

## LCD Bias With Digital VCOM Buffer for Notebook PCs and Tablet PCs

Check for Samples: [TPS65640](#)

### FEATURES

- 2.5-V to 5.5-V Input Voltage Range
- 3.6 to 12.7 V Boost Converter ( $AV_{DD}$ )
- 15 to 37 V Boost Converter with Temperature Compensation ( $V_{GH}$ )
- –8 V to –3.8 V Linear Negative Voltage Regulator ( $V_{GL}$  or  $NAV_{DD}$ )
- 1.5-V to 3-V Alternative Buck Converter or Low Dropout Regulator ( $V_{25}$ )
- 7 bits Programmable  $V_{COM}$  Calibrator With One Integrated Buffer Amplifiers
- 0.8 V to 5.1 V Programmable  $V_{COM}$  Voltage Output for Full  $AV_{DD}$  Application
- –4.1 V to 0.2 V Programmable  $V_{COM}$  Voltage Output for Positive and Negative  $AV_{DD}$  Application
- Two Operational Amplifiers
- Gate Voltage Shaping
- Programmable  $V_{GH}$  and  $V_{COM}$  Temperature Compensation
- $T_{CON}$  Reset Signal Generator With Programmable Delay
- I<sup>2</sup>C Interface for E<sup>2</sup>PROM Programming
- Thermal Shutdown
- Supports GIP and Non-GIP Displays
- 28 Pins, 5.5-mm × 3.5-mm 0.5-mm Pitch QFN

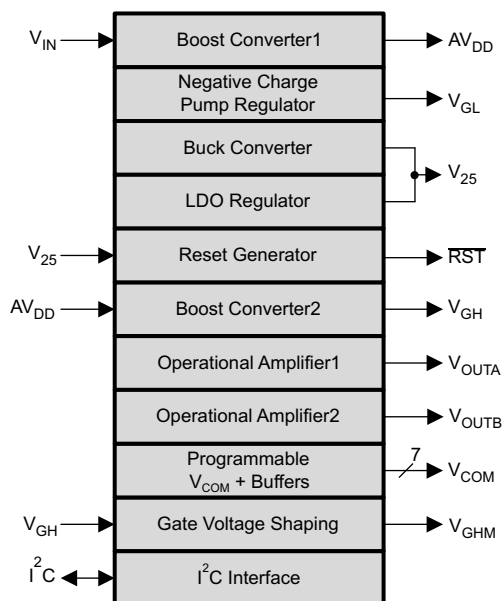
### APPLICATIONS

- Notebook PCs
- Tablet PCs

### DESCRIPTION

The TPS65640 is a compact LCD bias solution primarily intended for use in notebook and tablet PCs. The device comprises two boost converters to supply the LCD panel's source driver and gate driver or level shifter; one buck converters or a LDO regulator alternatively to supply the time controller logic voltages; a linear negative voltage regulator to supply gate off voltage or provide negative voltage for source driver; a programmable VCOM generator with one high-speed amplifier; a gate voltage shaping function and two high speed operational amplifiers.

All the regulators and  $V_{COM}$  voltage outputs are programmed through I<sup>2</sup>C interface and stored in the TPS65640 integrated E<sup>2</sup>PROM. The TPS65640 is available in 5.5-mm × 3.5-mm, 28-lead QFN package.



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### ORDERING INFORMATION<sup>(1)</sup>

T <sub>A</sub>	ORDERING	PACKAGE	PACKAGE MARKING
-40°C to 85°C	TPS65640	5.5-mm x 3.5-mm 28-pin QFN	PZXI

(1) The device is supplied taped and reeled, with 3000 devices per reel.

### ABSOLUTE MAXIMUM RATINGS<sup>(1)</sup>

over operating free-air temperature range (unless otherwise noted)

		VALUE		UNIT
		MIN	MAX	
Pin Voltage <sup>(2)</sup>	VIN, V25, V25_LX, RESET, COMP, SCL, SDA, VFLK, VT	-0.3	7	V
	VIN (100ms) Pulse	-0.3	12	V
	AVDD, LX	-0.3	20	V
	VCOM_OUT, INA+, INA-, OUTA, INB+, INB-, OUTB	-5	5	V
	VGH_LX, VGH, VGHM, RE	-0.3	40	V
	DRVN, VGL, NAVDD	-12	0.3	V
ESD Rating <sup>(3)</sup>	Human Body Model		2000	V
	Machine Model		200	V
	Charged Device Model		700	V
T <sub>A</sub>	Ambient temperature	-40	85	°C
T <sub>J</sub>	Junction temperature	-40	150	°C
T <sub>STG</sub>	Storage temperature	-65	150	°C

- (1) Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.
- (3) ESD testing is performed according to the respective JEDEC standard.

### THERMAL INFORMATION

THERMAL METRIC <sup>(1)</sup>		TPS65640	UNITS
		RHR	
		28 PINS	
θ <sub>JA</sub>	Junction-to-ambient thermal resistance <sup>(2)</sup>	37.4	°C/W
θ <sub>JCtop</sub>	Junction-to-case (top) thermal resistance <sup>(3)</sup>	26.3	
θ <sub>JB</sub>	Junction-to-board thermal resistance <sup>(4)</sup>	8.3	
ψ <sub>JT</sub>	Junction-to-top characterization parameter <sup>(5)</sup>	0.2	
ψ <sub>JB</sub>	Junction-to-board characterization parameter <sup>(6)</sup>	8.1	
θ <sub>JCbot</sub>	Junction-to-case (bottom) thermal resistance <sup>(7)</sup>	1.2	

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).
- (2) The junction-to-ambient thermal resistance under natural convection is obtained in a simulation on a JEDEC-standard, high-K board, as specified in JESD51-7, in an environment described in JESD51-2a.
- (3) The junction-to-case (top) thermal resistance is obtained by simulating a cold plate test on the package top. No specific JEDEC standard test exists, but a close description can be found in the ANSI SEMI standard G30-88.
- (4) The junction-to-board thermal resistance is obtained by simulating in an environment with a ring cold plate fixture to control the PCB temperature, as described in JESD51-8.
- (5) The junction-to-top characterization parameter, ψ<sub>JT</sub>, estimates the junction temperature of a device in a real system and is extracted from the simulation data for obtaining θ<sub>JA</sub>, using a procedure described in JESD51-2a (sections 6 and 7).
- (6) The junction-to-board characterization parameter, ψ<sub>JB</sub>, estimates the junction temperature of a device in a real system and is extracted from the simulation data for obtaining θ<sub>JA</sub>, using a procedure described in JESD51-2a (sections 6 and 7).
- (7) The junction-to-case (bottom) thermal resistance is obtained by simulating a cold plate test on the exposed (power) pad. No specific JEDEC standard test exists, but a close description can be found in the ANSI SEMI standard G30-88.

## RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

		MIN	TYP	MAX	UNIT
V <sub>IN</sub>	Input voltage range	2.5		5.5	V
<b>BOOST CONVERTER 1</b>					
AV <sub>DD</sub>	Boost converter 1 output voltage range	3.6		11	V
I <sub>AVDD</sub>	Boost converter 1 output current when 5.5 V ≥ VIN ≥ 2.5 V			400	mA
L <sub>1</sub>	Boost converter #1 inductor range	4.7		10	μH
C <sub>OUT1</sub>	Boost converter #1 output capacitance	10			μF
<b>BOOST CONVERTER 2</b>					
AV <sub>DD</sub>	Input voltage range	3.6		11 <sup>(1)</sup>	V
V <sub>GH</sub>	Output voltage range	15		37	V
I <sub>GH</sub>	Output current		15	40	mA
L <sub>4</sub>	Inductor	4.7	10	10	μH
C <sub>OUT4</sub>	Output capacitance	1	2.2		μF
R <sub>NTC</sub>	Thermistor resistance at 25 °C		10		kΩ
<b>BUCK CONVERTER (V<sub>25</sub>)</b>					
V <sub>25</sub>	Output voltage	1.5		3	V
I <sub>25</sub>	Output current			600	mA
L <sub>2</sub>	Inductor	2.2	4.7	10	μH
C <sub>OUT2</sub>	Output capacitance	4.7	10	22	μF
<b>LDO Regulator (V<sub>25</sub>)</b>					
V <sub>25</sub>	Output voltage	1.5		3	V
I <sub>25</sub>	Output current			350	mA
C <sub>OUT2</sub>	Output capacitance	1	4.7		μF

 (1) V<sub>GH</sub> – AV<sub>DD</sub> must be greater than 6 volts.

## ELECTRICAL CHARACTERISTICS

 V<sub>IN</sub> = 3.3 V; V<sub>25</sub> = 2.5 V, AV<sub>DD</sub> = 8.5 V, V<sub>GH</sub> = 23 V, V<sub>GL</sub> = –6 V, R<sub>CAMP</sub> = 200kΩ, C<sub>CAMP</sub> = 1 nF, NAV<sub>DD</sub> = AGND = PGND = 0V, T<sub>A</sub> = –40 °C to 85 °C. Typical values are at 25°C (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>POWER SUPPLY</b>						
I <sub>IN</sub>	Supply current into VIN	Converters not switching		2	3	mA
	Supply current into AVDD	No load on op-amp outputs		5	8.5	mA
	Supply current into VGH	No load on V <sub>GHM</sub>		0.1	1	mA
<b>UNDER VOLTAGE LOCKOUT</b>						
V <sub>UVLO</sub>	Undervoltage lockout threshold	V <sub>IN</sub> rising	2.3	2.35	2.4	V
		V <sub>IN</sub> falling T <sub>A</sub> = 25°C	2.05	2.2	2.25	
	Hysteresis	V <sub>IN</sub> rising – V <sub>IN</sub> falling		0.15		
<b>BOOST CONVERTER 1 (AV<sub>DD</sub>)</b>						
AV <sub>DD</sub>	Output voltage range		3.6		11	V
	Tolerance		–2%		2%	
V <sub>UVP1</sub>	Undervoltage threshold	AV <sub>DD</sub> falling	75	80	85	% of AV <sub>DD</sub>
T <sub>DLY_UVP1</sub>				160		ms
V <sub>SCP1</sub>	Short circuit threshold	AV <sub>DD</sub> falling	25	30	35	%
V <sub>OV1</sub>	Over Voltage threshold	AV <sub>DD</sub> rising	14.5	15	16	V
I <sub>LK1</sub>	Switch leakage current	AV <sub>DD</sub> = 13.5 V		10	20	μA
r <sub>DS(ON)1</sub>	Switch ON resistance	I <sub>LX</sub> = 1 A		0.2	0.3	Ω
I <sub>LIM1</sub>	AVDD switch current limit	AVDD ILIM = 0, T <sub>A</sub> = 25 °C	0.8	1	1.2	A
		AVDD ILIM = 1, T <sub>A</sub> = 25 °C	1.6	2	2.4	

**ELECTRICAL CHARACTERISTICS (continued)**

$V_{IN} = 3.3\text{ V}$ ;  $V_{25} = 2.5\text{ V}$ ,  $AV_{DD} = 8.5\text{ V}$ ,  $V_{GH} = 23\text{ V}$ ,  $V_{GL} = -6\text{ V}$ ,  $R_{CAMP} = 200\text{ k}\Omega$ ,  $C_{CAMP} = 1\text{ nF}$ ,  $NAV_{DD} = AGND = PGND = 0\text{ V}$ ,  $T_A = -40\text{ }^\circ\text{C}$  to  $85\text{ }^\circ\text{C}$ . Typical values are at  $25\text{ }^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
$D_{MAX1}$	Maximum Duty Cycle	<b>FREQ1</b> = 01	80%				
$f_{SW1}$	Oscillator frequency	<b>FREQ1</b> = 00, $T_A = 25\text{ }^\circ\text{C}$	480	600	720	kHz	
		<b>FREQ1</b> = 01, $T_A = 25\text{ }^\circ\text{C}$	600	750	900		
		<b>FREQ1</b> = 10, $T_A = 25\text{ }^\circ\text{C}$	720	900	1080		
		<b>FREQ1</b> = 11, $T_A = 25\text{ }^\circ\text{C}$	800	1000	1200		
$V_{LIR1}$	Line regulation, $V_{LIR} = \Delta AV_{DD} / (AV_{DD} \times \Delta V_{IN})$	$V_{IN} = 2.5\text{ V}$ to $5.5\text{ V}$ , $AV_{DD} = 8.5\text{ V}$ , $T_A = 25\text{ }^\circ\text{C}$	$\pm 0.1$			$\pm 0.15$	%/V
$V_{LOR1}$	Load regulation, $V_{LOR} = (AV_{DD\_20mA} - AV_{DD\_200mA}) / AV_{DD\_20mA}$	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 8.5\text{ V}$ , $I_{AVDD} = 20\text{ mA}$ to $200\text{ mA}$	1				%/A
$V_{SS1}$	$AV_{DD}$ soft stat duration	<b>SS1</b> = 00	20			ms	
		<b>SS1</b> = 01	40				
		<b>SS1</b> = 10	60				
		<b>SS1</b> = 11	80				
$T_{f1}$	$AV_{DD}$ switch ON voltage slew rate	<b>LX1TS</b> = 00	0.5			V/ns	
		<b>LX1TS</b> = 01	0.7				
		<b>LX1TS</b> = 10	0.9				
		<b>LX1TS</b> = 11	1.1				
<b>BUCK CONVERTER (<math>V_{25Buck}</math>)</b>							
$V_{25Buck}$	Output voltage		1.5	3		V	
	Tolerance	$(V_{25} - V_{25\_setting}) / V_{25\_setting}$	-2%	2%			
$V_{UVP2}$	Undervoltage threshold	$V_{25}$ falling	0.8	1	1.2	V	
	Hysteresis	$V_{25}$ rising	0.1				
$T_{DLY\_UVP2}$			160			ms	
$I_{LIM2}$	Switch current limit	$I_{SW2A}$ ramps from 0 A to 2 A	1	1.2	1.4	A	
$T_{SS2}$	Soft start duration		4			ms	
$r_{DS(ON)2A}$	Switch ON resistance	High-side, $I_{SW2A} = I_{LIM2}$	250		450	m $\Omega$	
$r_{DS(ON)2B}$		Low-side, $I_{SW2B} = 1\text{ A}$	100		200		
$f_{SW2}$	Switching frequency	$V_{IN} = 3.3\text{ V}$ ; $V_{25} = 2.5\text{ V}$ , $I_{25} = 200\text{ mA}$	1000	1250	1500	kHz	
$V_{LIR2}$	Line regulation, $V_{LIR} = \Delta V_{25} / (AV_{25} \times \Delta V_{IN})$	$V_{IN} = 2.5\text{ V}$ to $5.5\text{ V}$	$\pm 0.1$			$\pm 0.15$	%/V
$V_{LOR2}$	Load regulation	$V_{IN} = 3.3\text{ V}$ , $I_{25} = 1\text{ mA}$ to $400\text{ mA}$	1%				
<b>LINEAR REGULATOR (<math>V_{25LDO}</math>)</b>							
$V_{25LDO}$	Output voltage		1.5	3.0		V	
	Tolerance		-2.5%	2.5%			
$V_{UVP3}$	Undervoltage threshold	$V_{25}$ falling	0.8	1	1.2	V	
	Hysteresis	$V_{25}$ rising	0.1				
$T_{DLY\_UVP3}$			160			ms	
$V_{DO3}$	Dropout voltage	$I_{25} = 350\text{ mA}$ , $V_{25} = -3\%$	300	500		mV	
$V_{LIR3}$	Line regulation, $V_{LIR} = \Delta V_{25} / (V_{25} \times \Delta V_{IN})$	$V_{IN} = 2.8\text{ V}$ to $5.5\text{ V}$ , $I_{25} = 100\text{ mA}$	0.1			$\pm 0.15$	%/V
$V_{LOR3}$	Load regulation	$V_{IN} = 3.3\text{ V}$ , $I_{25} = 1\text{ mA}$ to $300\text{ mA}$	1				%/A
<b>BOOST CONVERTER 2 (<math>V_{GH}</math>)</b>							
$V_{GH}$	Output voltage range		15	37		V	
	Tolerance		-3%	3%			
$V_{OVP4}$	Overvoltage threshold	$T_A = 25\text{ }^\circ\text{C}$	38	39	40	V	
$V_{UVP4}$	Undervoltage threshold	$V_{GH}$ falling	75	80	85	% of $V_{GH}$	
$T_{DLY\_UVP4}$	Undervoltage protection shutdown delay		160			ms	
$I_{LK4}$	Switch leakage current	Switching off $V_{VGH\_LX} = 38\text{ V}$	10			20	$\mu\text{A}$

