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- $\bullet$  **Low Output Common-Mode Sensitivity to AGC Voltages**
- $\bullet$  **Input and Output Impedances Independent of AGC Voltage**
- $\bullet$ **Peak Gain . . . 38 dB Typ**
- $\bullet$ **Wide AGC Range . . . 50 dB Typ**
- $\bullet$ **3-dB Bandwidth . . . 50 MHz**
- $\bullet$  **Other Characteristics Similar to NE592 and uA733**

#### IN– **I** REF OUT  $\mathsf{V}_\mathsf{CC^+}$ TOUT– 1 2 3 4 8 7 6 5 IN+ AGC **N**  $V_{CC}$ OUT+<sub>I</sub> **D OR P PACKAGE (TOP VIEW) symbol + – AGC IN + IN – 7 4 5 2 1 8 REF OUT OUT+ OUT–**

### **description**

This device is a monolithic two-stage highfrequency amplifier with differential inputs and outputs.

Internal feedback provides wide bandwidth, low phase distortion, and excellent gain stability. Variable gain based on signal summation provides large AGC control over a wide bandwidth with low harmonic distortion. Emitter-follower outputs enable the device to drive capacitive loads. All stages are current-source biased to obtain high common-mode and supply-voltage rejection ratios. The gain may be electronically attenuated by applying a control voltage to the AGC pin. No external compensation components are required.

This device is particularly useful in TV and radio IF and RF AGC circuits, as well as magnetic-tape and disk-file systems where AGC is needed. Other applications include video and pulse amplifiers where a large AGC range, wide bandwidth, low phase shift, and excellent gain stability are required.

The TL026C is characterized for operation from 0°C to 70°C.

## **absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†**



† Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. This is a stress rating only, and functional operation of the device at these or any other conditions beyond those indicated in the recommended operating conditions section of this specification is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTE 1: All voltages are with respect to the midpoint of  $V_{\text{CC+}}$  and  $V_{\text{CC-}}$  except differential input and output voltages.

#### **DISSIPATION RATING TABLE**





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## **recommended operating conditions**



### **electrical characteristics at 25**°**C operating free-air temperature, VCC+ =** ±**6 V, VAGC = 0, REF OUT pin open (unless otherwise specified)**





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**electrical characteristics over recommended operating free-air temperature range,**  $V_{CC\pm} = \pm 6$  **V, VAGC = 0, REF OUT pin open (unless otherwise specified)**

	<b>PARAMETER</b>	<b>FIGURE</b>	<b>TEST CONDITIONS</b>	<b>MIN</b>	<b>TYP</b>	<b>MAX</b>	<b>UNIT</b>
A <sub>V</sub> D	Large-signal differential voltage amplification		$V_O(PP) = 3 V$ , $R_L = 2 k\Omega$	55		115	V/V
$I_{IO}$	Input offset current					6	μA
<sup>I</sup> IB	Input bias current					40	μA
<b>VICR</b>	Common-mode input voltage range	3		$+1$			V
Voo	Output offset voltage		$V_{ID} = 0$ , $R_1 = \infty$			1.5	V
$V_{O(PP)}$	Maximum peak-to-peak output voltage swing		$R_1 = 2 k\Omega$	2.8			V
	Input resistance at AGC, IN+, or IN -			8			$k\Omega$
<b>CMRR</b>	Common-mode rejection ratio	3	$V_{\text{IC}} = \pm 1 \text{ V}, \qquad f = 100 \text{ kHz}$	50			dB
k <sub>SVR</sub>	Supply voltage rejection ratio $(\Delta V_{CC}/\Delta V_{IO})$	$\overline{4}$	$\Delta V_{\text{CC}}$ + = $\pm$ 0.5 V, $\Delta V_{\rm CC} = \pm 0.5 \text{ V}$	50			dB
lsink(max)	Maximum output sink current		$V_{ID} = 1 V$ , $V_O = 3 V$	2.8	4		mA
$_{\text{LCC}}$	Supply current		No load. No signal			30	mA

