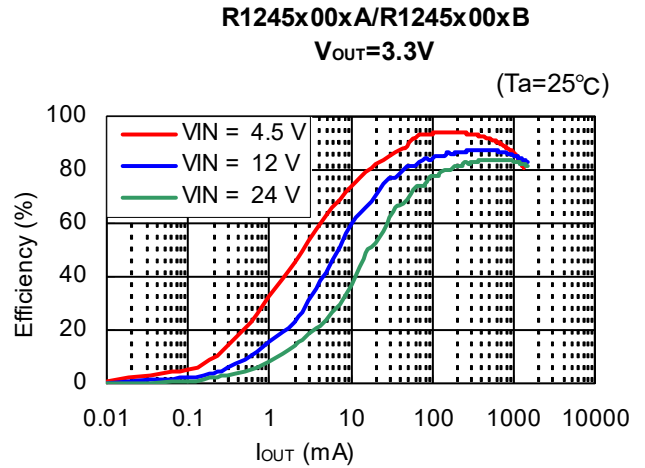
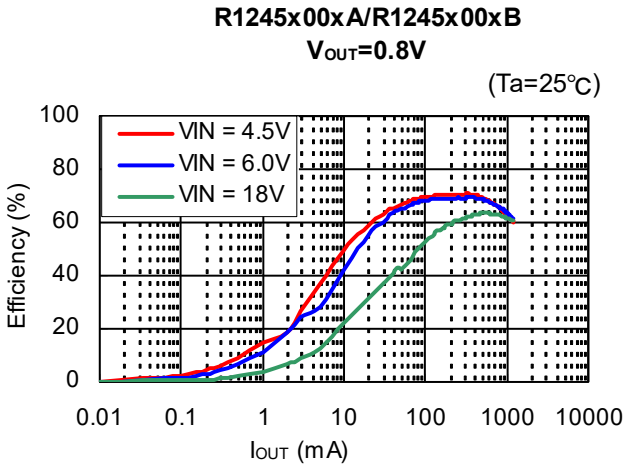
R1245x00xB

 $V_{OUT} = 3.3\text{ V}$, $V_{IN} = 12\text{ V}$, $R_{OUT} = 0.05\ \Omega$, $T_a = 25^\circ\text{C}$ 

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21) Output current vs. Efficiency (Version A/B)

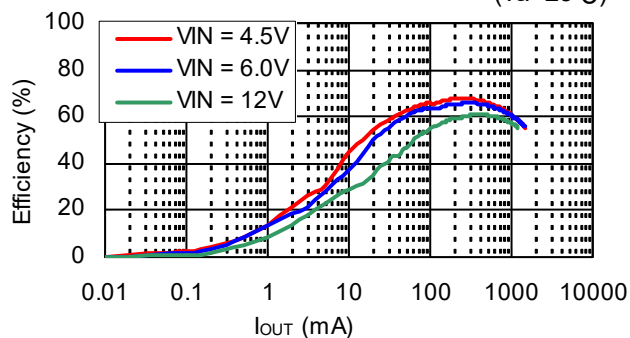


22) Output Current vs. Efficiency (Version C/D)

R1245x00xC/R1245x00xD

V_{OUT}=0.8V

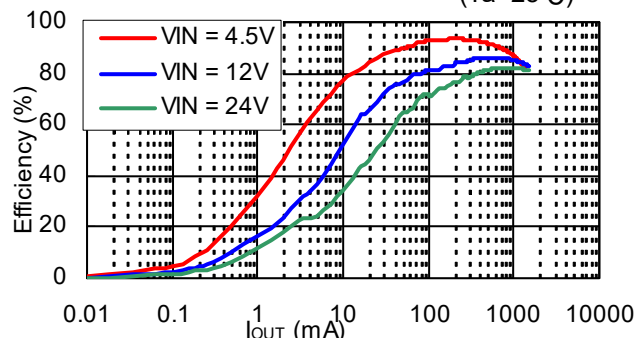
(Ta=25°C)



R1245x00xC/R1245x00xD

V_{OUT}=3.3V

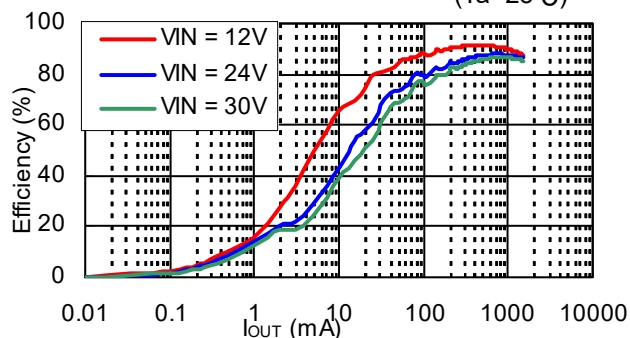
(Ta=25°C)



R1245x00xC/R1245x00xD

V_{OUT}=5.0V

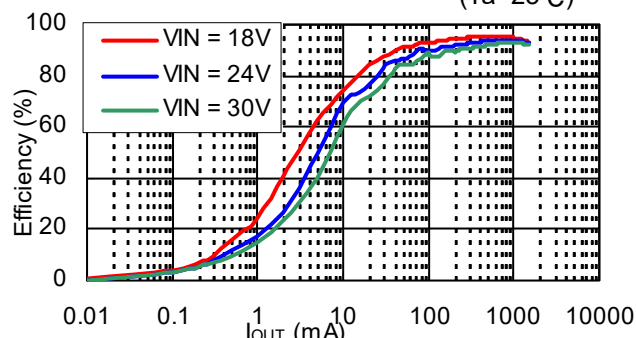
(Ta=25°C)



R1245x00xC/R1245x00xD

V_{OUT}=12V

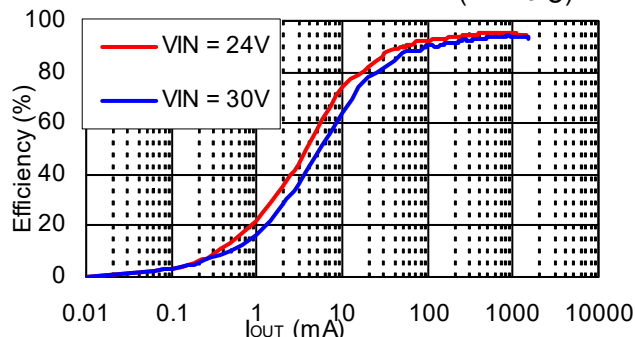
(Ta=25°C)



R1245x00xC/R1245x00xD

V_{OUT}=15V

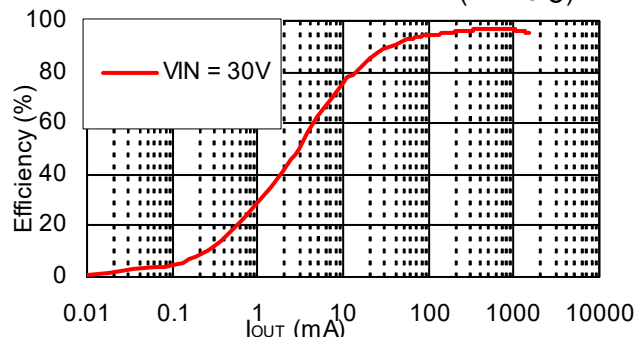
(Ta=25°C)