**ELECTRICAL CHARACTERISTICS (continued)**

$V_{IN} = 3.3\text{ V}$ ;  $V_{25} = 2.5\text{ V}$ ,  $AV_{DD} = 8.5\text{ V}$ ,  $V_{GH} = 23\text{ V}$ ,  $V_{GL} = -6\text{ V}$ ,  $R_{CAMP} = 200\text{ k}\Omega$ ,  $C_{CAMP} = 1\text{ nF}$ ,  $NAV_{DD} = AGND = PGND = 0\text{ V}$ ,  $T_A = -40\text{ }^\circ\text{C}$  to  $85\text{ }^\circ\text{C}$ . Typical values are at  $25\text{ }^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$f_{SW4}$	VGH swithching frequency	<b>FREQ4</b> = 0	300	400	500	kHz
		<b>FREQ4</b> = 1	600	800	1000	
$r_{DS(ON)4}$	VGH switch ON resistance	$I_{VGH\_LX} = 1\text{ A}$		0.5	1	$\Omega$
$I_{LIM4}$	VGH switch current limit		0.9	1.2	1.5	A
$T_{SS4}$	VGH soft start duration	<b>SS4</b> = 00		4		ms
		<b>SS4</b> = 01		8		
		<b>SS4</b> = 10		12		
		<b>SS4</b> = 11		16		
$D_{MAX4}$			88%	90%		
$I_{VT}$	Thermistor reference current	$V_{VT} = 1\text{ V}$		40		$\mu\text{A}$
$V_{LIR4}$	Line regulation	$AV_{DD} = 3.6\text{ V}$ to $11\text{ V}$		$\pm 0.1$	$\pm 0.15$	%/V
$V_{LOR4}$	Load regulation	$I_{GH} = 5\text{ mA}$ to $40\text{ mA}$		1		%/A
<b>PROGRAMMABLE <math>V_{COM}</math> CALIBRATOR</b>						
$V_{S+} - V_{S-}$	VCOM buffer supply voltage				15	V
$V_{COM}$	VCOM voltage accuracy, $V_{COM} - V_{COM\_setting}$	$I_{OUT} = 0\text{ mA}$	-6		6	LSB
		Load regulation		1	2	V/A
$I_{SC2}$	Short circuit current	$AV_{DD} = 8.5\text{ V}$ , $NAV_{DD} = 0\text{ V}$ , $V_{COM\_OUT} = AV_{DD} / 2$ , $I_{SOURCE} = 1\text{ mA}$ to $20\text{ mA}$		1	2	mA
		$AV_{DD} = 5\text{ V}$ , $NAV_{DD} = -5\text{ V}$ , $V_{COM\_OUT} = 0\text{ V}$ , $I_{SOURCE} = 1\text{ mA}$ to $20\text{ mA}$		1	2	
		$AV_{DD} = 8.5\text{ V}$ , $NAV_{DD} = 0\text{ V}$ , $V_{COM\_OUT} = AV_{DD} / 2$ , $I_{SINK} = -1\text{ mA}$ to $-20\text{ mA}$		1	2	
		$AV_{DD} = 5\text{ V}$ , $NAV_{DD} = -5\text{ V}$ , $V_{COM\_OUT} = 0\text{ V}$ , $I_{SINK} = -1\text{ mA}$ to $-20\text{ mA}$		1	2	
$SR_2$	Slew rate	$AV_{DD} = 5\text{ V}$ , $V_{COM\_OUT} = AV_{DD}$ , $NAV_{DD} = -5\text{ V}$		-200		mA
		$AV_{DD} = 5\text{ V}$ , $V_{COM\_OUT} = NAV_{DD} = -5\text{ V}$		200		
$BW_2$	Small signal 3dB bandwidth	$V_{COM\_OUT} = AV_{DD} / 2 + 1\text{ V}$		12		V/ $\mu\text{s}$
$BW_2$	Small signal 3dB bandwidth	$V_{COM\_OUT} = AV_{DD} / 2$ , $V_{SIGNAL} = 60\text{ mV}_{PP}$ , no load		12		MHz
<b>OPERATIONAL AMPLIFIER 1 and 2 (<math>AV_{DD} = 5\text{ V}</math>, <math>NAV_{DD} = -5\text{ V}</math>, <math>R_L = 10\text{ k}\Omega</math>, <math>C_L = 10\text{ pF}</math>, <math>T_A = 25\text{ }^\circ\text{C}</math>)</b>						
$V_{IO1}$	Input offset voltage	$V_{CM} = (AV_{DD} + NAV_{DD}) / 2$	-15		15	mV
$\Delta V_{IO} / \Delta T$	Average offset voltage drift	$T_A = -40\text{ }^\circ\text{C}$ to $85\text{ }^\circ\text{C}$		5		$\mu\text{V}/^\circ\text{C}$
$R_{IN1}$	Input impedance			1		G $\Omega$
$C_{IN1}$	Input capacitance			1.35		pF
$V_{CM1}$	Input common mode voltage range	$AV_{DD} = 5\text{ V}$ , $NAV_{DD} = -5\text{ V}$	-4		3	V
$A_{VOL1}$	Open loop gain	$V_{CM} = (AV_{DD} + NAV_{DD}) / 2$	75	95		dB
$PSRR_1$	Power supply rejection ratio	$V_{CM} = (AV_{DD} + NAV_{DD}) / 2$	60	70		dB
$CMRR_1$	Common mode rejection ration	$V_{CM} = (AV_{DD} + NAV_{DD}) / 2$	50	80		dB
$V_{OL1}$	Output swing low	$I_L = 5\text{ mA}$		4.85	4.92	V
$V_{OH1}$	Output swing High	$I_L = -5\text{ mA}$	-4.92	-485		V
$I_{OC1}$	Continuous output current			$\pm 35$		mA
$I_{PK1}$	Peak output current	$V_{IN+} = (AV_{DD} + NAV_{DD}) / 2$ , $V_{IN-} = (AV_{DD} + NAV_{DD}) / 2 \pm 1\text{ V}$ , open-loop	$\pm 120$			mA
tS	Setting to $\pm 0.1\%$	$A_V = -1$ , $V_{IN-} = (AV_{DD} + NAV_{DD}) / 2 \pm 1\text{ V}$		500		ns
$SR_1$	Slew rate	$A_V = -1$ , $V_{IN-} = (AV_{DD} + NAV_{DD}) / 2 \pm 1\text{ V}$		12		V/ $\mu\text{s}$
$BW_1$	Small signal 3 dB bandwidth	$A_V = -1$ , $V_{CM} = (AV_{DD} + NAV_{DD}) / 2$ , $V_{SIGNAL} = 60\text{ mV}_{PP}$		5		MHz
PM	Phase margin			50		Degree
CS	Channel Separation	$A_V = -1$ , $V_{CM} = (AV_{DD} + NAV_{DD}) / 2$ , $V_{SIGNAL} = 60\text{ mV}_{PP}$ , $f = 5\text{ MHz}$		75		dB
<b>GATE OFF REGULATION CONTROLLER (<math>V_{GL}</math>)</b>						

**ELECTRICAL CHARACTERISTICS (continued)**

$V_{IN} = 3.3\text{ V}$ ;  $V_{25} = 2.5\text{ V}$ ,  $AV_{DD} = 8.5\text{ V}$ ,  $V_{GH} = 23\text{ V}$ ,  $V_{GL} = -6\text{ V}$ ,  $R_{CAMP} = 200\text{ k}\Omega$ ,  $C_{CAMP} = 1\text{ nF}$ ,  $NAV_{DD} = AGND = PGND = 0\text{ V}$ ,  $T_A = -40\text{ }^\circ\text{C}$  to  $85\text{ }^\circ\text{C}$ . Typical values are at  $25\text{ }^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$V_{GL}$	$V_{GL}$ voltage regulate accuracy	Output voltage	-3.8		-8	V
		Tolerance	-3%		3%	
$I_{DRVN}$	DRVN source current		1	4	6	mA
$V_{LIR5}$	Line regulation	$I_{DRVN} = 1\text{ mA}$ , $V_{IN} = 2.5\text{ V}$ to $5.5\text{ V}$		1	6	mV
<b>GATE VOLTAGE SHAPING</b>						
$r_{DS(ON)H}$	VGH to VGHM ON resistance	$V_{GH} = 24\text{ V}$ , $I_{GHM} = 10\text{ mA}$ , $V_{FLK} = 2.5\text{ V}$		13	25	$\Omega$
$r_{DS(ON)L}$	VGHM to RE ON resistance	$V_{GHM} = 24\text{ V}$ , $I_{GHM} = 10\text{ mA}$ , $V_{FLK} = 0\text{ V}$		13	25	$\Omega$
$V_{IH}$	High-level input voltage	$V_{FLK}$ rising	1.5			V
$V_{IL}$	Low-level input voltage	$V_{FLK}$ falling			0.6	V
$t_{PLH}$	Propagation delay	$V_{GHM}$ rising, $2.5\text{ V}$ , 50% thresholds, $C_{OUT} = 150\text{ pF}$ , $R_E = 0\text{ m}\Omega$		100	200	ns
$t_{PHL}$		$V_{GHM}$ falling, $2.5\text{ V}$ , 50% thresholds, $C_{OUT} = 150\text{ pF}$ , $R_E = 0\text{ m}\Omega$		100	200	
$t_{DLY}$	Gate voltage shaping / LCD bias ready delay range	<b>DLY</b> = 00		0		ms
		<b>DLY</b> = 01		20		
		<b>DLY</b> = 10		40		
		<b>DLY</b> = 11		60		
<b>T<sub>CON</sub> RESET GENERATOR</b>						
$V_{DIV}$	Detecting voltage falling threshold	<b>VDIV</b> = 000	1.08	1.2	1.32	V
		<b>VDIV</b> = 001	1.26	1.4	1.54	
		<b>VDIV</b> = 010	1.44	1.6	1.76	
		<b>VDIV</b> = 011	1.62	1.8	1.98	
		<b>VDIV</b> = 100	1.8	2	2.2	
		<b>VDIV</b> = 101	1.98	2.2	2.42	
		<b>VDIV</b> = 110	2.16	2.4	2.64	
		<b>VDIV</b> = 111	2.34	2.6	2.86	
	Hysteresis			150		mV
$V_{OL(RST)}$	Output voltage	$I_{RST} = 1\text{ mA}$ (sinking)			0.5	V
$I_{LK(RST)}$	Leakage current	$V_{RST} = 2.5\text{ V}$			1	$\mu\text{A}$
$t_{RESET}^{(1)}$	Reset delay time	<b>RESET</b> = 0000		0		ms
		...		...		
		<b>RESET</b> = 1111		30		
<b>THERMAL SHUTDOWN</b>						
$T_{SD}$	Thermal shutdown temperature	$T_J$ rising		150		$^\circ\text{C}$
<b>I<sup>2</sup>C INTERFACE</b>						
ADDR	Configuration parameters slave address			E8		
	Programmable $V_{COM}$ slave address			9E		
$V_{IL}$	Low level input voltage	Supply = $2.5\text{ V}$ , $V_{IN}$ falling, standard and fast modes			$0.3 \times V_{25}$	V
$V_{IH}$	High level input voltage	Supply = $2.5\text{ V}$ , $V_{IN}$ rising, standard and fast <sup>4</sup> modes	$0.7 \times V_{25}$			V
$V_{HYS}$	Hysteresis	Supply = $2.5\text{ V}$ , applicable to fast mode only	125			mV
$V_{OL}$	Low level output voltage	Sinking $3\text{ mA}$			500	mV
$C_I$	Input capacitance				10	pF
$f_{SCL}$	Clock frequency	Standard mode			100	kHz
		Fast mode			400	
$t_{LOW}$	Clock low period	Standard mode	4.7			$\mu\text{s}$
		Fast mode	1.3			
$t_{HIGH}$	Clock high period	Standard mode	4			$\mu\text{s}$
		Fast mode	0.6			

(1) Refer to [Table 12](#) for RESET time delay break down.