## **PARAMETER MEASUREMENT INFORMATION**







**Figure 3. Test Circuit**



**Figure 2. Test Circuit**



**Figure 4. Test Circuit**



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**TYPICAL CHARACTERISTICS**

**Figure 5**



## **APPLICATION INFORMATION**

#### **gain characteristics**

Figure 5 shows the differential voltage amplification versus the differential gain-control voltage (V<sub>AGC</sub> – V<sub>ref</sub>).  $V_{\rm AGC}$  is the absolute voltage applied to the A<sub>GC</sub> input and V<sub>ref</sub> is the dc voltage at the REF OUT output. As V<sub>AGC</sub> increases with respect to  $V_{ref}$ , the TL026C gain changes from maximum to minimum. As shown in Figure 5 for example, V<sub>AGC</sub> would have to vary from approximately 180 mV less than V<sub>ref</sub> to approximately 180 mV greater than V<sub>ref</sub> to change the gain from maximum to minimum. The total signal change in V<sub>AGC</sub> is defined by the following equation.

$$
\Delta V_{AGC} = V_{ref} + 180 \text{ mV} - (V_{ref} - 180 \text{ mV})
$$
\n
$$
\tag{1}
$$

 $\Delta V_{\text{AGC}} = 360 \text{ mV}$ 

However, because V<sub>AGC</sub> varies as the ac AGC signal varies and also differentially around V<sub>ref</sub>, then V<sub>AGC</sub> should have an ac signal component and a dc component. To preserve the dc and thermal tracking of the device, this dc voltage must be generated from V<sub>ref</sub>. To apply proper bias to the AGC input, the external circuit used to generate  $V_{AGC}$  must combine these two voltages. Figures 6 and 7 show two circuits that will perform this operation and are easy to implement. The circuits use a standard dual operational amplifier for AGC feedback. By providing rectification and the required feedback gain, these circuits are also complete AGC systems.

### **circuit operation**

Amplifier A1 amplifies and inverts the rectified and filtered AGC signal voltage V<sub>C</sub> producing output voltage V1. Amplifier A2 is a differential amplifier that inverts V1 again and adds the scaled V<sub>ref</sub> voltage. This conditioning makes V<sub>AGC</sub> the sum of the signal plus the scaled V<sub>ref</sub>. As the signal voltage increases, V<sub>AGC</sub> increases and the gain of the TL026C is reduced. This maintains a constant output level.

#### **feedback circuit equations**

Following the AGC input signal (Figures 6 and 7) from the OUT output through the feedback amplifiers to the AGC input produces the following equations:





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## **APPLICATION INFORMATION**

Amplifier A2 inverts V1 producing a positive AGC signal voltage. Therefore, the input voltage to the TL026C AGC pin consists of an AGC signal equal to:

$$
\frac{R2}{R1} V_C
$$
 (6)

and a dc voltage derived from  $V_{ref}$ , defined as the quiescent value of  $V_{AGC}$ .

$$
V_{AGC}(q) = 2\frac{R6}{R5 + R6}V_{ref} \tag{7}
$$

For the initial resistor calculations,  $V_{ref}$  is assumed to be typically 1.4 V making quiescent  $V_{AGC}$  approximately 1.22 V (V<sub>AGC</sub>(q) = V<sub>ref</sub> – 180 mV). This voltage allows the TL026C to operate at maximum gain under no-signal and low-signal conditions. In addition, with  $V_{ref}$  used as both internal and external reference, its variation from device to device automatically adjusts the overall bias and makes AGC operation essentially independent of the absolute value of V<sub>ref</sub>. The resistor divider needs to be calculated only once and is valid for the full tolerance of Vref.

### **output voltage limits (see Figures 6 and 7)**

The output voltage level desired must fall within the following limits:

- 1. Because the data sheet minimum output swing is 3 V peak-to-peak using a 2-kΩ load resistor, the user-selected design limit for the peak output swing should not exceed 1.5 V.
- 2. The voltage drop of the rectifying diode determines the lower voltage limit. When a silicon diode is used, this voltage is approximately 0.7 V. The output voltage  $V<sub>O</sub>$  must have sufficient amplitude to exceed the rectifying diode drop. Aschottky diode can be used to reduce the  $V<sub>O</sub>$  level required.