R1245x00xC/R1245x00xD

V_{OUT}=24V

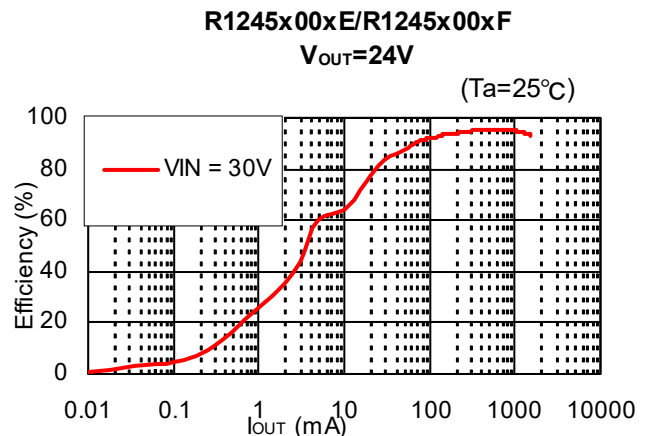
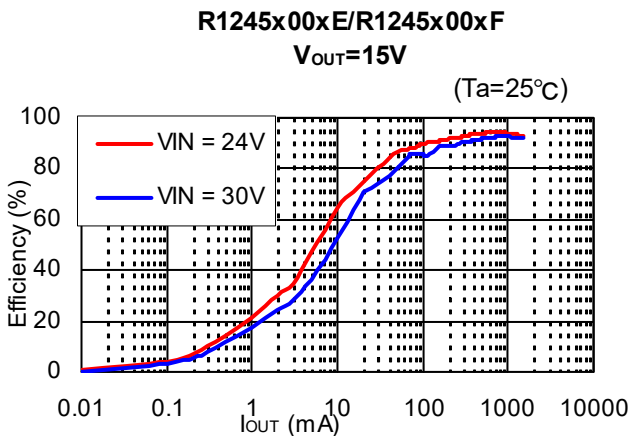
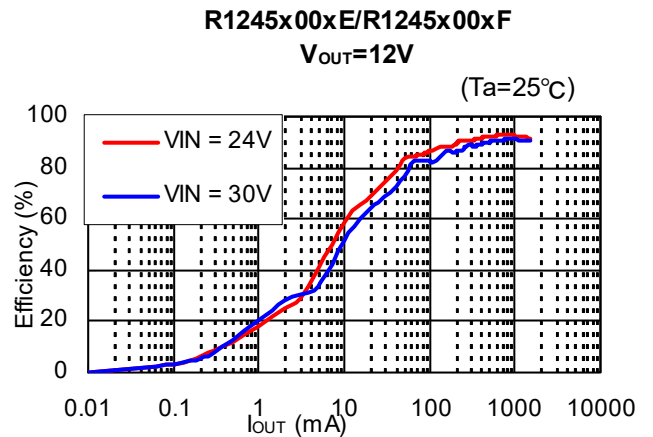
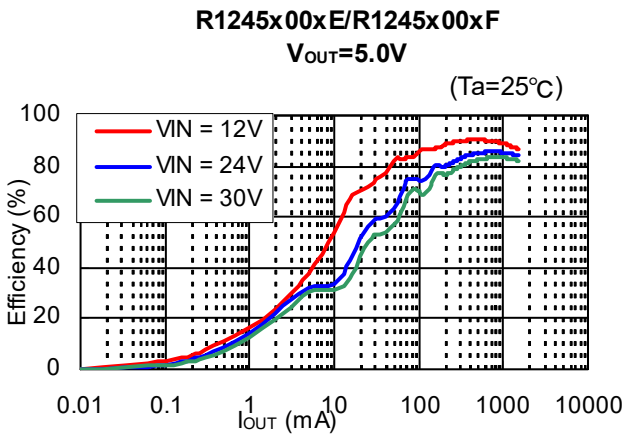
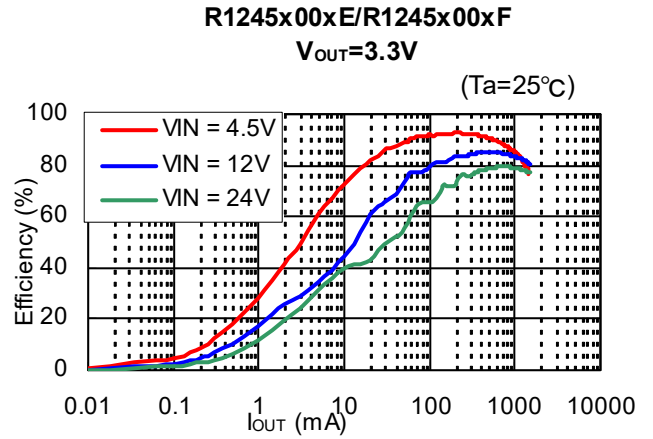
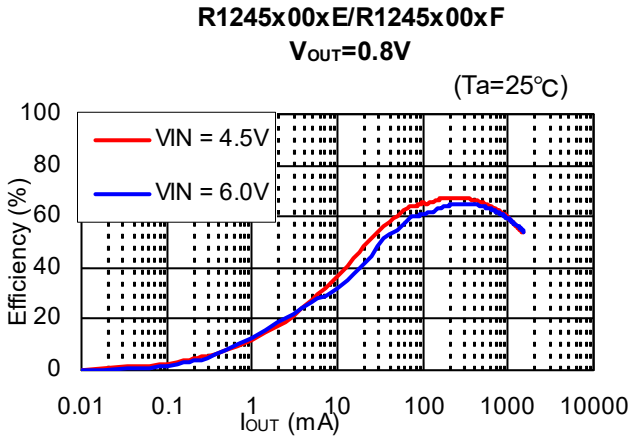
(Ta=25°C)



R1245x

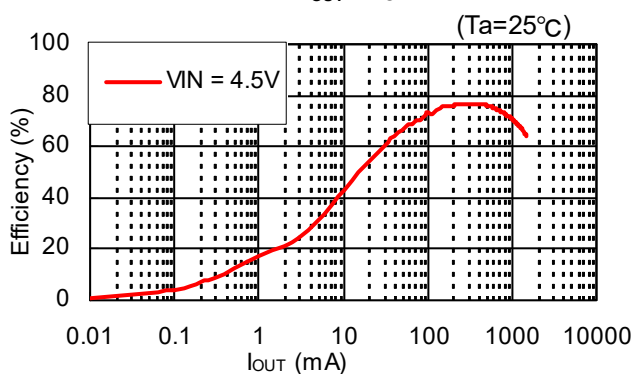
No. EC-269-201022

23) Output current vs. Efficiency (Version E/F)

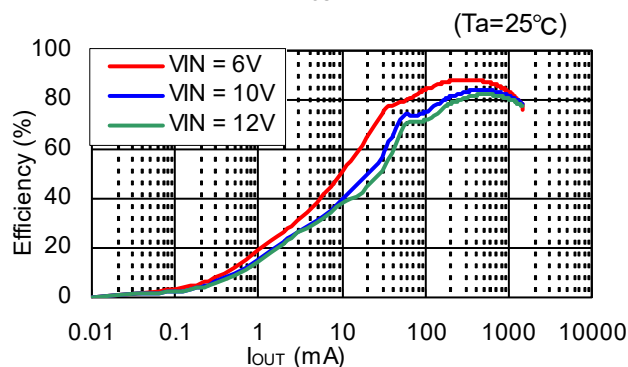


24) Output current vs. Efficiency (Version G/H)