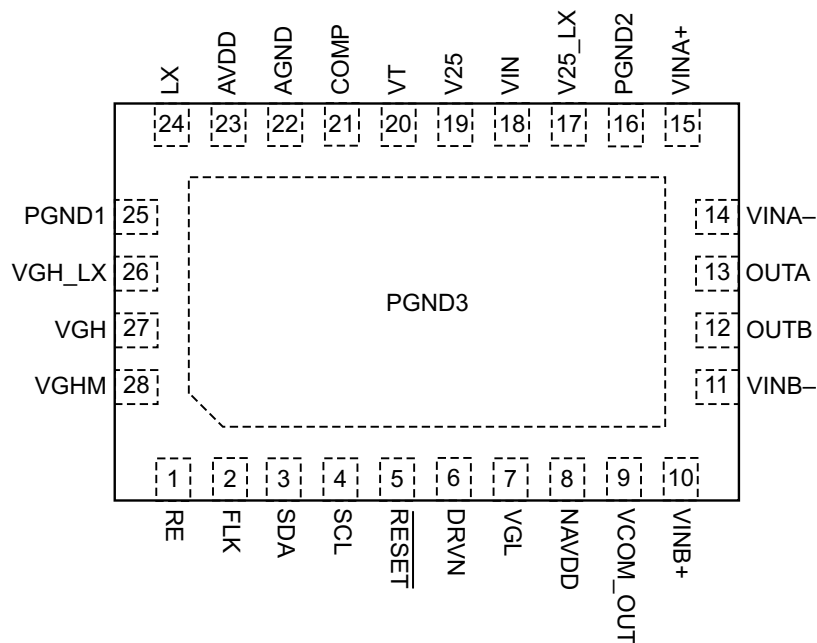
**ELECTRICAL CHARACTERISTICS (continued)**

$V_{IN} = 3.3\text{ V}$ ;  $V_{25} = 2.5\text{ V}$ ,  $AV_{DD} = 8.5\text{ V}$ ,  $V_{GH} = 23\text{ V}$ ,  $V_{GL} = -6\text{ V}$ ,  $R_{CAMP} = 200\text{ k}\Omega$ ,  $C_{CAMP} = 1\text{ nF}$ ,  $NAV_{DD} = AGND = PGND = 0\text{ V}$ ,  
 $T_A = -40\text{ }^\circ\text{C}$  to  $85\text{ }^\circ\text{C}$ . Typical values are at  $25\text{ }^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{BUF}$	Bus free time between a STOP and a START condition	Standard mode	4.7			$\mu\text{s}$
		Fast mode	1.3			
$t_{hd:STA}$	Hold time for a repeated START condition	Standard mode	4			$\mu\text{s}$
		Fast mode	0.6			
$t_{su:STA}$	Set-up time for a repeated START condition	Standard mode	4			$\mu\text{s}$
		Fast mode	0.6			
$t_{su:DAT}$	Data set-up time	Standard mode	250			ns
		Fast mode	100			
$t_{hd:DAT}$	Data hold time	Standard mode	0.05		3.45	$\mu\text{s}$
		Fast mode	0.05		0.9	
$t_{RCL1}$	Rise time of SCL after a repeated START condition and after an ACK bit	Standard mode	20 + $0.1C_B$		1000	ns
		Fast mode	20 + $0.1C_B$		1000	
$t_{RCL}$	Rise time of SCL	Standard mode	20 + $0.1C_B$		1000	ns
		Fast mode	20 + $0.1C_B$		300	
$t_{FCL}$	Fall time of SCL	Standard mode	20 + $0.1C_B$		300	ns
		Fast mode	20 + $0.1C_B$		300	
$t_{RDA}$	Rise time of SDA	Standard mode	20 + $0.1C_B$		1000	ns
		Fast mode	20 + $0.1C_B$		300	
$t_{FDA}$	Fall time of SDA	Standard mode	20 + $0.1C_B$		300	ns
		Fast mode	20 + $0.1C_B$		300	
$t_{su:STO}$	Set-up time for STOP condition	Standard mode	4			$\mu\text{s}$
		Fast mode	0.6			
$C_B$	Capacitive load on SDA and SCL	Standard mode			400	pF
		Fast mode			400	
<b>E<sup>2</sup>PROM</b>						
$N_{WRITE}$	Number of write cycles		1000			
$t_{WRITE}$	Write time				100	ms
	Data retention	Storage temperature = $150\text{ }^\circ\text{C}$	100000			hrs

## DEVICE INFORMATION

### PIN ASSIGNMENT 28 PIN 5.5mm x 3.5mm RHR PACKAGE TOP VIEW



### PIN FUNCTIONS

PIN		TYPE	DESCRIPTION
NAME	NO.		
AGND	22	P	Ground
AVDD	23	I	AVDD sense pin
COMP	21	O	Boost converter 1 compensation. Connect a suitable compensation network (typically a series R-C combination) between this pin and ground
DRVN	6	O	Drive output for negative linear regulator
FLK	2	I	Gate voltage shaping flicker clock input
LX	24	P	Boost convert 1 switch node
NAVDD	8	I	Negative AVDD voltage input
OUTA	13	O	Operational amplifier A output
OUTB	12	O	Operational amplifier B output
PGND1	25	P	Power Ground 1 for boost converter 2
PGND2	16	P	Power Ground 2 for buck converter
PGND3	29	P	Power Ground 3 for boost converter 1
RE	1	O	Gate voltage shaping discharge resistor connection
RESET	5	O	T-CON reset output
SCL	4	I	I <sup>2</sup> C Interface serial clock
SDA	3	I/O	I <sup>2</sup> C Interface serial data
VCOM_OUT	9	O	VCOM amplifier output
VGH	27	P	Gate voltage shaping input and boost converter 2 output sense
VGH_LX	26	P	Boost converter 2 switch node
VGHM	28	O	Gate voltage shaping output
VGL	7	I	Negative linear regulator sense pin
VIN	18	P	Supply voltage



**PIN FUNCTIONS (continued)**

PIN		TYPE	DESCRIPTION
NAME	NO.		
VINA+	15	I	Operational amplifier B non-inverting input
VINA–	14	I	Operational amplifier A inverting input
VINB+	10	I	Operational amplifier B non-inverting input
VINB–	11	I	Operational amplifier B inverting input
VT	20	I	Boost converter 2 and V <sub>COM</sub> reference external thermistor network connection
V25	19	O	Buck converter or LDO regulator output sense
V25_LX	17	P	Buck converter switch node or LDO regulator output

## TYPICAL CHARACTERISTICS

## TABLE OF GRAPHS

PARAMETER	CONDITIONS	FIGURE
<b>BOOSTER CONVERTER 1</b>		
Efficiency vs. Load Current	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ and $8.5\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $f_{SW} = 1\text{ MHz}$	<a href="#">Figure 1</a>
Output Voltage Ripple	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $I_{AVDD} = 200\text{ mA}$ , $f_{SW} = 1\text{ MHz}$	<a href="#">Figure 2</a>
Load Transient Response	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $I_{AVDD} = 20\text{ mA}$ to $200\text{ mA}$	<a href="#">Figure 3</a>
Startup	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $f_{SW} = 1\text{ MHz}$ , $I_{LOAD} = 55\text{ }\Omega$	<a href="#">Figure 4</a>
Over Voltage Protection	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $f_{SW} = 1\text{ MHz}$	<a href="#">Figure 5</a>
Under Voltage Protection	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $f_{SW} = 1\text{ MHz}$	<a href="#">Figure 6</a>
<b>BUCK CONVERTER</b>		
Efficiency vs. Load Current	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 1.8\text{ V}$ and $2.5\text{ V}$	<a href="#">Figure 7</a>
Output Voltage Ripple	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$ , $I_{V25} = 600\text{ mA}$	<a href="#">Figure 8</a>
Load Transient Response	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$ , $I_{V25} = 20$ to $200\text{ mA}$	<a href="#">Figure 9</a>
Startup	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$ , $I_{LOAD} = 12.5\text{ }\Omega$	<a href="#">Figure 10</a>
Undervoltage Protection	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$	<a href="#">Figure 11</a>
<b>LDO VOLTAGE REGULATOR</b>		
Load Transient Response	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$ , $I_{V25} = 20$ to $200\text{ mA}$	<a href="#">Figure 12</a>
Startup	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$ , $I_{LOAD} = 12.5\text{ }\Omega$	<a href="#">Figure 13</a>
Undervoltage Protection	$V_{IN} = 3.3\text{ V}$ , $V_{25} = 2.5\text{ V}$	<a href="#">Figure 14</a>
<b>BOOST CONVERTER 2</b>		
Efficiency vs. Load Current	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $f_{SW} = 800\text{ kHz}$	<a href="#">Figure 15</a>
Efficiency vs. Load Current	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 8.5\text{ V}$ , $V_{GH} = 25\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $f_{SW} = 800\text{ kHz}$	<a href="#">Figure 16</a>
Output Voltage Ripple	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $I_{VGH} = 50\text{ mA}$ , $f_{SW} = 800\text{ kHz}$	<a href="#">Figure 17</a>
Load Transient Response	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $I_{VGH} = 10$ to $50\text{ mA}$	<a href="#">Figure 18</a>
Startup	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $f_{SW} = 800\text{ kHz}$	<a href="#">Figure 19</a>
Under Voltage Protection	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $L = 10\text{ }\mu\text{H}$ , $f_{SW} = 800\text{ kHz}$	<a href="#">Figure 20</a>
<b>NEGATIVE CHARGE PUMP REGULATOR CONTROL</b>		
Output Voltage Ripple	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GL} = -4.5\text{ V}$ , $I_{GL} = 50\text{ mA}$	<a href="#">Figure 21</a>
Load Transient Response	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GL} = -4.5\text{ V}$ , $I_{GL} = 10$ to $50\text{ mA}$	<a href="#">Figure 22</a>
<b>GATE VOLTAGE SHAPING</b>	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5\text{ V}$ , $AV_{DD} = 5\text{ V}$ ,	<a href="#">Figure 23</a>
<b>OPERATIONAL AMPLIFIER SLEW RATE</b>	$V_{IN} = 3.3\text{ V}$ , $V_{GH} = 16\text{ V}$ , $NAV_{DD} = -5\text{ V}$ , $INA+ = -1\text{ V}$ to $1\text{ V}$	<a href="#">Figure 24</a>
<b>POWER ON SEQUENCY</b>	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $V_{GL} = -4.5\text{ V}$	<a href="#">Figure 25</a>
<b>POWER OFF SEQUENCY</b>	$V_{IN} = 3.3\text{ V}$ , $AV_{DD} = 5.5\text{ V}$ , $V_{GH} = 16\text{ V}$ , $V_{GL} = -4.5\text{ V}$	<a href="#">Figure 26</a>