## **gain calculations for a peak output voltage of 1 V**

A peak output voltage of 1 V was chosen for gain calculations because it is approximately midway between the limits of conditions 1 and 2 in the preceding paragraph.

Using equation 3 ( $V_C = V_{OP} - V_d$ ),  $V_C$  is calculated as follows:

$$
V_C = 1 V - 0.7 V
$$

 $V_C = 0.3 V$ 

Therefore, the gain of A1 must produce a voltage V1 that is equal to or greater than the total change in  $V_{\text{AGC}}$ for maximum TL026C gain change.

With a total change in  $V_{AGC}$  of 360 mV and using equation 4, the calculation is as follows:

$$
-\frac{V1}{V_C} = \frac{\Delta V_{AGC}}{V_C} = \frac{R2}{R1} = \frac{0.36}{0.3} = 1.2
$$

If R1 is 10 kΩ, R2 is 1.2 time R1 or 12 kΩ.

Since the output voltage for this circuit must be between 0.85 V and 1.3 V, the component values in Figures 6 and 7 provide a nominal 1-V peak output limit. This limit is the best choice to allow for temperature variations of the diode and minimum output voltage specification.



## **APPLICATION INFORMATION**

The circuit values in Figures 6 and 7 will produce the best results in this general application. Because of rectification and device input constraints, the circuit in Figure 6 will not provide attenuation and has about 32 dB of control range. The circuit shown in Figure 7 will have approximately 25% variation in the peak output voltage limit due to the variation in gain of the TL592 device to device. In addition, if a lower output voltage is desired, the output of the TL026C can be used for approximately 40 mV of controlled signal.

## **considerations for the use of the TL026C**

To obtain the most reliable results, RF breadboarding techniques must be used. A groundplane board should be used and power supplies should be bypassed with 0.1-µF capacitors. Input leads and output leads should be as short as possible and separated from each other.

A peak input voltage greater than 200 mV will begin to saturate the input stages of the TL026C and, while the circuit is in the AGC mode, the output signal may become distorted.

To observe the output signal of TL026C or TL592, low-capacitance FET probes or the output voltage divider technique shown in Figure 6 should be used.



NOTE:  $V_{\text{CC+}} = 6$  V and  $V_{\text{CC-}} = -6$  V for TL026C and amplifiers A1 and A2.

#### **Figure 6. Typical Application Circuit With No Attenuation**



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**APPLICATION INFORMATION**

NOTE:  $V_{CC}$  + = 6 V and  $V_{CC}$  = = - 6 V for TL026C and amplifiers A1 and A2.

**Figure 7. Typical Application Circuit With Attenuation**





## **PACKAGING INFORMATION**



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**ACTIVE:** Product device recommended for new designs.

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**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

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**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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**TEXAS** 

## **TAPE AND REEL INFORMATION**

**ISTRUMENTS** 





#### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**







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# **PACKAGE MATERIALS INFORMATION**



\*All dimensions are nominal



## **TEXAS NSTRUMENTS**

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## **TUBE**



## **B - Alignment groove width**

\*All dimensions are nominal





# **PACKAGE OUTLINE**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



# **EXAMPLE BOARD LAYOUT**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



# **EXAMPLE STENCIL DESIGN**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.



## **MECHANICAL DATA**

## PS (R-PDSO-G8)

**PLASTIC SMALL-OUTLINE PACKAGE** 



A. All linear dimensions are in millimeters.

B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion, not to exceed 0,15.





NOTES:

- A. All linear dimensions are in millimeters.
- Β. This drawing is subject to change without notice.
- Publication IPC-7351 is recommended for alternate designs. C.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations. E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



 $P (R-PDIP-T8)$ 

PLASTIC DUAL-IN-LINE PACKAGE



- B. This drawing is subject to change without notice.
- C. Falls within JEDEC MS-001 variation BA.



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