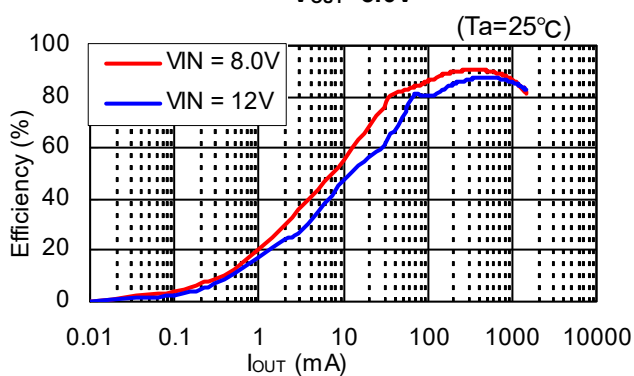
R1245x00xG/R1245x00xH
V_{OUT}=1.5V



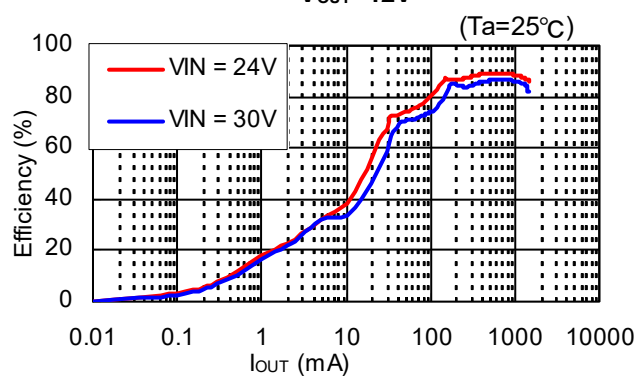
R1245x00xG/R1245x00xH
V_{OUT}=3.3V



R1245x00xG/R1245x00xH
V_{OUT}=5.0V



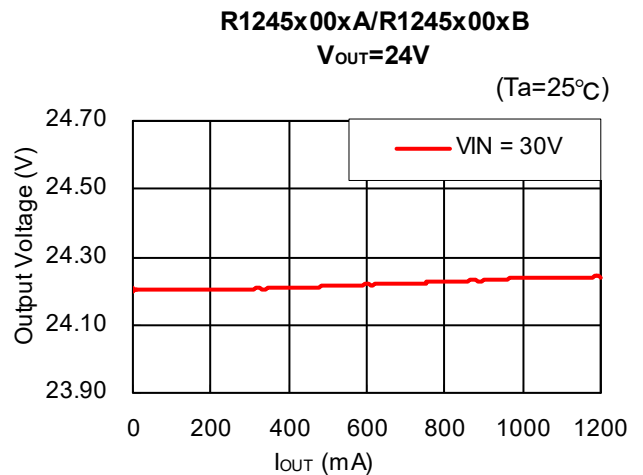
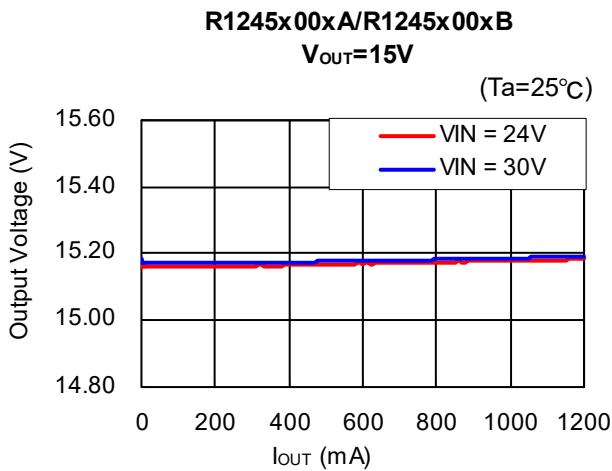
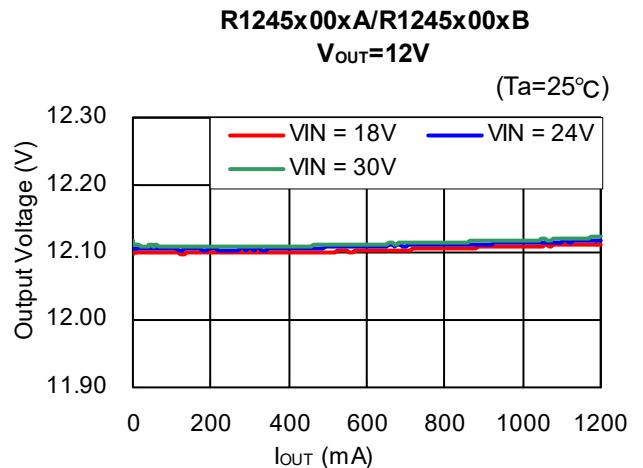
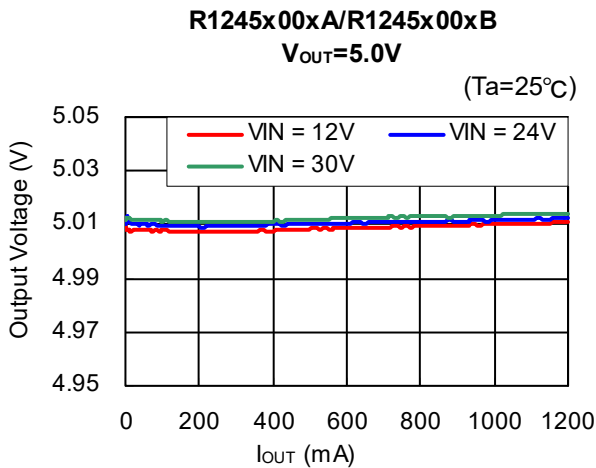
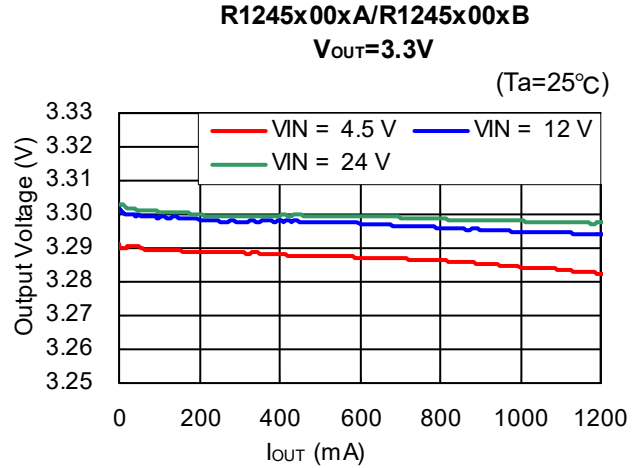
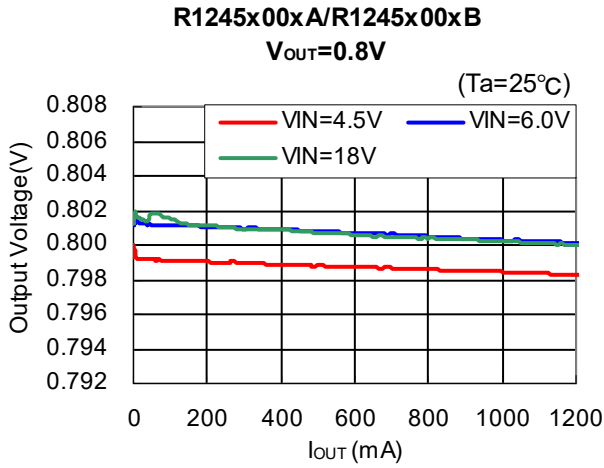
R1245x00xG/R1245x00xH
V_{OUT}=12V



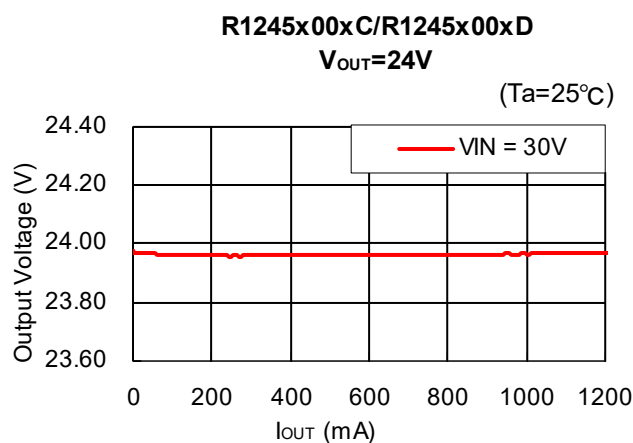
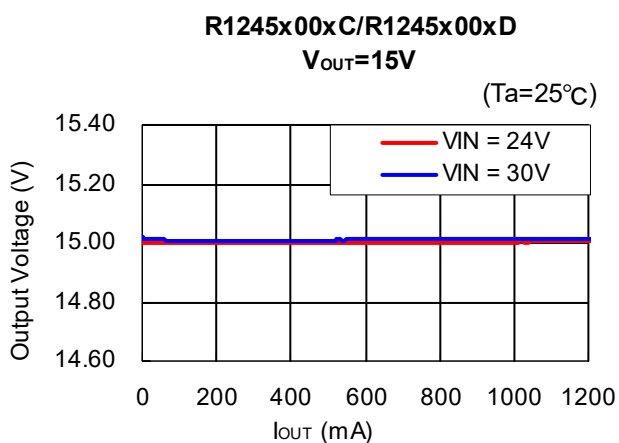
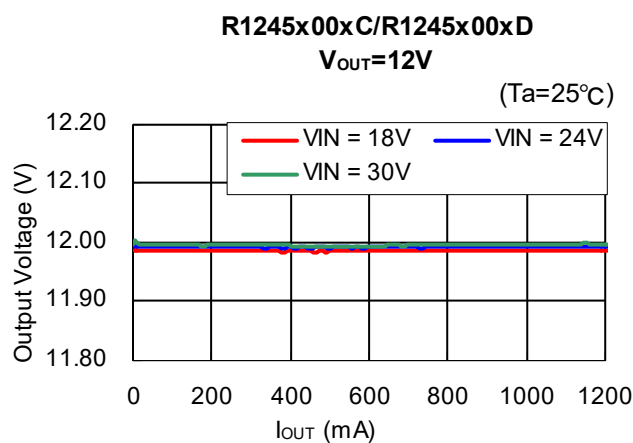
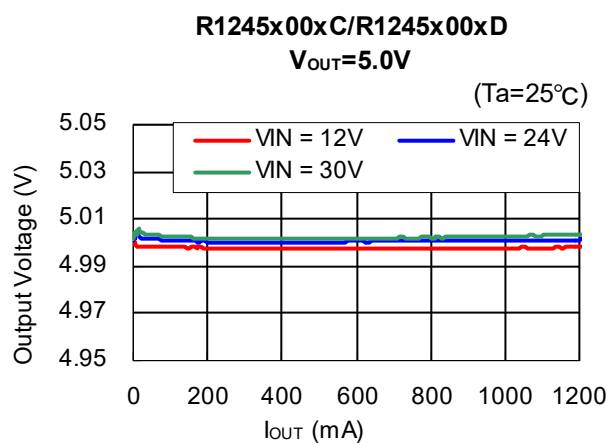
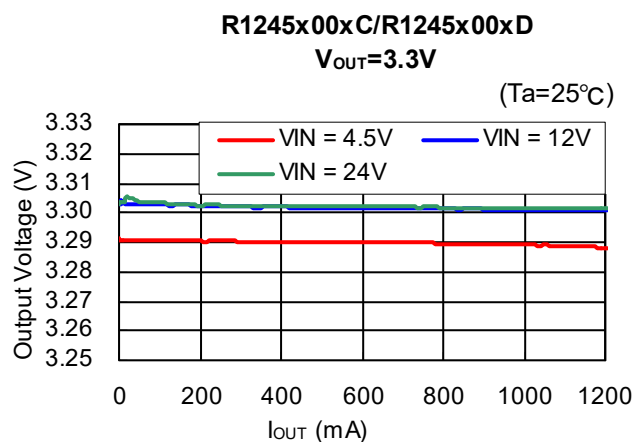
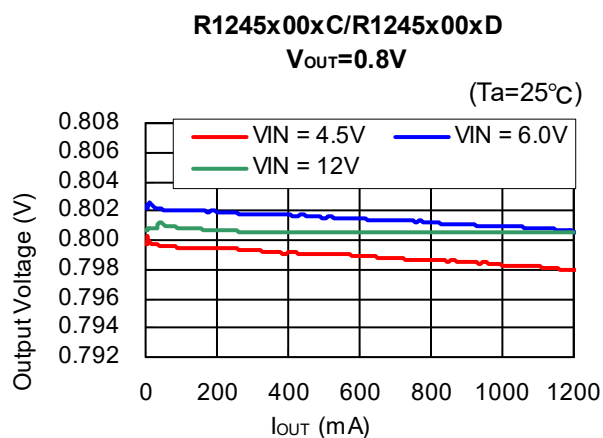
R1245x