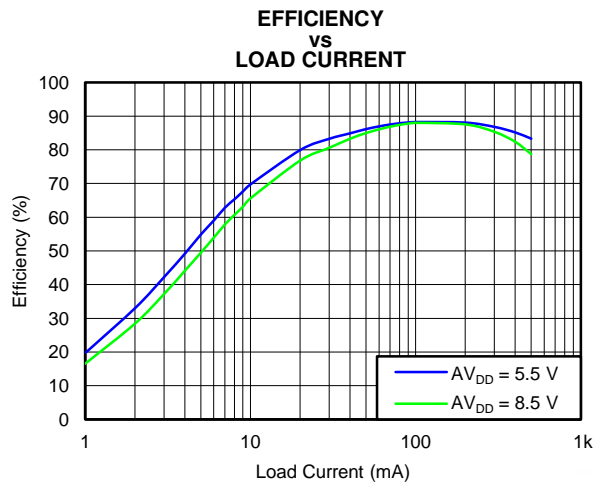


Figure 1. Boost Converter 1 Efficiency

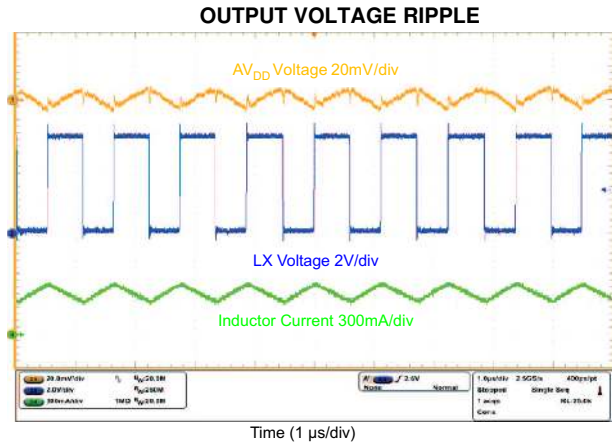


Figure 2. Boost Converter 1 Output Ripple

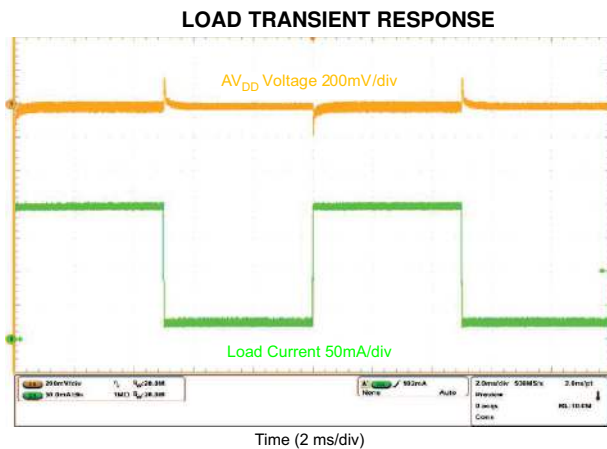


Figure 3. Boost Converter 1 Load Transient Response

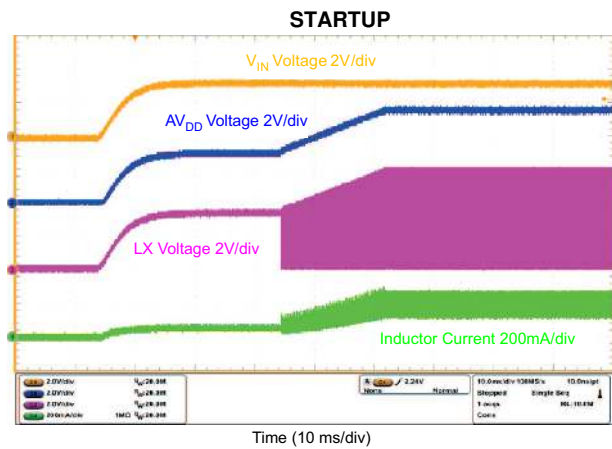


Figure 4. Boost Converter 1 Startup

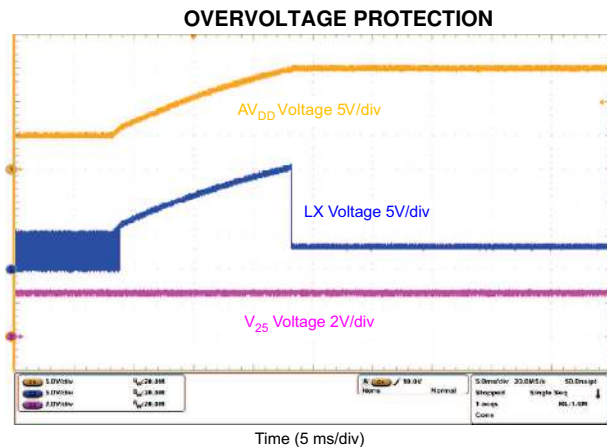


Figure 5. Boost Converter 1 Overvoltage Protection

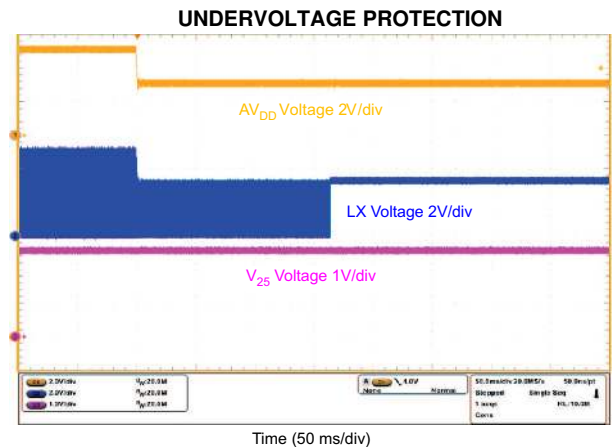


Figure 6. Boost Converter 1 Undervoltage Protection

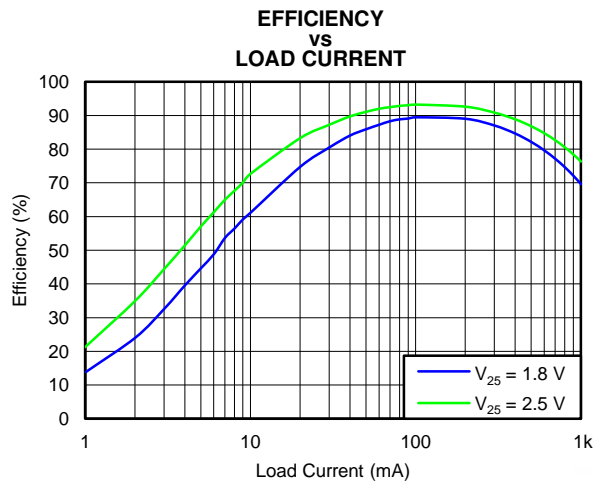


Figure 7. Buck Converter Efficiency

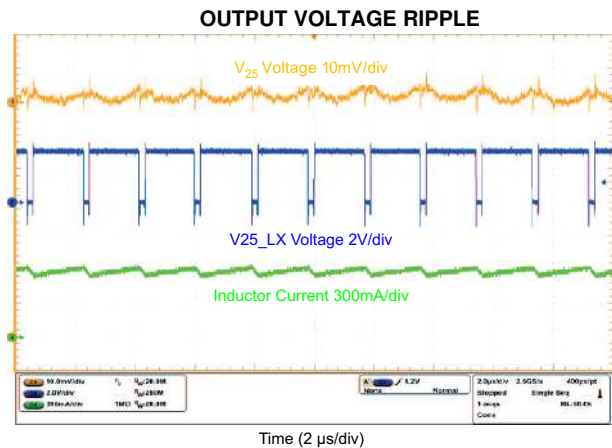


Figure 8. Buck Converter Output Ripple

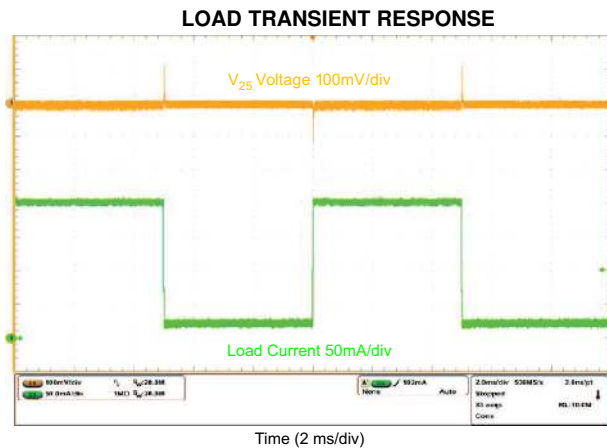


Figure 9. Buck Converter Load Transient Response

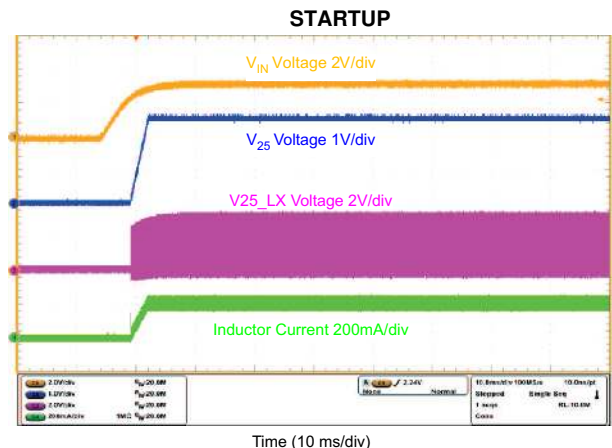


Figure 10. Buck Converter Startup

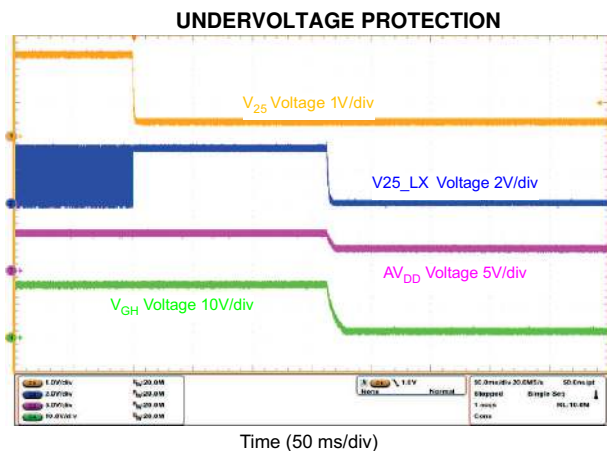


Figure 11. Buck Converter Undervoltage Protection

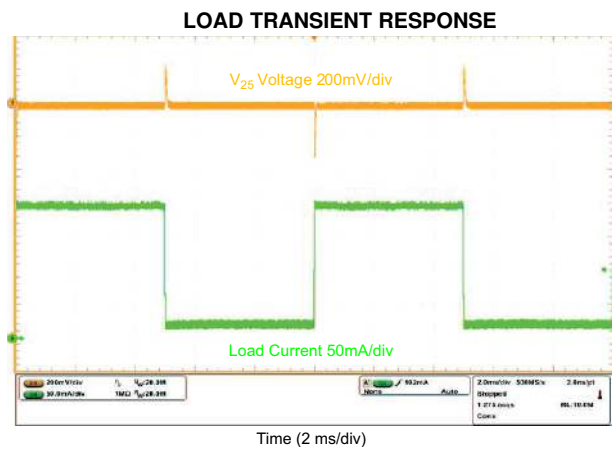


Figure 12. LDO Load Transient Response

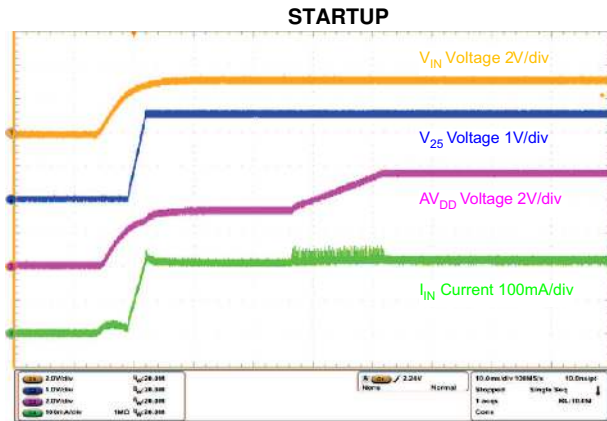


Figure 13. LDO Startup

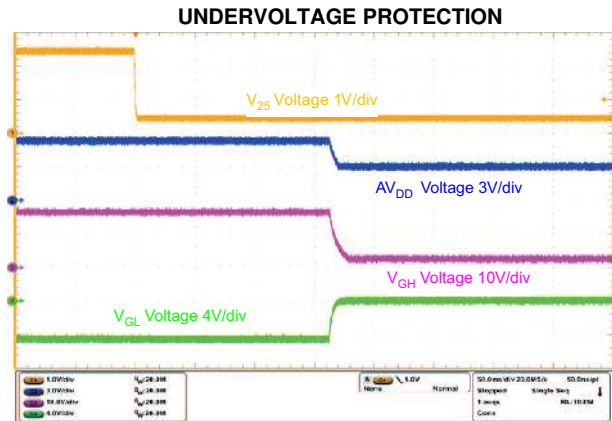


Figure 14. LDO Undervoltage Protection

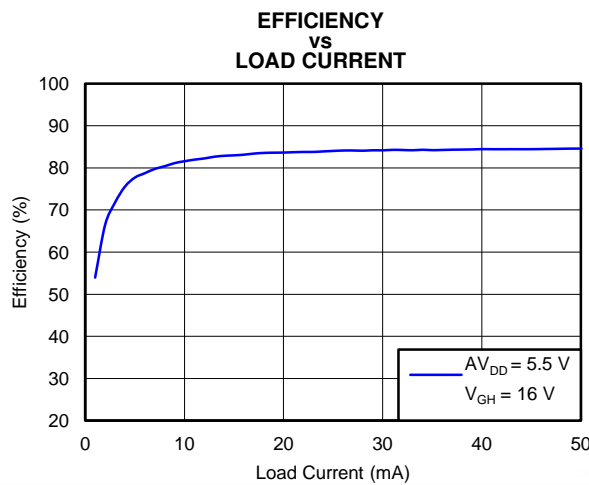


Figure 15. Boost Converter 2 Efficiency

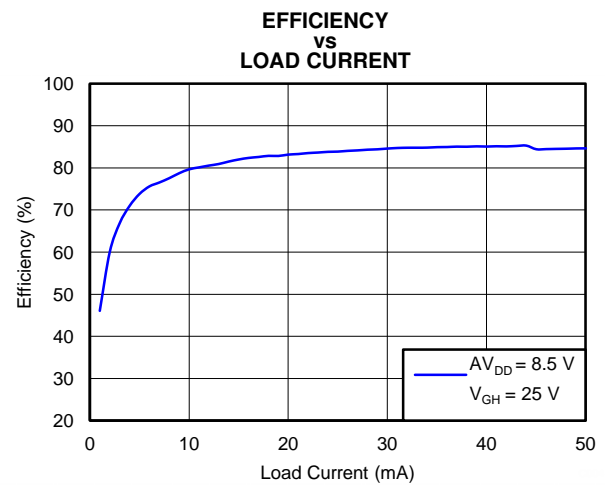


Figure 16. Boost Converter 2 Efficiency

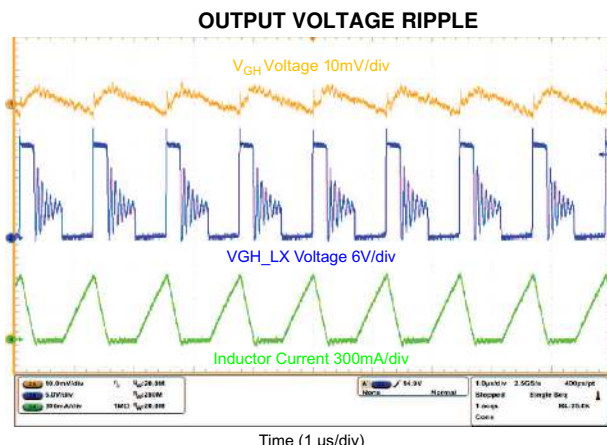


Figure 17. Boost Converter 2 Output Ripple

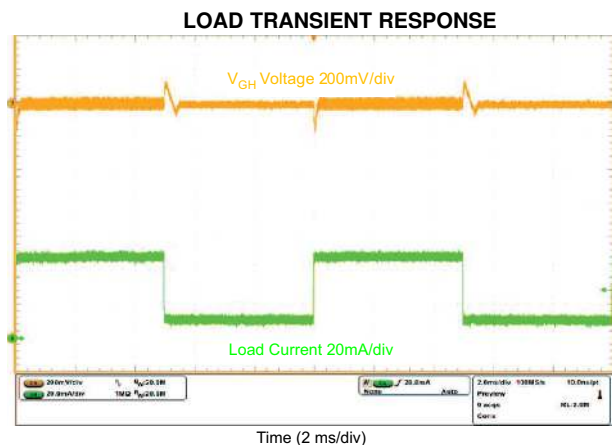


Figure 18. Boost Converter 2 Load Transient Response

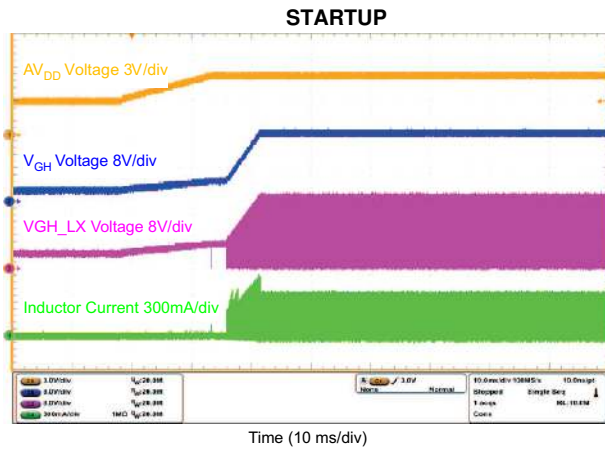


Figure 19. Boost Converter 2 Startup

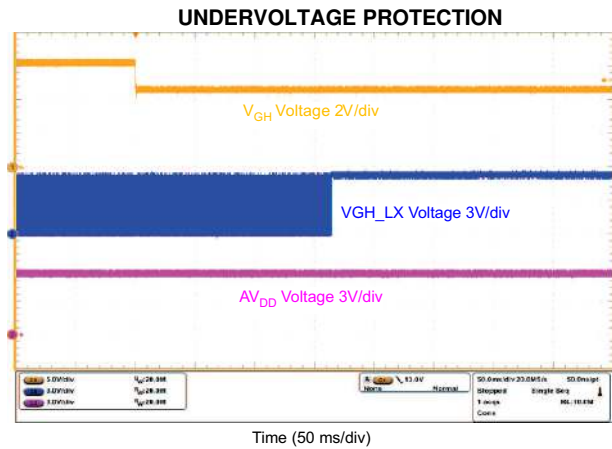


Figure 20. Boost Converter 2 Undervoltage Protection

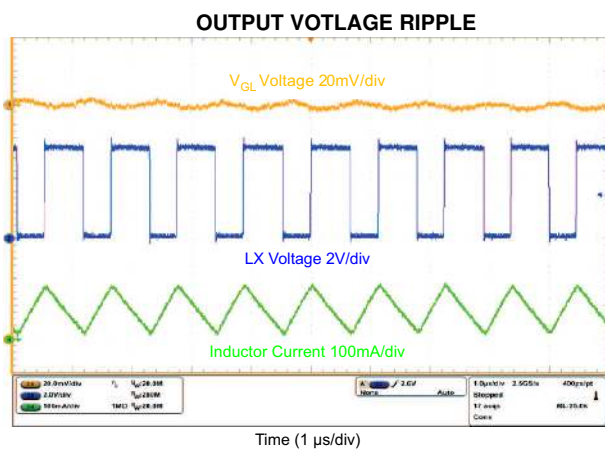


Figure 21. Negative Charge Pump Output Ripple

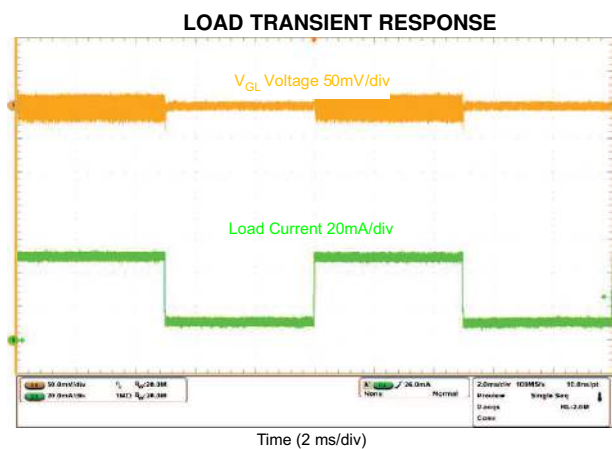


Figure 22. Negative Charge Pump Load Transient Response

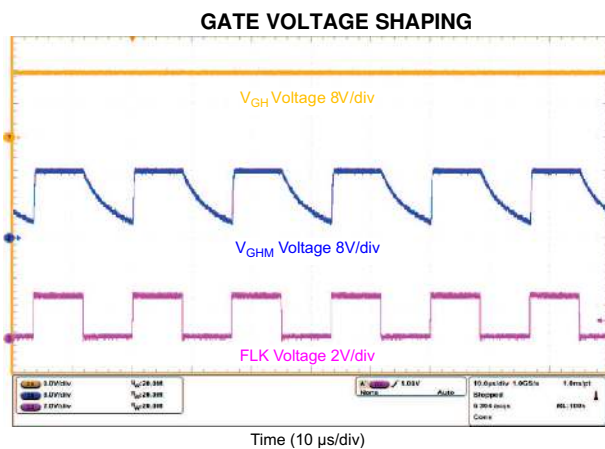


Figure 23. Gate Voltage Shaping

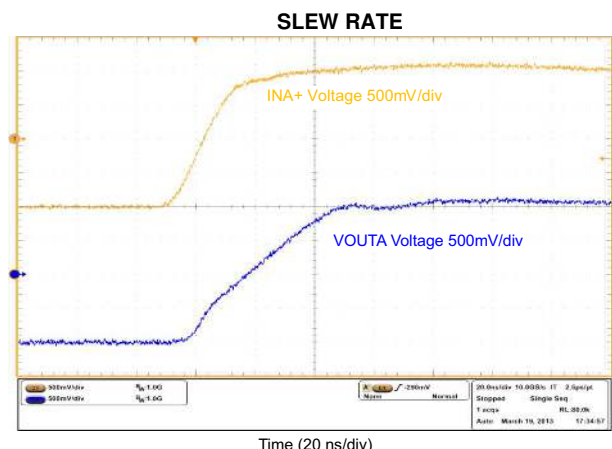


Figure 24. Operational Amplifier Slew Rate

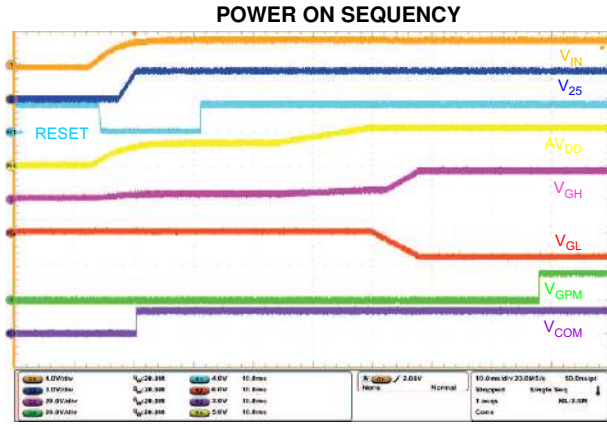


Figure 25. Power Off Sequency

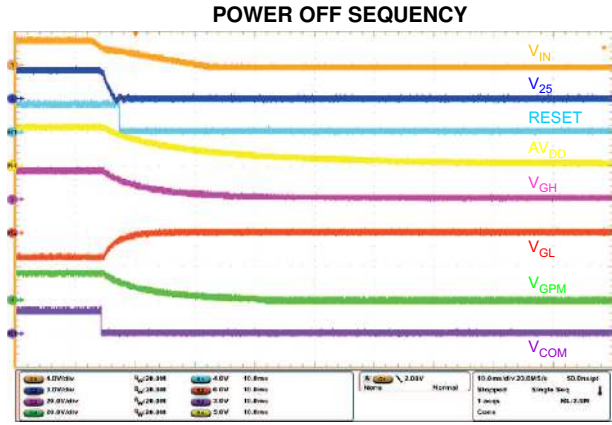


Figure 26. Power Off Sequency

DETAILED DESCRIPTION

An internal block diagram of the TPS65640 is shown in Figure 27.

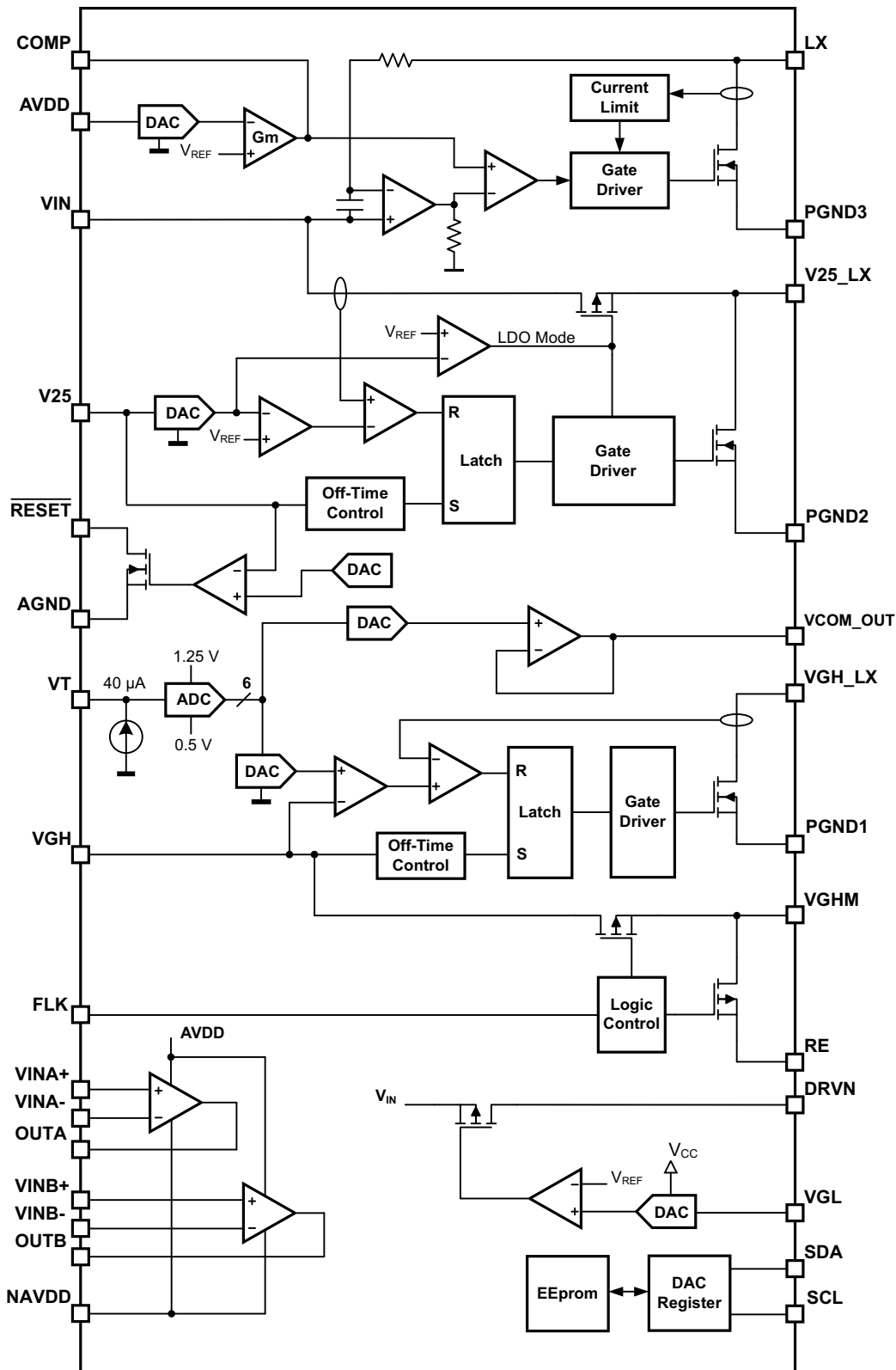


Figure 27. Internal Block Diagram



## BOOST CONVERTER 1 ( $AV_{DD}$ )

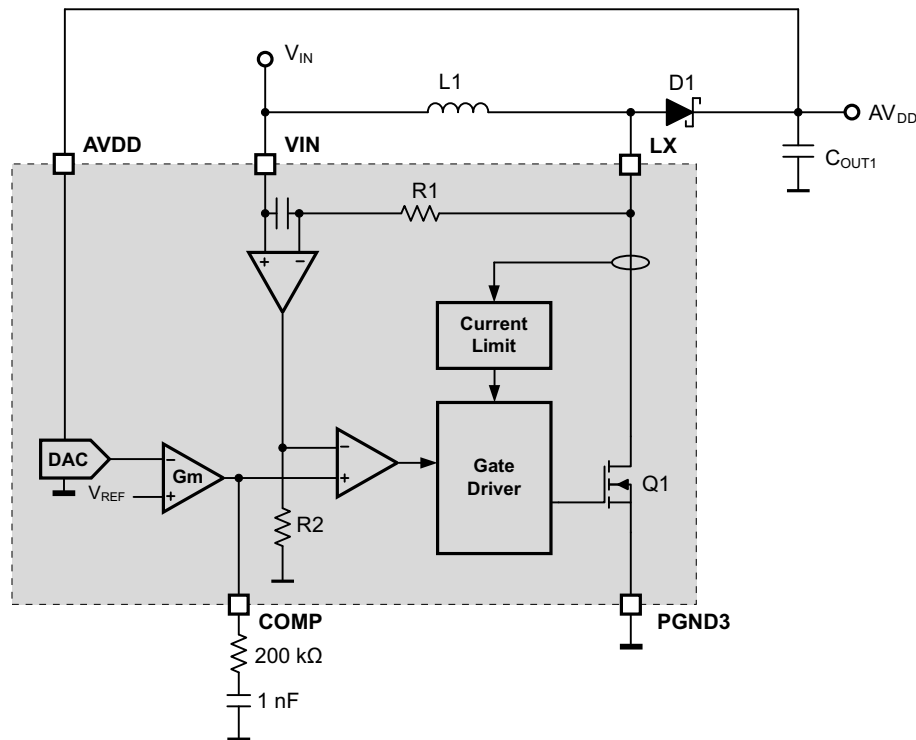


Figure 28. Boost Converter 1 Internal Block Diagram

### Switching Frequency (Boost Converter 1)

Boost Converter 1 can be configured to operate at 600 kHz, 800 kHz, 1000 kHz, or 1200 kHz. In general, the higher switching frequency offers better transient performance at the expense of slightly reduced efficiency. In some applications, it may be necessary to select a particular switching frequency to minimize EMI problems. The switching frequency is determined by the state of the **FREQ1** configuration bit in the **AVDDCONFIG** register.

### Compensation (Boost Converter 1)

Boost Converter 1 uses an external compensation network connected to its COMP pin to stabilize its feedback loop. A simple series R-C network connected between this pin and ground is sufficient to achieve good performance (that is, stable and with good transient response) in most applications. Good starting values, which will work for many applications, are 200 kΩ and 1 nF.

In some applications (for example, those using electrolytic output capacitors), it may be necessary to include a second compensation capacitor between the COMP pin and ground. This has the effect of adding an additional pole in the feedback loop's frequency response, which can be used to cancel the zero introduced by the electrolytic output capacitor's ESR.

### Output Voltage (Boost Converter 1)

Boost converter 1's output voltage can be programmed from 3.6 V to 11 V with 100-mV increment using the **AVDD** register. Because changing the output voltage in big steps can temporarily demand switch currents greater than the switch's current limit, it is recommended that  $AV_{DD}$  be changed in 100-mV steps, for example, first change  $AV_{DD}$  from 7 V to 7.1 V, then to 7.2 V, then to 7.3 V, and so on until the desired output voltage has been achieved.

### Start-Up (Boost Converter 1)

Boost converter 1 starts immediately after the  $V_{25}$  voltage raming to its programmed voltage.

To minimize inrush current during start-up, boost converter 1 ramps its output voltage in  $t_{SS1}$  milliseconds. The value of  $t_{SS1}$  can be programmed from 20ms to 80ms using the **SS1** bits in **AVDDCONFIG** register.

Boost converter 1's internal power good signal is asserted when two conditions are met:

- the converter's soft-start ramp has reached its final value
- the converter's output voltage is greater than its UVP threshold.

The power good signal is latched and will only be reset when the supply voltage is cycled.

### Current limit (Boost Converter 1)

The boost converter 1 has built-in cycle-by-cycle current limit for the power MOSFET. When the inductor current or the power MOSFET current reaches  $I_{LIM}$ , the power MOSFET will be tuned off immediately until the next switching cycle. The  $I_{LIM}$  can be programmed from 1 A to 2 A using the **AVDD\_ILIM** bit in **AVDDCONFIG** register.

### Design Procedure (Boost Converter 1)

The first step in the design procedure is to verify whether the maximum possible output current of the boost converter 1 supports the specific application requirements.

1. Converter Duty Cycle:

$$D = 1 - \frac{V_{IN} \times \eta}{V_{AVDD}} \quad (1)$$

2. Inductor Ripple Current:

$$\Delta I_L = \frac{V_{IN} \times D}{f_s \times L} \quad (2)$$

3. Maximum Output Current:

$$I_{OUT\_max} = \left( I_{LIM\_min} - \frac{\Delta I_L}{2} \right) \times (1 - D) \quad (3)$$

4. Peak Switching Current:

$$I_{SWPEAK} = \frac{I_{OUT}}{1 - D} + \frac{\Delta I_L}{2} \quad (4)$$

$\eta$  = Estimated boost converter efficiency (use the number from the efficiency plots or 0.9 as an estimation)

$f_s$  = Switching frequency

$L$  = Selected inductor value (typ. 10  $\mu$ H)

$I_{LIM\_min}$ : Minimum current limit

$I_{SWPEAK}$  = Peak switch current for the used output current

$\Delta I_L$  = Inductor peak-to-peak ripple current

The peak switch current  $I_{SWPEAK}$  is the current that the integrated switch, the inductor and the external Schottky diode have to be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

### Inductor Selection (Boost Converter 1)

<b>Inductor Value:</b>	$4.7 \mu\text{H} \leq L \leq 10 \mu\text{H}$	Higher the inductor value the lower the inductor current ripple and the output voltage ripple but the slower the transient response.
<b>Saturation Current:</b>	$I_{SAT} \geq I_{SWPEAK}$ OR $I_{SAT} \geq I_{LIM\_max}$	The inductor saturation current must be higher than the switch peak current for the max. peak output current or as a more conservative approach higher than the max. switch current limit.
<b>DC Resistance:</b>	The lower the inductors resistance the lower the losses and the higher the efficiency.	

### Rectifier Diode Selection (Boost Converter 1)

Diode type: Schottky or super barrier rectifier (SBR) for better efficiency.

Forward voltage: The lower the forward voltage  $V_F$  the higher the efficiency and the lower the diode temperature.

Reverse voltage:  $V_R$  must be higher than the output voltage and should be higher than the OVP voltage typically 15 V.

Thermal characteristics: The diode must be able to handle the dissipated power of  $P_D = V_F \times I_{OUT}$ .

### Output Capacitor Selection (Boost Converter 1)

For best output voltage filtering, TI recommends low-ESR ceramic capacitors. Two 4.7  $\mu\text{F}$  (or four 2.2- $\mu\text{F}$ ) ceramic capacitors work for most applications. To improve the load transient response more capacitance can be added between the rectifier diode.

To calculate the output voltage ripple the following equations can be used:

$$\Delta V_{C\_RIPPLE} = \frac{V_{AVDD} - V_{IN}}{V_{AVDD} \times f_s} \times \frac{I_{OUT}}{C_{OUT}} + \Delta V_{C\_ESR} \quad (5)$$

$$\Delta V_{C\_ESR} = I_{SWPEAK} \times R_{C\_ESR} \quad (6)$$

## BUCK CONVERTER ( $V_{25}$ )

The buck converter uses a current mode, quasi-constant off-time topology that offers high efficiency, fast transient response, and constant ripple current amplitude under all operating conditions (see Figure 29). The converter's off time is inversely proportional  $V_{25}$  and therefore constant when the converter is in regulation. Thus for a given  $V_{IN}$  the converter operates at a constant frequency that changes temporarily when the converter reacts to load changes.

When the latch is set, transistor  $Q_1$  is turned on and transistor  $Q_2$  is turned off. As inductor  $L_2$  charges, the current flowing through  $Q_1$  ramps up at a rate determined by the difference between  $V_{IN}$  and  $V_{CORE}$  and the value of  $L_2$ . The ramping current is sensed across  $Q_1$ , and when it reaches the level demanded by error amplifier  $A_1$  the output of comparator  $A_2$  goes high, resetting the latch. The reset latch turns off  $Q_1$  and turns on  $Q_2$ . Inductor  $L_2$  now discharges through  $Q_2$  for a fixed off time. At the end of the off time, the latch is set, turning on  $Q_1$  and turning off  $Q_2$ , and the cycle repeats.