No. EC-269-201022

25) Output current vs Output voltage (Version A/B)



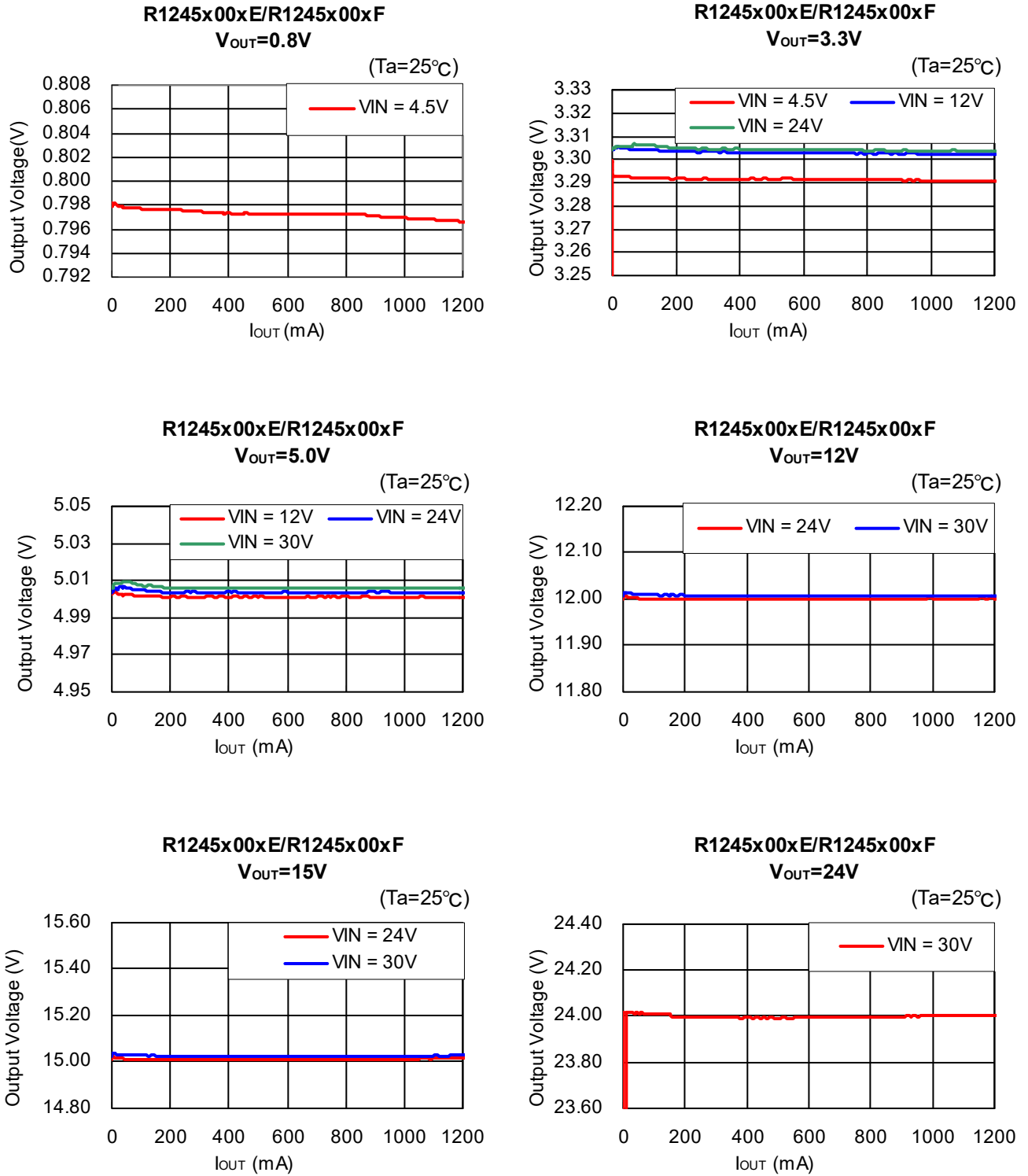
26) Output current vs. Output voltage (Version C/D)



R1245x

No. EC-269-201022

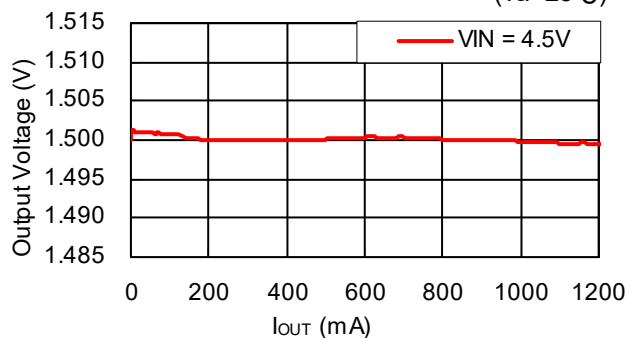
27) Output current vs. Output voltage (Version E/F)



28) Output current vs. Output voltage (Version G/H)

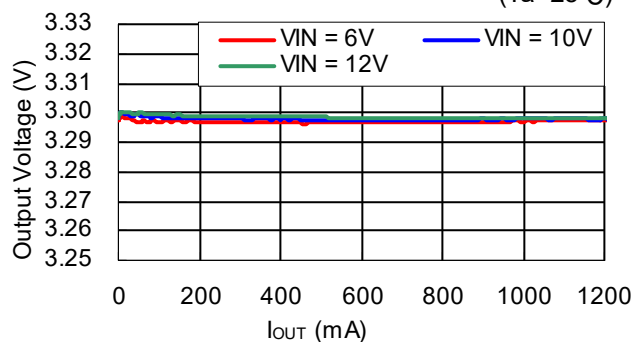
R1245x00xG/R1245x00xH
 $V_{OUT}=1.5V$

($T_a=25^{\circ}C$)



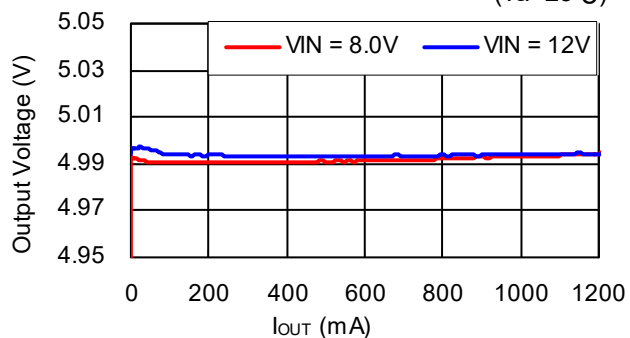
R1245x00xG/R1245x00xH
 $V_{OUT}=3.3V$

($T_a=25^{\circ}C$)



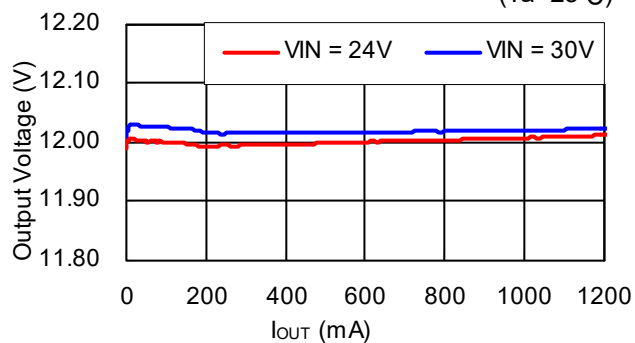
R1245x00xG/R1245x00xH
 $V_{OUT}=5.0V$

($T_a=25^{\circ}C$)



R1245x00xG/R1245x00xH
 $V_{OUT}=12V$

($T_a=25^{\circ}C$)



R1245x

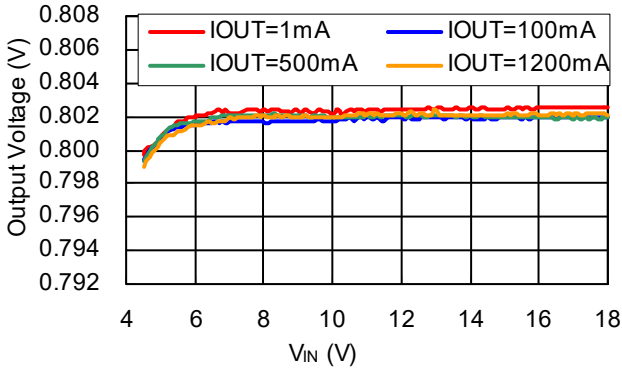
No. EC-269-201022

29) Input voltage vs. Output voltage (Version A/B)

R1245x00xA/R1245x00xB

$V_{OUT}=0.8V$

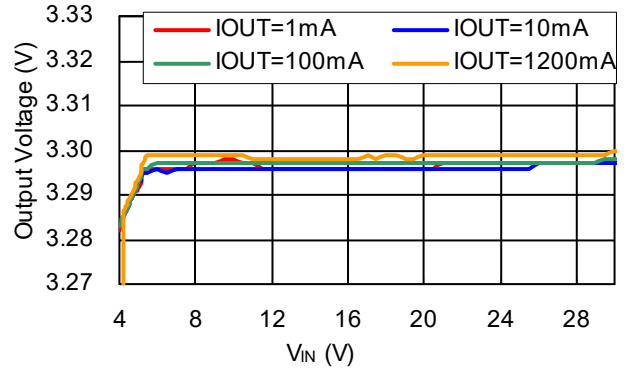
($T_a=25^\circ C$)



R1245x00xA/R1245x00xB

$V_{OUT}=3.3V$

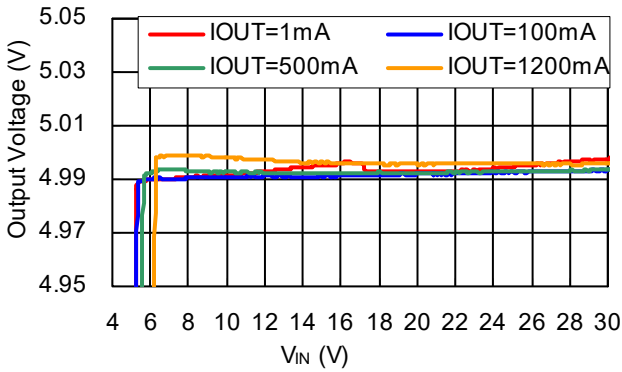
($T_a=25^\circ C$)



R1245x00xA/R1245x00xB

$V_{OUT}=5.0V$

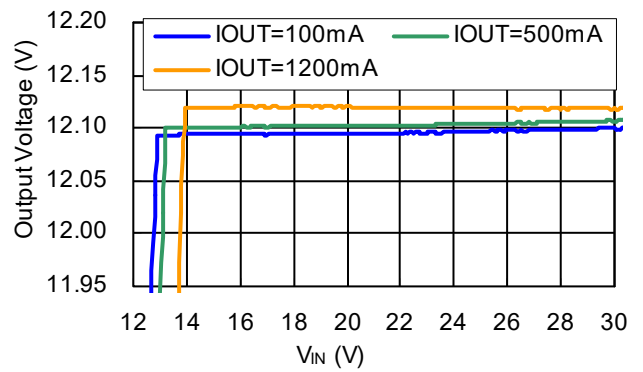
($T_a=25^\circ C$)



R1245x00xA/R1245x00xB

$V_{OUT}=12V$

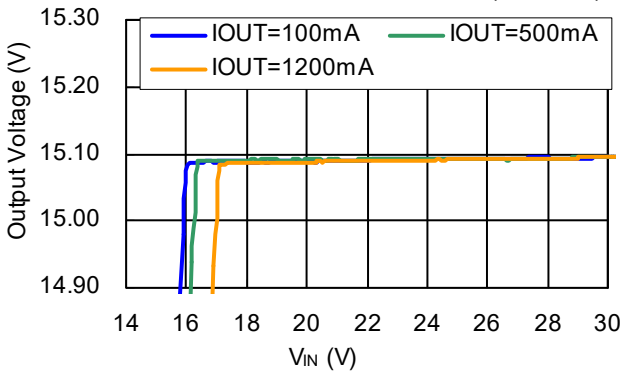
($T_a=25^\circ C$)



R1245x00xA/R1245x00xB

$V_{OUT}=15V$

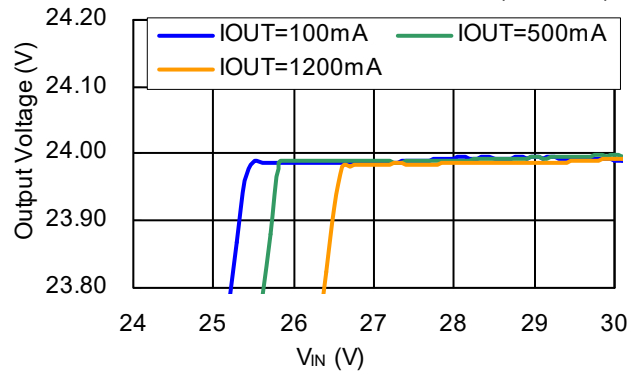
($T_a=25^\circ C$)



R1245x00xA/R1245x00xB

$V_{OUT}=24V$

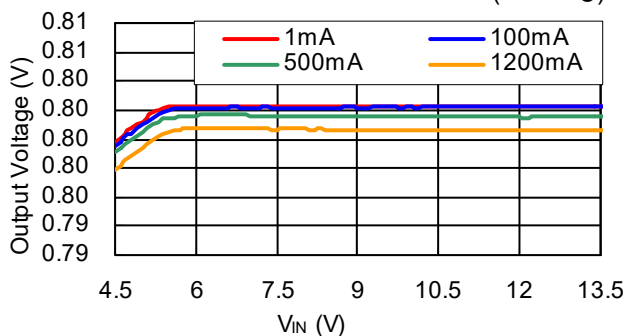
($T_a=25^\circ C$)



30) Input voltage vs. Output voltage (Version C/D)