The sensed output voltage is divided down by a multiplying DAC and used as negative feedback to amplifier  $A_1$ . The output of  $A_1$  is the error signal required to regulate  $V_{25}$  at the desired voltage.

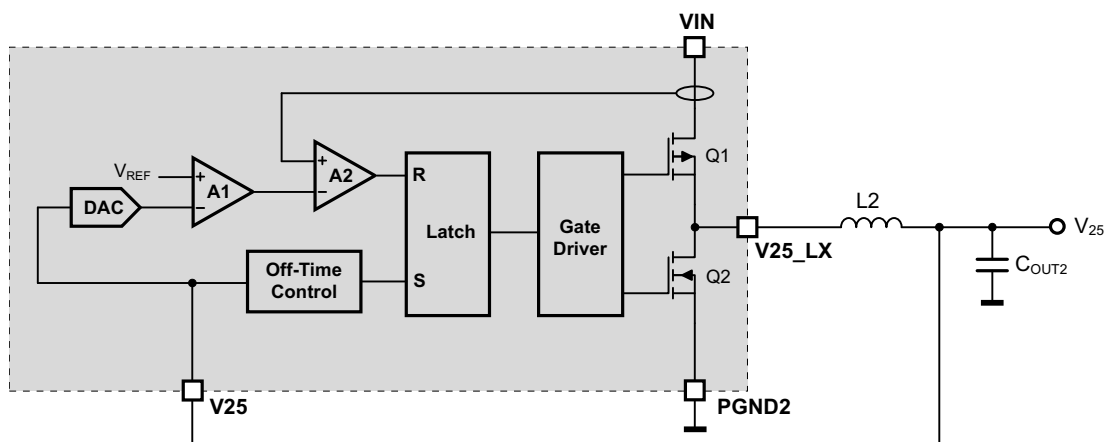


Figure 29. Buck Converter 1 Block Diagram

### Output Voltage (Buck Converter)

Buck converter's output voltage can be programmed from 1.5 V to 3.0 V using the **V25** register.

### Start-Up (Buck Converter)

Buck converter starts as soon as the supply voltage exceeds the under-voltage lockout threshold (the same time as the linear regulator starts).

To minimize inrush current during start-up, buck converter ramps  $V_{25}$  from 0 V to programmed voltage in  $t_{SS2}$  milliseconds. The value of  $t_{SS2}$  is around 0.5 ms to 4.0 ms.

The same ramp rate is used for both buck converter and the linear regulator (LDO).

### Current limit (Buck Converter)

The buck converter has built-in cycle-by-cycle current limit for the high side power MOSFET, Q1 in [Figure 29](#). When the inductor current or the MOSFET Q1 current reaches  $I_{LIM}$ , the Q1 is turned off immediately until the next switching cycle. The  $I_{LIM}$  is typically 1.2 A.

### Design Procedure (Buck Converter)

The first step in the design procedure is to verify whether the maximum possible output current of the buck converter supports the specific application requirements.

1. Switching Frequency:

$$f_s = \frac{V_{IN} \times \eta - V_{25}}{V_{IN} \times \eta \times T_{off}} \quad (7)$$

2. Converter Duty Cycle

$$D = \frac{V_{25}}{V_{IN} \times \eta} \quad (8)$$

3. Inductor Ripple Current:

$$\Delta I_L = \frac{(V_{IN} - V_{25}) \times D}{f_s \times L} \quad (9)$$

4. Maximum Output Current:

$$I_{OUT\_max} = I_{LIM\_min} - \frac{\Delta I_L}{2} \quad (10)$$

5. Peak Switching Current:

$$I_{SWPEAK} = I_{OUT} + \frac{\Delta I_L}{2} \quad (11)$$

$T_{off}$  = Buck boost switch duty off time (typ. 200 ns)

$\eta$  = Estimated boost converter efficiency (use the number from the efficiency plots or 0.8 as an estimation)

$f_s$  = Switching frequency

$L$  = Selected inductor value (typ. 10  $\mu$ H)

$I_{LIM\_min}$ : Minimum current limit

$I_{SWPEAK}$  = Peak switch current for the used output current

$\Delta I_L$  = Inductor peak-to-peak ripple current

The peak switch current  $I_{SWPEAK}$  is the current that the integrated switch, the inductor and the external Schottky diode have to be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

### Inductor Selection (Buck Converter)

<b>Inductor Value:</b>	$4.7 \mu\text{H} \leq L \leq 10 \mu\text{H}$	Higher the inductor value the lower the inductor current ripple and the output voltage ripple but the slower the transient response.
------------------------	--	--

<b>Saturation Current:</b>	$I_{SAT} \geq I_{SWPEAK}$ OR $I_{SAT} \geq I_{LIM\_max}$	The inductor saturation current must be higher than the switch peak current for the max. peak output current or as a more conservative approach higher than the max. switch current limit.
<b>DC Resistance:</b>	The lower the inductors resistance the lower the losses and the higher the efficiency.	

### Output Capacitor Selection (Buck Converter)

For best output voltage filtering, TI recommends low-ESR ceramic capacitors. Two 4.7- $\mu$ F (or four 2.2- $\mu$ F) ceramic capacitors work for most applications. To improve the load transient response more capacitance can be added between the rectifier diode.

To calculate the output voltage ripple the following equations can be used:

$$\Delta V_{C\_RIPPLE} = \frac{V_{25}}{V_{IN} \times f_s} \times \frac{I_{OUT}}{C_{OUT}} + \Delta V_{C\_ESR} \tag{12}$$

$$\Delta V_{C\_ESR} = I_{SWPEAK} \times R_{C\_ESR} \tag{13}$$

### LDO REGULATOR ( $V_{25}$ )

A low-dropout (LDO) linear regulator generates  $V_{25}$  (see Figure 30). The linear regulator is supplied from  $V_{IN}$  and it's an alternative option to buck converter. The  $V_{25}$  voltage could be supplied either by Buck converter or LDO determined by the state of the **BUCK/LDO** configuration bit in the **CONFIG** register.

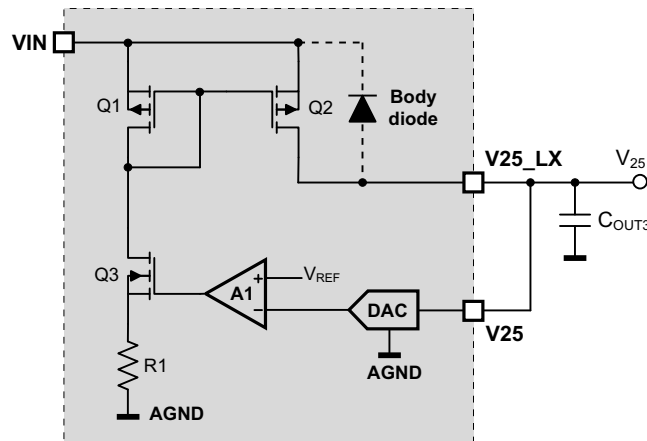


Figure 30. Linear Regulator Block Diagram

Amplifier  $A_1$  regulates the current through  $Q_3$  by comparing a reduced version of the output voltage with a bandgap voltage reference  $V_{REF}$ . The output of  $Q_3$  is mirrored by  $Q_1$  and  $Q_2$  to generate the desired output voltage. In practice,  $Q_2$  is made much bigger than  $Q_1$ . This means that the current flowing through  $Q_1$  and  $Q_3$  is smaller than the output current by the same ratio as the transistor areas.

The maximum output current is inherently limited by the maximum output voltage of  $A_1$ , the value of resistor  $R_1$ , and the characteristics of transistor  $Q_3$ .

### Output Voltage (LDO Regulator)

LDO's output voltage can be programmed from 1.5 V to 3.0 V using the **V25** register. Because the **V25\_LX** pin alternates for LDO regulator's output voltage and buck converter's switch node, select buck converter with LDO circuit configuration can make the permanent damage. The LDO regulator mode is factory default setup.

### Start-Up (Low Dropout Regulator)

LDO starts as soon as the supply voltage exceeds the under-voltage lockout threshold (the same time as the buck converter starts).

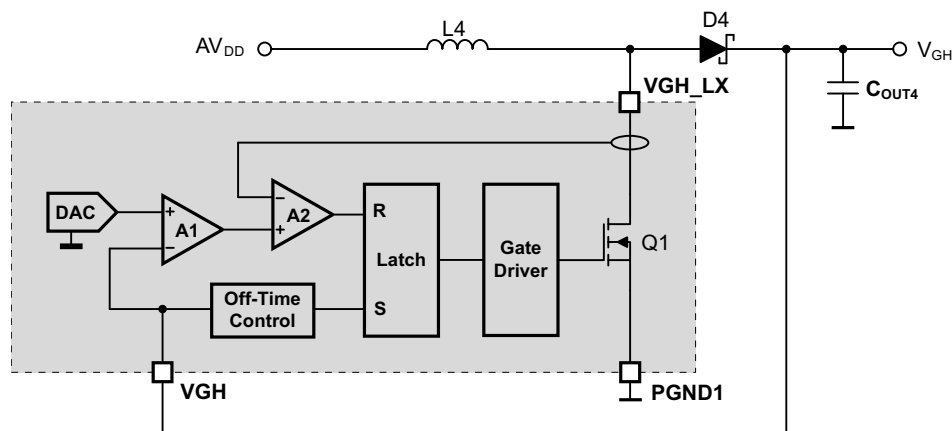
To minimize inrush current during start-up, LDO regulator ramps  $V_{25}$  from 0V to programmed voltage in  $t_{SS2}$  milliseconds. The value of  $t_{SS2}$  is around 0.5 ms to 4.0 ms.

The same ramp rate is used for both buck converter and the linear regulator.

## BOOST CONVERTER 2 ( $V_{GH}$ )

Boost converter 2 is a low-power boost converter that can be used to generate the LCD panel's gate ON voltage  $V_{GH}$ . Operating the converter in DCM removes the right-half-plane zero from its transfer function, simplifying its stabilization and allowing the use of small chip inductors. To simplify its application and to minimize the external parts required, boost converter 2 features internal compensation and soft-start circuitry.

A simplified block diagram of boost converter 2 is shown in [Figure 31](#).



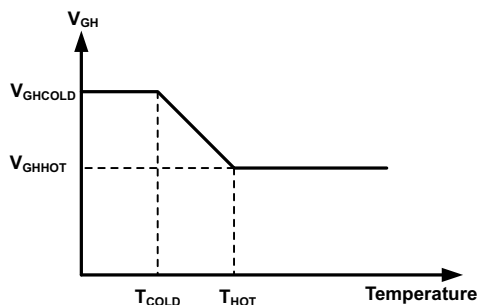
**Figure 31. Boost Converter 2 Block Diagram**

## Switching Frequency (Boost Converter 2)

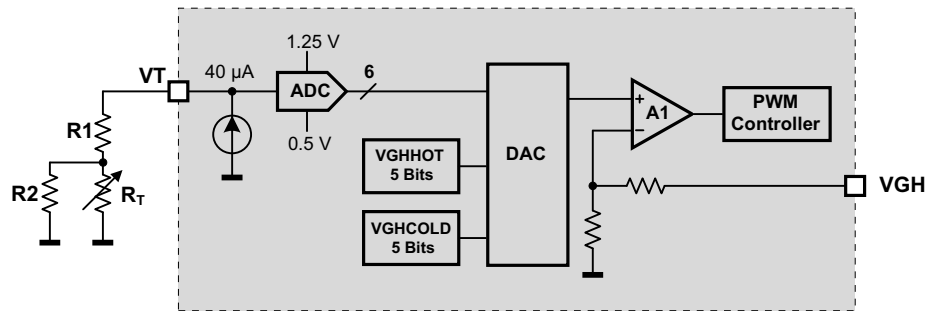
Boost Converter 2 can be configured to operate at 400 kHz or 800 kHz. The switching frequency is determined by the state of the **FREQ4** configuration bit in the **VGHCONFIG** register.

## Output Voltage Temperature Compensation (Boost Converter 2)

Boost converter 2 can be temperature compensated, allowing its output voltage to transition from a higher voltage at low temperatures  $V_{GH(COLD)}$  to a lower voltage at high temperatures  $V_{GH(HOT)}$  (see [Figure 32](#) and [Figure 33](#)).



**Figure 32. Boost Converter 2 Temperature Compensation Characteristic**



**Figure 33. Boost Converter 2 Temperature Compensation Block Diagram**

Referring to [Figure 33](#), The thermistor network formed by R1, R2, and  $R_T$  <sup>(1)</sup> generates a voltage at the VT pin whose value decreases with increasing temperature. With proper selection <sup>(2)</sup> of the external components  $R_T$ , R1 and R2, temperatures  $T_{HOT}$  and  $T_{COLD}$  can be configured to suit each display's characteristics. A spreadsheet allowing easy calculation of component values is available from Texas Instruments free of charge.

### Output Voltage (Boost Converter 2)

The output voltage of boost converter 2 at cold temperatures can be programmed from 15 V to 37 V using the **VGHCOLD** register.

The output voltage of boost converter 2 at hot temperatures can be programmed from 15 V to 37 V using the **VGHHOT** register.

In applications that do not require temperature compensation, the **VGHT** bit in **CONFIG** register should be set to 1 and the **VGHHOT** register used to set the voltage of  $V_{GH}$ .

Because changing the output voltage in big steps can temporarily demand switch currents greater than the switch's current limit, it is recommended that  $V_{GH}$  be changed in 1 V steps, i.e. first change  $V_{GH}$  from 15 V to 16 V, then to 16 V, then to 17 V, and so on until the desired output voltage has been achieved.

### Start-Up (Boost Converter 2)

Boost converter 2 is enabled when AVDD has finished ramping to its programmed voltage.

To minimize inrush current during start-up, boost converter 2 ramps  $V_{GH}$  to its programmed value in  $t_{SS4}$  seconds. The value of  $t_{SS4}$  can be programmed from 4 ms to 16 ms using the **SS4** bits in **VGHCONFIG** register. The same ramp rate is used for both boost converter 2 and the negative charge pump regulator.

Boost converter 2's internal power good signal is asserted when two conditions are met:

- the converter's soft-start ramp has reached its final value
- the converter's output voltage is greater than its UVP threshold.

The power good signal is latched and will only be reset when the supply voltage is cycled.

### Current limit (Boost Converter 2)

The boost converter 2 has built-in cycle-by-cycle current limit for the power MOSFET. When the inductor current or the power MOSFET current reaches  $I_{LIM}$ , the power MOSFET will be tuned off immediately until the next switching cycle. The  $I_{LIM}$  is typically 1.2 A for boost converter 2.

### Design Procedure (Boost Converter 2)

The first step in the design procedure is to verify whether the maximum possible output current of the boost converter supports the specific application requirements.

1. Converter Duty Cycle:

(1)  $R_T$  should be a negative temperature coefficient (NTC) type whose resistance at 25°C is 10kΩ.

(2) Texas Instruments can provide a spreadsheet that calculates suitable component values automatically.

$$D = 1 - \frac{V_{AVDD} \times \eta}{V_{GH}} \quad (14)$$

2. Inductor Ripple Current:

$$\Delta I_L = \frac{V_{AVDD} \times D}{f_s \times L} \quad (15)$$

3. Maximum Output Current:

$$I_{OUT\_max} = \left( I_{LIM\_min} - \frac{\Delta I_L}{2} \right) \times (1 - D) \quad (16)$$

4. Peak Switching Current:

$$I_{SWPEAK} = \frac{I_{OUT}}{1 - D} + \frac{\Delta I_L}{2} \quad (17)$$

$\eta$  = Estimated boost converter efficiency (use the number from the efficiency plots or 0.9 as an estimation)

$f_s$  = Switching frequency

$L$  = Selected inductor value (typ. 10  $\mu$ H)

$I_{LIM\_min}$ : Minimum current limit

$I_{SWPEAK}$  = Peak switch current for the used output current

$\Delta I_L$  = Inductor peak-to-peak ripple current

The peak switch current  $I_{SWPEAK}$  is the current that the integrated switch, the inductor and the external Schottky diode have to be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

### Inductor Selection (Boost Converter 2)

<b>Inductor Value:</b>	$4.7 \mu\text{H} \leq L \leq 10 \mu\text{H}$	Higher the inductor value the lower the inductor current ripple and the output voltage ripple but the slower the transient response.
<b>Saturation Current:</b>	$I_{SAT} \geq I_{SWPEAK}$ or $I_{SAT} \geq I_{LIM\_max}$	The inductor saturation current must be higher than the switch peak current for the max. peak output current or as a more conservative approach higher than the max. switch current limit.
<b>DC Resistance:</b>	The lower the inductors resistance the lower the losses and the higher the efficiency.	

### Rectifier Diode Selection (Boost Converter 2)

Diode type: Schottky or super barrier rectifier (SBR) for better efficiency.

Forward voltage: The lower the forward voltage  $V_F$  the higher the efficiency and the lower the diode temperature.

Reverse voltage:  $V_R$  must be higher than the output voltage and should be higher than the OVP voltage 39 V.

Thermal characteristics: The diode must be able to handle the dissipated power of  $P_D = V_F \times I_{OUT}$ .

### Output Capacitor Selection

For best output voltage filtering, TI recommends low-ESR ceramic capacitors. Two 4.7- $\mu$ F (or four 2.2- $\mu$ F) ceramic capacitors work for most applications. To improve the load transient response more capacitance can be added between the rectifier diode.

To calculate the output voltage ripple the following equations can be used:

$$\Delta V_{C\_RIPPLE} = \frac{V_{GH} - V_{AVDD}}{V_{GH} \times f_s} \times \frac{I_{OUT}}{C_{OUT}} + \Delta V_{C\_ESR} \quad (18)$$

$$\Delta V_{C\_ESR} = I_{SWPEAK} \times R_{C\_ESR} \quad (19)$$



## NEGATIVE CHARGE PUMP VOLTAGE REGULATOR CONTROL ( $V_{GL}$ )

The negative charge pump voltage regulator control an external NPN transistor to regulate the  $V_{GL}$  output. As typical application circuit Figure 34 illustrated, a one time negative voltage charge pump based on the  $AV_{DD}$  boost switching provides the source voltage to the emitter of NPN transistor. Depending on the feedback voltage applied on the VGL pin, A<sub>1</sub> error amplifier regulates the current through Q3. The proportional current mirrored by Q1 to Q2 sends to the base of NPN transistor from DRVN pin. Therefore, the regulation is achieved by controlled voltage drop between collector and emitter of NPN transition.

Normally the negative charge pump regulator is to provide gate OFF voltage to the gate driver or level shift. In additional, for positive and negative  $AV_{DD}$  application, it can also be used for negative  $AV_{DD}$  regulating. Because of charge bump voltage loss, it is recommended to leave enough voltage guard band (for example, 1 V for 50-mA load) between positive  $AV_{DD}$  to negative  $AV_{DD}$ .

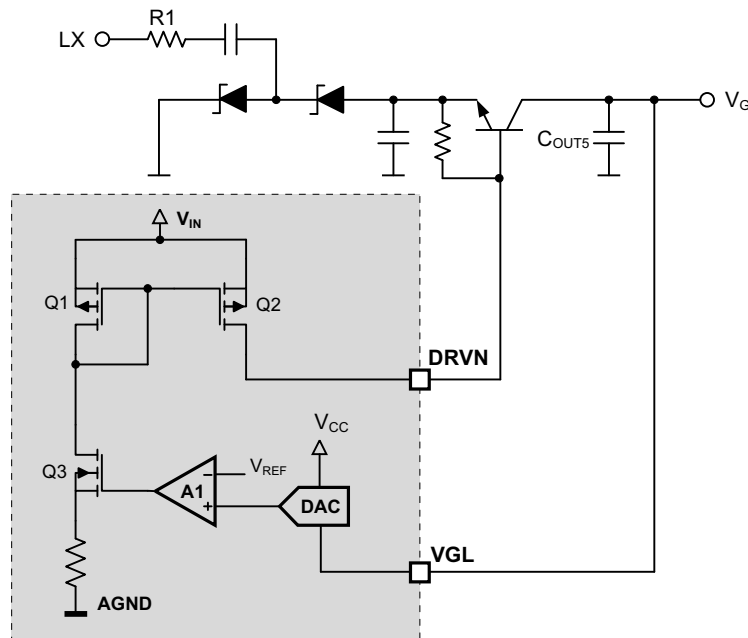


Figure 34. Negative Charge Pump Block Diagram

### Output Voltage (Negative Charge Pump)

Negative charge pump's output voltage can be programmed from  $-8$  V to  $-3.8$  V using the **VGL** register.

### Start-Up (Negative Charge Pump)

Negative charge pump is enabled together with booster converter 2 when  $AV_{DD}$  has finished ramping to its programmed voltage.

The same ramp rate is shared for both booster converter 2 and negative charge pump regulator. The negative charge pump regulator ramps  $V_{GL}$  to its programmed value from 0V in  $t_{SS4}$  seconds. The value of  $t_{SS4}$  can be programmed from 4 ms to 16 ms using the **SS4** bits in **VGHCONFIG** register.

### NPN Transistor Selection (Negative Charge Pump)

The NPN transistor used to regulator  $V_{GL}$  or Negative  $AV_{DD}$  should have a DC gain ( $h_{FE}$ ) of at least 100 when its collector current is equal to the charge pump's output current. The transistor should also be able withstand voltages up to  $V_{IN}$  across its collector-emitter ( $V_{CE}$ ).

The power dissipated in the transistor is given by Equation 20. The transistor must be able to dissipate this power without its junction becoming too hot. Note that the ability to dissipate power depends on adequate PCB thermal design.

$$P_Q = [V_{IN} - (2 \times V_F) - |V_{GL}|] \times I_{GL} \quad (20)$$

Where  $I_{GL}$  is the mean (not RMS) output current drawn from the charge pump.

### Diode Selection (Negative Charge Pump)

Small-signal diodes can be used for most low current applications (<50 mA) and higher rated diodes for higher power applications. The average current through the diode is equal to the output current, so that the power dissipated in the diode is given by [Equation 21](#)

$$P_D = I_{GL} \times V_F \quad (21)$$

The peak current through the diode occurs during start-up and for a few cycles may be as high as a few amps. However, this condition typically lasts for <1 ms and can be tolerated by many diodes whose repetitive current rating is much lower. The diodes' reverse voltage rating should be equal to at least  $2 \times V_{IN}$ .

### Capacitor Selection (Negative Charge Pump)

For the lowest output voltage ripple, low-ESR ceramic capacitors are recommended. The actual value is not critical and 1  $\mu$ F to 10  $\mu$ F is suitable for most applications. Large capacitors provide better performance in applications where large load transient currents are present.

A flying capacitor in the range of 100 nF to 1  $\mu$ F is suitable for most applications. Larger values experience a smaller voltage drop by the end of each switching cycle, and allow higher output voltages or currents, or both, to be achieved. Smaller values tend to be physically smaller and cheaper.

### OVER-VOLTAGE AND UNDER-VOLTAGE PROTECTION ( $AV_{DD}$ , $V_{25}$ , $V_{GH}$ )

Each voltage regulator output is protected against under-voltages and over-voltages.

Over-voltage conditions are detected if  $AV_{DD}$  output rises over typical 15 V or  $V_{GH}$  output rises over typical 39 V, in which cases the  $AV_{DD}$  boost switch or  $V_{GH}$  boost switch will be turned off until the overvoltage conditions is removed.

Undervoltage conditions are detected if a regulator output falls below certain level of its programmed voltage for longer than a time period, in which case the relevant voltage regulator is disabled. To recover normal operation following an under-voltage condition, the cause of the error condition must be removed and the supply voltage  $V_{IN}$  cycled.

**Table 1. Under Voltage Protection**

UVP	ERROR CONDITION	TIME PERIOD	PROTECT BEHAVIOR	RECOVERY CONDITION
$V_{25}$	< 1 V	> 160 ms	$V_{25}$ buck converter or LDO, $AV_{DD}$ boost converter, $V_{GH}$ boost converter and $V_{GL}$ regulator are disabled. $\overline{RESET}$ pin is pulled low.	Error condition is removed and $V_{IN}$ is cycled (POR).
$AV_{DD}$	< 80%	> 160 ms	$AV_{DD}$ boost converter, $V_{GH}$ boost convert and $V_{GL}$ voltage regulator are disabled.	Error condition is removed and $V_{IN}$ is cycled (POR).
$V_{GH}$	< 80%	> 160 ms	$V_{GH}$ boost converter is disabled.	Error condition is removed and $V_{IN}$ is cycled (POR).

### RESET GENERATOR

The  $\overline{RESET}$  pin generates an active-low reset signal for the T-CON (see [Figure 35](#)). During power-up the reset timer ( $t_{RESET}$ ) starts when  $V_{25}$  has finished ramping. The reset pulse duration can be programmed from 0 ms to 30 ms using the **RESET** register.

The  $\overline{RESET}$  output is an open-drain type that requires an external pull-up resistor. Pull-up resistor values in the range 10 k $\Omega$  to 100 k $\Omega$  are recommended for most applications.

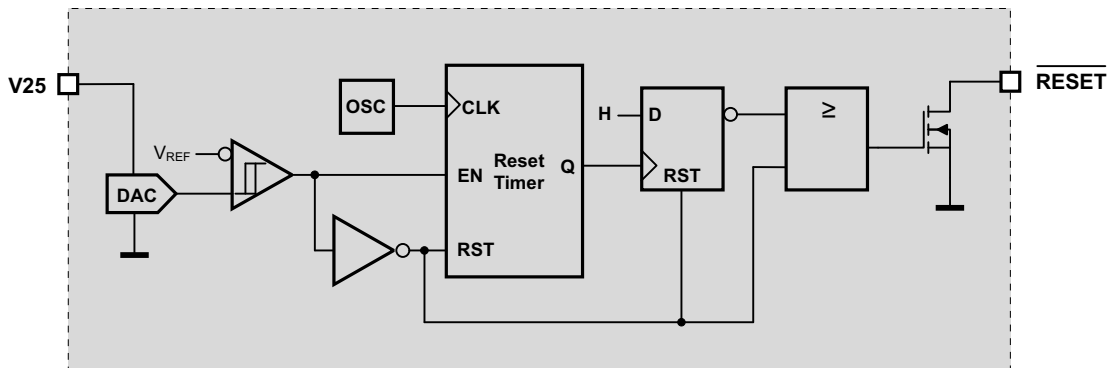


Figure 35. Reset Internal Block Diagram

### GATE VOLTAGE SHAPING

The gate voltage shaping function can be used to reduce image sticking in LCD panels by modulating the LCD panel's gate ON voltage ( $V_{GH}$ ). Figure 36 shows a block diagram of the gate voltage shaping function and Figure 37 shows the typical waveforms during operation.

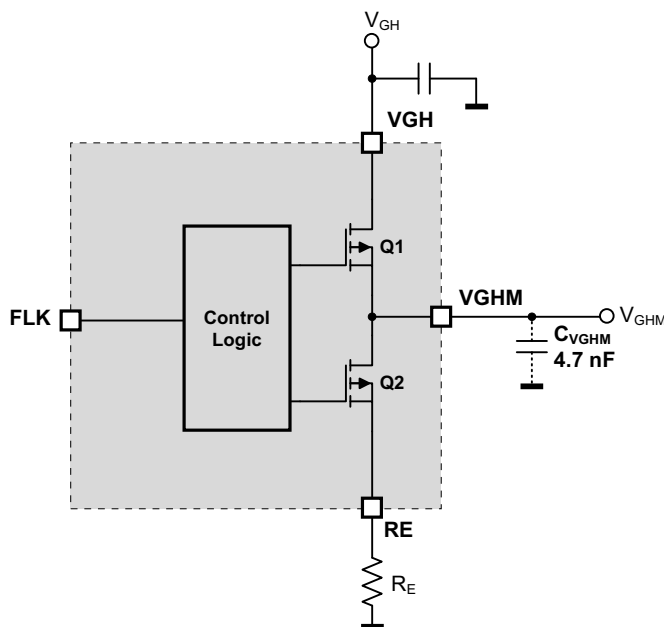


Figure 36. Gate Voltage Shaping Block Diagram

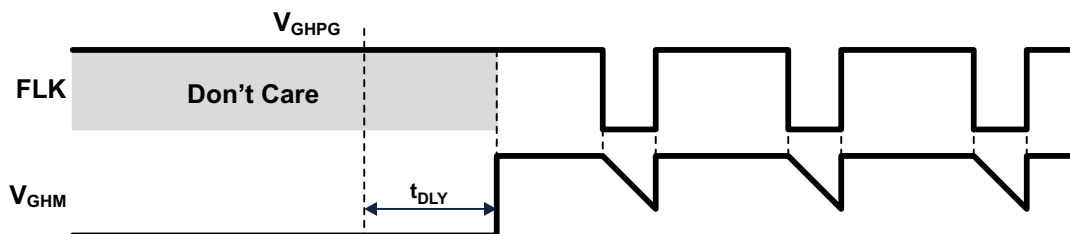


Figure 37. Gate Voltage Shaping Waveforms

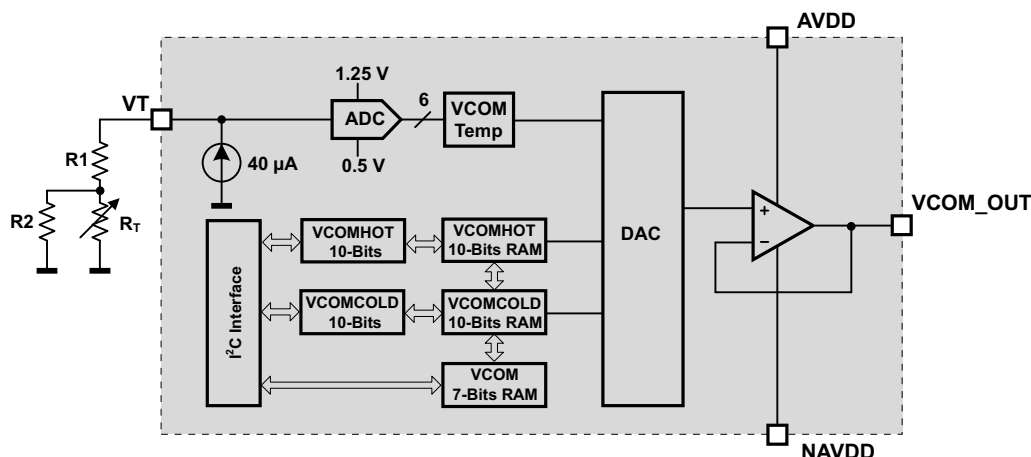
Gate voltage shaping is controlled by the FLK input. When FLK is high, Q<sub>1</sub> is on, Q<sub>2</sub> is off, and V<sub>G<sub>HM</sub></sub> is equal to V<sub>GH</sub>. On the falling edge of FLK, Q<sub>1</sub> is turned off, Q<sub>2</sub> is turned on, and the LCD panel load connected to the VG<sub>HM</sub> pin discharges through the external resistor connected to the RE pin.