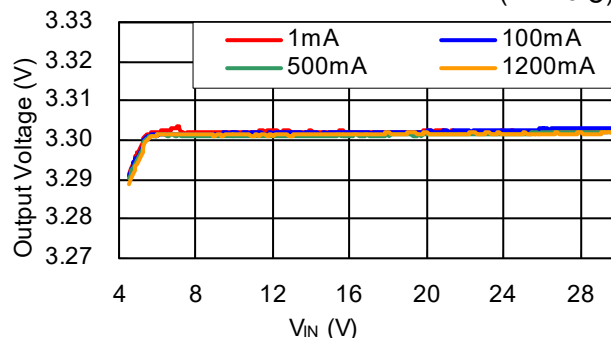
R1245x00xC/R1245x00xD
V_{OUT}=0.8V

(Ta=25°C)



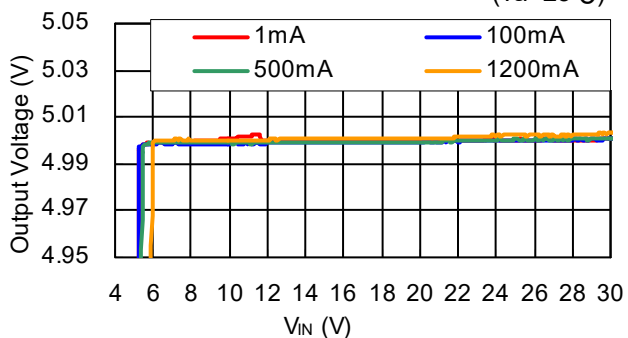
R1245x00xC/R1245x00xD
V_{OUT}=3.3V

(Ta=25°C)



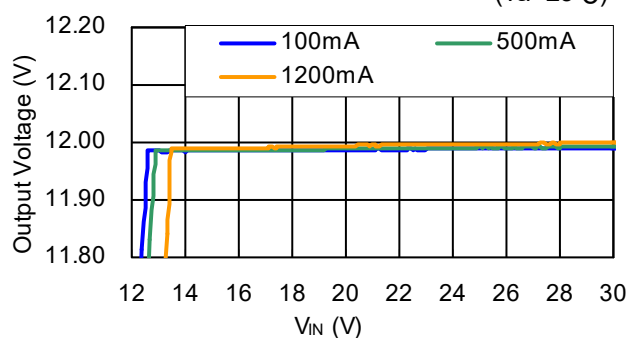
R1245x00xC/R1245x00xD
V_{OUT}=5.0V

(Ta=25°C)



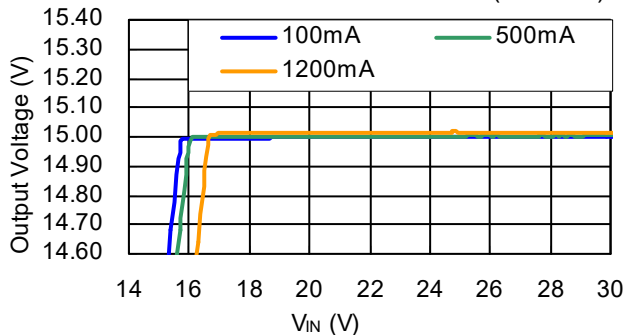
R1245x00xC/R1245x00xD
V_{OUT}=12V

(Ta=25°C)



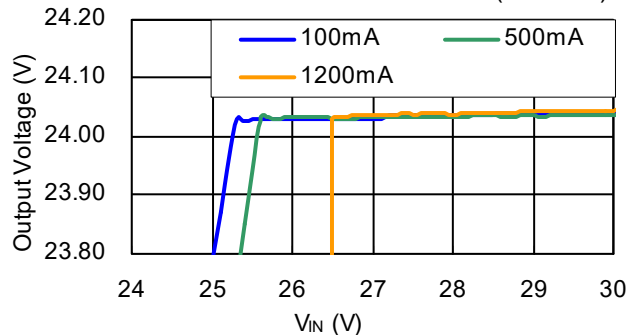
R1245x00xC/R1245x00xD
V_{OUT}=15V

(Ta=25°C)



R1245x00xC/R1245x00xD
V_{OUT}=24V

(Ta=25°C)



R1245x

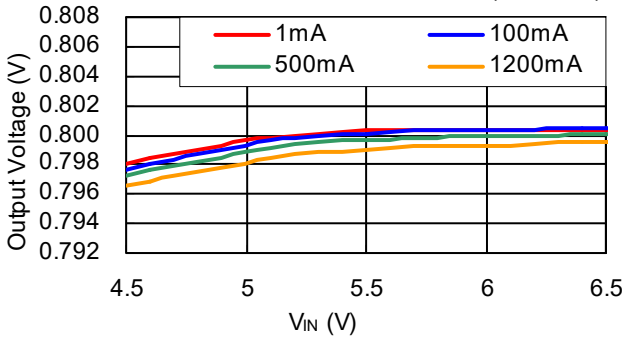
No. EC-269-201022

31) Input voltage vs. Output voltage (Version E/F)

R1245x00xE/R1245x00xF

$V_{OUT}=0.8V$

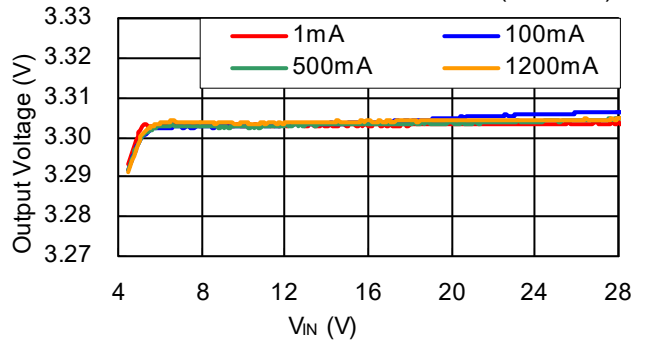
($T_a=25^\circ C$)



R1245x00xE/R1245x00xF

$V_{OUT}=3.3V$

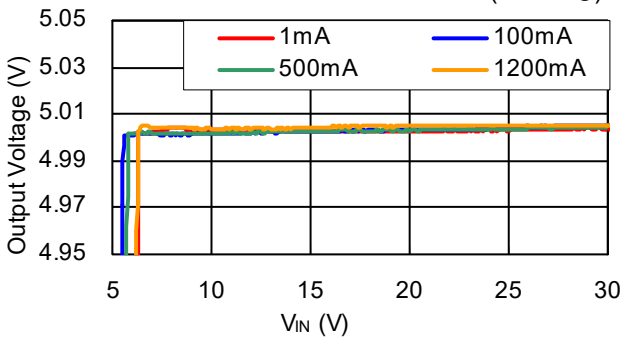
($T_a=25^\circ C$)



R1245x00xE/R1245x00xF

$V_{OUT}=5.0V$

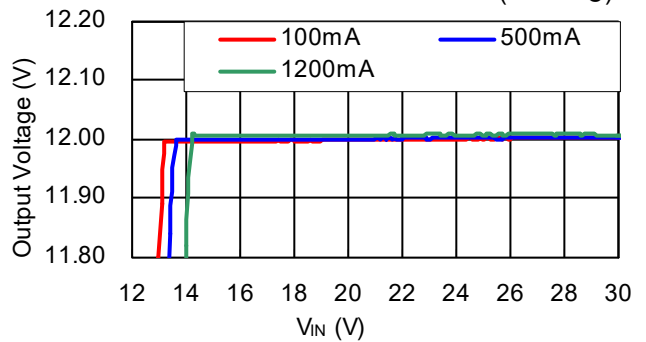
($T_a=25^\circ C$)



R1245x00xE/R1245x00xF

$V_{OUT}=12V$

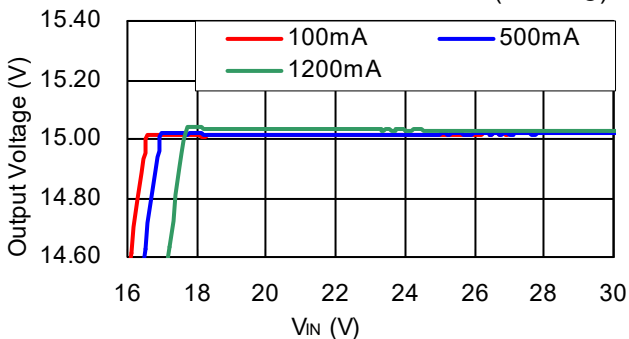
($T_a=25^\circ C$)



R1245x00xE/R1245x00xF

$V_{OUT}=15V$

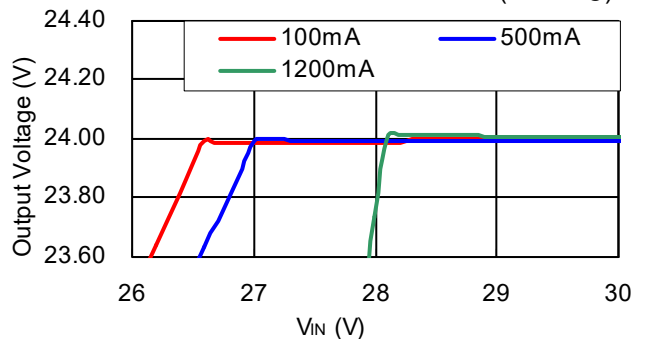
($T_a=25^\circ C$)



R1245x00xE/R1245x00xF

$V_{OUT}=24V$

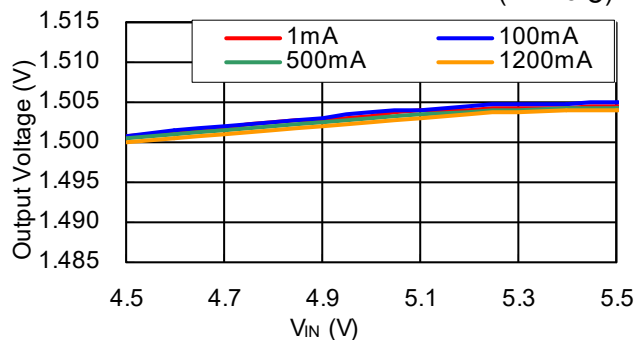
($T_a=25^\circ C$)



32) Input voltage vs. Output voltage (Version G/H)

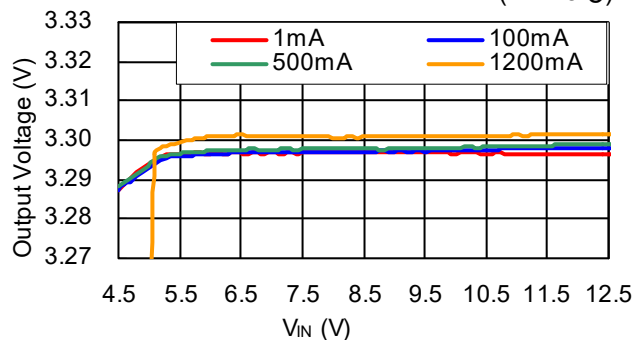
R1245x00xG/R1245x00xH
V_{OUT}=1.5V

(Ta=25°C)



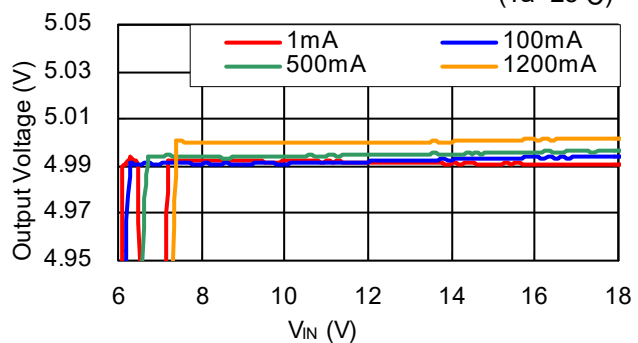
R1245x00xG/R1245x00xH
V_{OUT}=3.3V

(Ta=25°C)



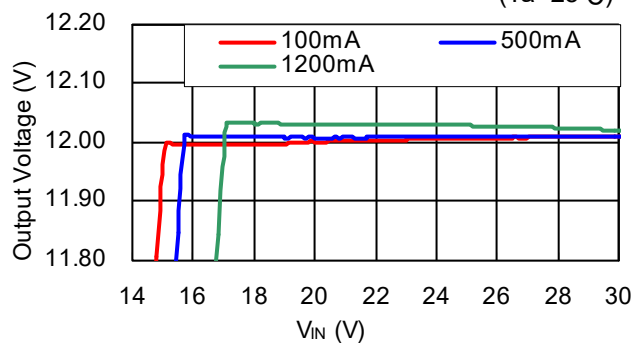
R1245x00xG/R1245x00xH
V_{OUT}=5.0V

(Ta=25°C)



R1245x00xG/R1245x00xH
V_{OUT}=12V

(Ta=25°C)



The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

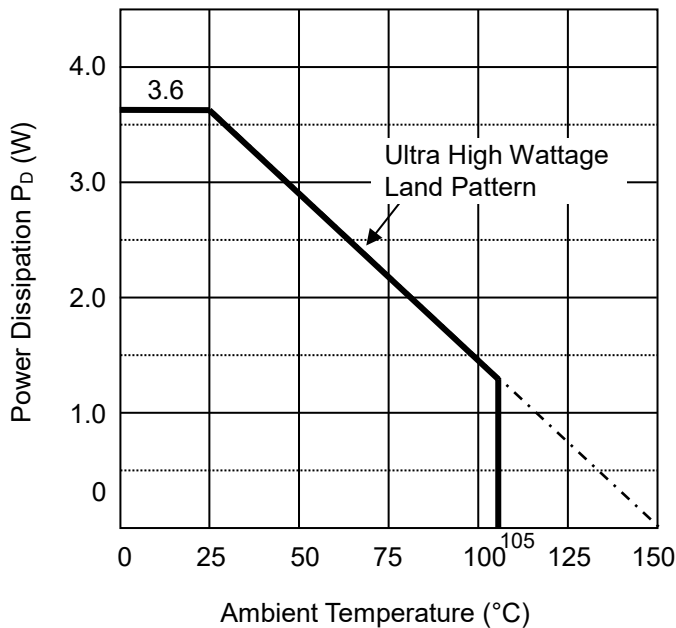
Measurement Conditions

Ultra High Wattage Land Pattern	
Environment	Mounting on Board (Wind Velocity = 0 m/s)
Board Material	Glass Cloth Epoxy Plastic (Four-Layer Board)
Board Dimensions	76.2 mm × 114.3 mm × 0.8 mm
Copper Ratio	Outer Layers (First and Fourth Layers): 95% of 50 mm Square Inner Layers (Second and Third Layers): 100% of 50 mm Square
Through-holes	φ 0.4 mm × 21 pcs

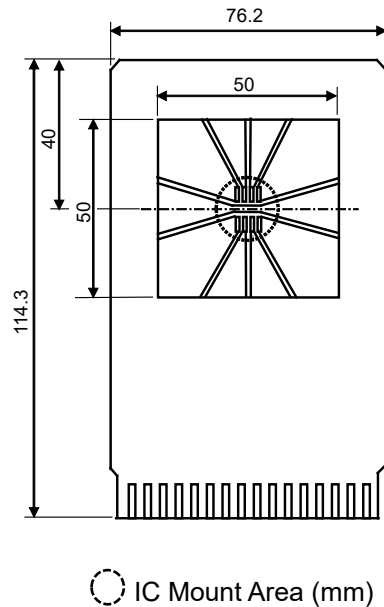
Measurement Result

(Ta = 25°C, Tjmax = 150°C)

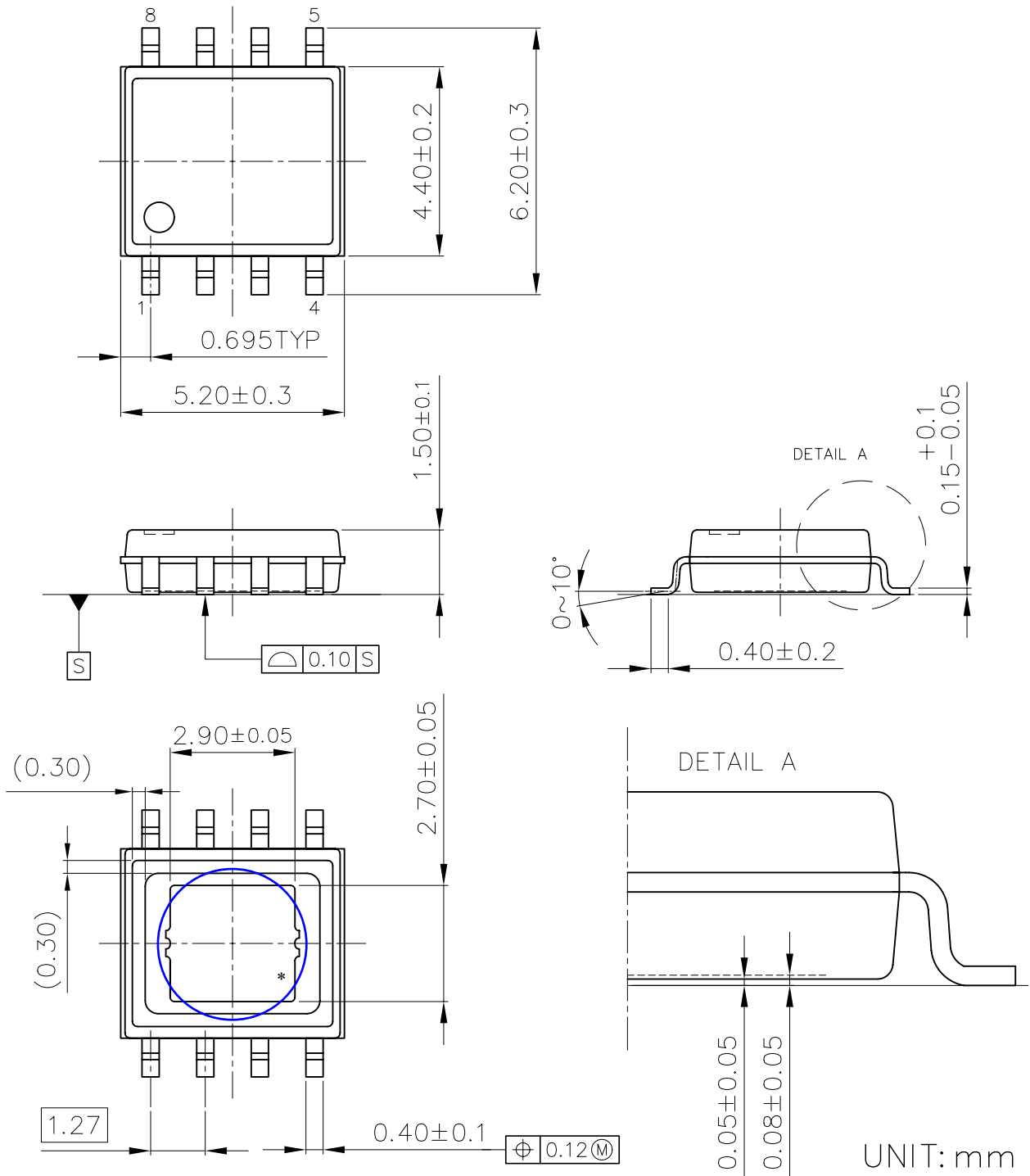
Ultra High Wattage Land Pattern	
Power Dissipation	3.6 W
Thermal Resistance	$\theta_{ja} = (150 - 25^\circ\text{C}) / 3.6 \text{ W} = 35^\circ\text{C/W}$
	$\theta_{jc} = 10^\circ\text{C/W}$



Power Dissipation vs. Ambient Temperature



Measurement Board Pattern



HSOP-8E Package Dimensions

* The tab on the bottom of the package shown by blue circle is a substrate potential (GND). The tab must be connected to the ground plane on the board.

The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

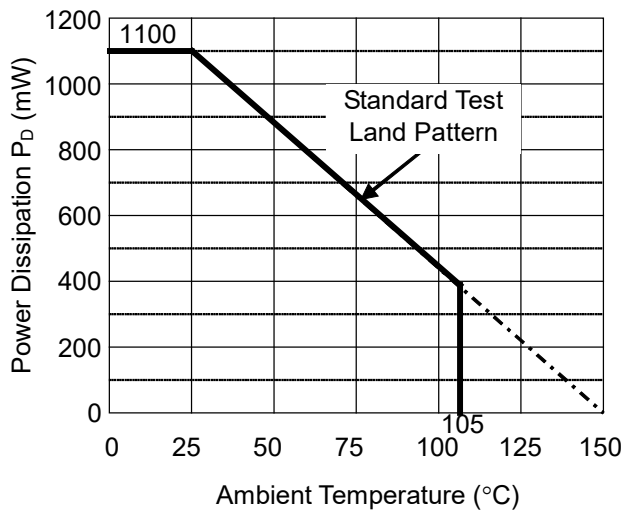
Measurement Conditions

	Standard Test Land Pattern
Environment	Mounting on Board (Wind Velocity = 0 m/s)
Board Material	Glass Cloth Epoxy Plastic (Double-Sided Board)
Board Dimensions	40 mm × 40 mm × 1.6 mm
Copper Ratio	Top Side: Approx. 50% Bottom Side: Approx. 50%
Through-holes	φ 0.54 mm × 30 pcs

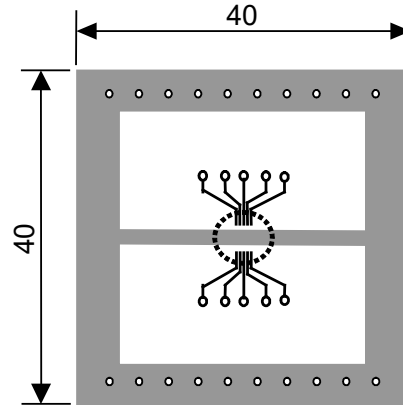
Measurement Result

(Ta = 25°C, Tjmax = 150°C)

	Standard Test Land Pattern
Power Dissipation	1100 mW
Thermal Resistance	$\theta_{ja} = (150^{\circ}\text{C} - 25^{\circ}\text{C}) / 1.1 \text{ W} = 114^{\circ}\text{C/W}$

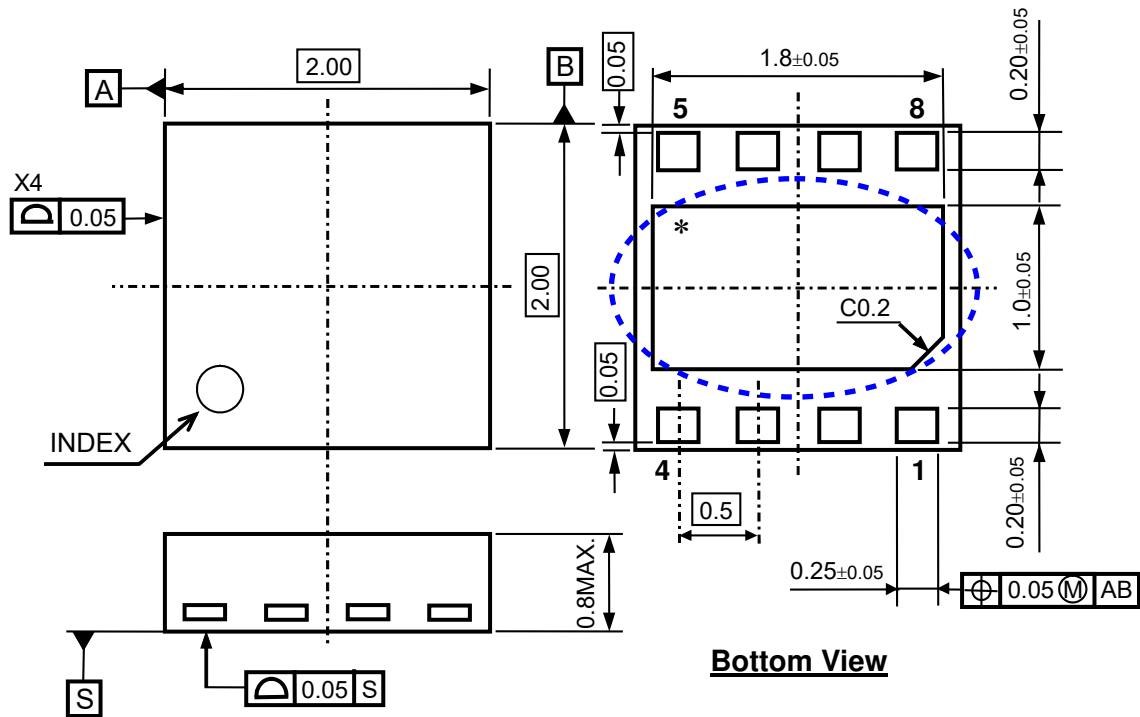


Power Dissipation vs. Ambient Temperature



○ IC Mount Area (mm)

Measurement Board Pattern



DFN2020-8 Package Dimensions (Unit: mm)

* The tab on the bottom of the package shown by blue circle is a substrate potential (GND). The tab must be connected to the ground plane on the board.



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