During power-up Q<sub>2</sub> is held permanently on and Q<sub>1</sub> permanently off, regardless of the state of the FLK signal, until t<sub>DLY</sub> milliseconds after boost converter 2 (V<sub>GH</sub>) has finished ramping. The value of t<sub>DLY</sub> can be programmed from 0ms to 60ms using the **DLY** register.

During power-down Q<sub>2</sub> is held permanently on and Q<sub>1</sub> permanently off, regardless of the state of the FLK signal.

### PROGRAMMABLE V<sub>COM</sub> CALIBRATOR (V<sub>COM</sub>)

The programmable VCOM calibrator uses a DAC to generate an offset Voltage for LCD panel common voltage reference.



**Figure 38. Programmable V<sub>COM</sub> Calibrator Block Diagram**

The VCOM voltage calibration needs two steps for adjustment.

First step is to set the central value of V<sub>COM</sub> voltage according to the AV<sub>DD</sub>, V<sub>GH</sub> and LCD panel characteristic. The VCOM voltage is programmable from 1.5 V to 5.0 V or –4 V to 0.8 V by **VCOMHOT** register. The first step is normally done by PCB assembly manufacturer.

Second step is to calibrate the V<sub>COM</sub> voltage on the LCD panel assembly line by **VCOM** RAM register through I<sup>2</sup>C digital interface. The **VCOM** register value indicates the voltage increment or decrement of VCOM\_OUT which is preset by **VCOMHOT**. Once the proper value is identified, the VCOM\_OUT voltage value can be renewed with **VCOM** register value added. The default value for VCOM register is **1000000**. If 1000001 is written into **VCOM** register, the VCOM\_OUT voltage will increase with one DAC step, 10mV. In the other hand if 0111111 is written to **VCOM** register, the VCOM\_OUT voltage will decrease with one DAC step, 10 mV.

The VCOM voltage also supports temperature compensation and allows its output voltage to transition from a lower voltage at low temperatures V<sub>COMCOLD</sub> to a higher voltage at high temperatures V<sub>COMHOT</sub> (see Figure 39). The temperature compensation for VCOM could be turn on/off by bit **VCOMT** in register **CONFIG**. If temperature compensation for VCOM is ON state, both **VCOMHOT** and **VCOMCOLD** need to be input. Otherwise only **VCOMHOT** is active for VCOM voltage setting without temperature compensation.

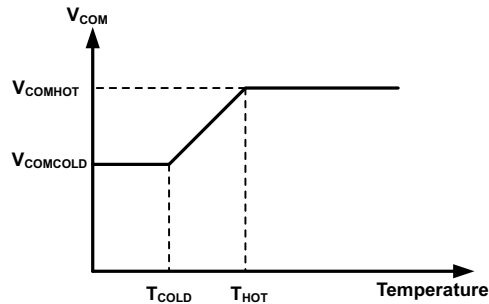


Figure 39.  $V_{COM}$  Temperature Compensation Characteristic

## OPERATIONAL AMPLIFIERS

Like most operational amplifiers, the  $V_{COM}$  amplifiers are not designed to drive purely capacitive loads, so it is not recommended to connect a capacitor directly to their outputs in an attempt to increase performance; however, the amplifiers are capable of delivering high peak currents that make such capacitors unnecessary.

To optimize performance, the  $V_{COM}$  amplifiers' positive supplies are connected internally to the AVDD pin and negative supplies are connected internally to NAVDD pin (See Figure 40 for operational amplifier internal block diagram).

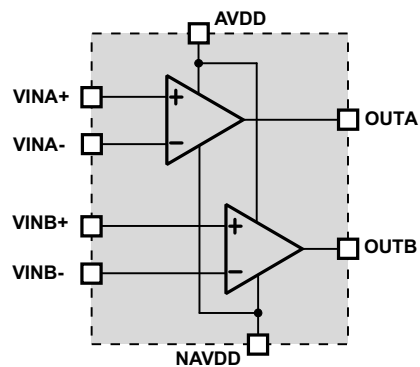


Figure 40. Operational Amplifier Block Diagram

The two integrated operational amplifiers are able to be disabled for non-used application to minimize the power consumption. Setting the **OPA\_A** bit or **OPA\_B** bit in **CONFIG** register can turn on/off operational amplifier A or B individually.

To minimize the additional power dissipated when operational amplifier is turned off, it is recommended to short the both inverter input and non-inverter input to same voltage bias or leave them floating.

## CONFIGURATION PARAMETERS

The TPS65640 divides the configuration parameters into two categories:

- $V_{COM}$  calibration
- All other configuration parameters

In typical applications, all configuration parameters except  $V_{COM}$  are programmed by the subcontractor during PCB assembly, and  $V_{COM}$  is programmed by the display manufacturer during display calibration.

## RAM and E<sup>2</sup>PROM

Configuration parameters can be changed by writing the desired values to the appropriate RAM register or registers. The RAM registers are volatile and their contents are lost when power is removed from the device. By writing to the Control Register, it is possible to store the active configuration in non-volatile E<sup>2</sup>PROM so that it will subsequently be used as the default setting upon when the device is powered up.

### Configuration Parameters (Excluding VCOM Calibration)

Table 2 shows the memory map of the configuration parameters.

**Table 2. Configuration Memory Map**

Register Address	Register Name	Factory Default	Description
00h	CONFIG	FAh	Sets function control bits
01h	AVDD	3Ah	Sets the output voltage of AVDD boost converter
02h	AVDDCONFIG	0Ah	Sets miscellaneous configuration bits for AVDD boost converter
03h	VGHHOT	09h	Sets the output voltage of VGH boost converter at high temperatures (VGHT = 0) or VGH boost converter (VGHT=1)
04h	VGHCOLD	09h	Sets the output voltage of VGH boost converter at low temperatures (VGHT=0)
05h	VGHCONFIG	02h	Sets miscellaneous configuration bits for VGH boost converter
06h	VGL	1Fh	Sets the output voltage of VGL linear regulator
07h	V25	0Ah	Sets the output voltage of buck converter.
08h	VDIV	01h	Sets the threshold of the /RST signals
09h	RESET	06h	Sets the reset pulse duration
0Ah	DLY	01h	Sets the gate voltage shaping delay
0Bh	VCOMHOT	5Fh	Presets the output voltage of VCOM reference at high temperatures (VCOMT = 0) or VCOM reference (VCOMT=1)
0Ch	VCOMCOLD	5Fh	Presets the output voltage of VCOM reference at low temperatures (VCOMT=0)
FFh	Control	00h	Controls whether read and write operations access RAM or E <sup>2</sup> PROM registers

**CONFIG (00h)**

The **CONFIG** register can be written to and read from.

**Table 3. CONFIG Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
VCOMR	VCOMT	OPA_B	OPA_A	BUCK/LDO	VGL	VGHT	VGH
<b>VGH</b>	Bit 0	This bit enables/disables the boost converter for VGH voltage regulator.					
	0	Enables the VGH boot converter					
	1	Disables the VGH boost converter					
<b>VGHT</b>	Bit 1	This bit enables/disables the temperature compensation for VGH regulator.					
	0	Enables the temperature compensation for VGH voltage regulator					
	1	Disables the temperature compensation for VGH voltage regulator					
<b>VGL</b>	Bit 2	This bit enables/disables the VGL linear voltage regulator.					
	0	Enables the VGL linear voltage regulator					
	1	Disables the VGL linear voltage regulator					
<b>BUCK/LDO</b>	Bit 3	This bit selects the operation mode for V25 voltage regulator.					
	0	Selects the Buck converter for V25 voltage regulator					
	1	Selects the LDO for V25 voltage regulator					
<b>OPA_A</b>	Bit 4	This bit enables/disables the OPA_A operational amplifier.					
	0	Enables the OPA_A operational amplifier					
	1	Disables the OPA_A operational amplifier					
<b>OPA_B</b>	Bit 5	This bit enables/disables the OPA_B operational amplifier.					
	0	Enables the OPA_B operational amplifier					
	1	Disables the OPA_B operational amplifier					
<b>VCOMT</b>	Bit 6	This bit enables/disables the temperature compensation for VCOM voltage					
	0	Enables the temperature compensation for VCOM voltage					
	1	Disables the temperature compensation for VCOM voltage					
<b>VCOMR</b>	Bit 7	This bit sets the $V_{COM}$ voltage output range					
	0	$V_{COM} = 0.8\text{ V} \sim 5\text{ V}$ for full $AV_{DD}$ Application					
	1	$V_{COM} = -4.1\text{ V} \sim 0.2\text{ V}$ for PN $AV_{DD}$ Application					

**AVDD (01h)**

The **AVDD** register can be written to and read from.

**Table 4. AVDD Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>	<b>AVDD</b>						
<b>AVDD</b>	Bits	These bits select boost converter 1's output voltage (AVDD)					
	6-0	0000000	N.A.	1000010	AV <sub>DD</sub> = 6.6 V	1100010	AV <sub>DD</sub> = 9.8 V
	.....		N.A.	1000011	AV <sub>DD</sub> = 6.7 V	1100011	AV <sub>DD</sub> = 9.9 V
	0100100	AV <sub>DD</sub> = 3.6 V	1000100	AV <sub>DD</sub> = 6.8 V	1100100	AV <sub>DD</sub> = 10.0 V	AV <sub>DD</sub> = 10.0 V
	0100101	AV <sub>DD</sub> = 3.7 V	1000101	AV <sub>DD</sub> = 6.9 V	1100101	AV <sub>DD</sub> = 10.1 V	AV <sub>DD</sub> = 10.1 V
	0100110	AV <sub>DD</sub> = 3.8 V	1000110	AV <sub>DD</sub> = 7.0 V	1100110	AV <sub>DD</sub> = 10.2 V	AV <sub>DD</sub> = 10.2 V
	0100111	AV <sub>DD</sub> = 3.9 V	1000111	AV <sub>DD</sub> = 7.1 V	1100111	AV <sub>DD</sub> = 10.3 V	AV <sub>DD</sub> = 10.3 V
	0101000	AV <sub>DD</sub> = 4.0 V	1001000	AV <sub>DD</sub> = 7.2 V	1101000	AV <sub>DD</sub> = 10.4 V	AV <sub>DD</sub> = 10.4 V
	0101001	AV <sub>DD</sub> = 4.1 V	1001001	AV <sub>DD</sub> = 7.3 V	1101001	AV <sub>DD</sub> = 10.5 V	AV <sub>DD</sub> = 10.5 V
	0101010	AV <sub>DD</sub> = 4.2 V	1001010	AV <sub>DD</sub> = 7.4 V	1101010	AV <sub>DD</sub> = 10.6 V	AV <sub>DD</sub> = 10.6 V
	0101011	AV <sub>DD</sub> = 4.3 V	1001011	AV <sub>DD</sub> = 7.5 V	1101011	AV <sub>DD</sub> = 10.7 V	AV <sub>DD</sub> = 10.7 V
	0101100	AV <sub>DD</sub> = 4.4 V	1001100	AV <sub>DD</sub> = 7.6 V	1101100	AV <sub>DD</sub> = 10.8 V	AV <sub>DD</sub> = 10.8 V
	0101101	AV <sub>DD</sub> = 4.5 V	1001101	AV <sub>DD</sub> = 7.7 V	1101101	AV <sub>DD</sub> = 10.9 V	AV <sub>DD</sub> = 10.9 V
	0101110	AV <sub>DD</sub> = 4.6 V	1001110	AV <sub>DD</sub> = 7.8 V	1101110	AV <sub>DD</sub> = 11.0 V	AV <sub>DD</sub> = 11.0 V
	0101111	AV <sub>DD</sub> = 4.7 V	1001111	AV <sub>DD</sub> = 7.9 V	1101111	AV <sub>DD</sub> = 11.1 V	AV <sub>DD</sub> = 11.1 V
	0110000	AV <sub>DD</sub> = 4.8 V	1010000	AV <sub>DD</sub> = 8.0 V	1110000	AV <sub>DD</sub> = 11.2 V	AV <sub>DD</sub> = 11.2 V
	0110001	AV <sub>DD</sub> = 4.9 V	1010001	AV <sub>DD</sub> = 8.1 V	1110001	AV <sub>DD</sub> = 11.3 V	AV <sub>DD</sub> = 11.3 V
	0110010	AV <sub>DD</sub> = 5.0 V	1010010	AV <sub>DD</sub> = 8.2 V	1110010	AV <sub>DD</sub> = 11.4 V	AV <sub>DD</sub> = 11.4 V
	0110011	AV <sub>DD</sub> = 5.1 V	1010011	AV <sub>DD</sub> = 8.3 V	1110011	AV <sub>DD</sub> = 11.5 V	AV <sub>DD</sub> = 11.5 V
	0110100	AV <sub>DD</sub> = 5.2 V	1010100	AV <sub>DD</sub> = 8.4 V	1110100	AV <sub>DD</sub> = 11.6 V	AV <sub>DD</sub> = 11.6 V
	0110101	AV <sub>DD</sub> = 5.3 V	1010101	AV <sub>DD</sub> = 8.5 V	1110101	AV <sub>DD</sub> = 11.7 V	AV <sub>DD</sub> = 11.7 V
	0110110	AV <sub>DD</sub> = 5.4 V	1010110	AV <sub>DD</sub> = 8.6 V	1110110	AV <sub>DD</sub> = 11.8 V	AV <sub>DD</sub> = 11.8 V
	0110111	AV <sub>DD</sub> = 5.5 V	1010111	AV <sub>DD</sub> = 8.7 V	1110111	AV <sub>DD</sub> = 11.9 V	AV <sub>DD</sub> = 11.9 V
	0111000	AV <sub>DD</sub> = 5.6 V	1011000	AV <sub>DD</sub> = 8.8 V	1111000	AV <sub>DD</sub> = 12.0 V	AV <sub>DD</sub> = 12.0 V
	0111001	AV <sub>DD</sub> = 5.7 V	1011001	AV <sub>DD</sub> = 8.9 V	1111001	AV <sub>DD</sub> = 12.1 V	AV <sub>DD</sub> = 12.1 V
	0111010	AV <sub>DD</sub> = 5.8 V	1011010	AV <sub>DD</sub> = 9.0 V	1111010	AV <sub>DD</sub> = 12.2 V	AV <sub>DD</sub> = 12.2 V
	0111011	AV <sub>DD</sub> = 5.9 V	1011011	AV <sub>DD</sub> = 9.1 V	1111011	AV <sub>DD</sub> = 12.3 V	AV <sub>DD</sub> = 12.3 V
	0111100	AV <sub>DD</sub> = 6.0 V	1011100	AV <sub>DD</sub> = 9.2 V	1111100	AV <sub>DD</sub> = 12.4 V	AV <sub>DD</sub> = 12.4 V
	0111101	AV <sub>DD</sub> = 6.1 V	1011101	AV <sub>DD</sub> = 9.3 V	1111101	AV <sub>DD</sub> = 12.5 V	AV <sub>DD</sub> = 12.5 V
	0111110	AV <sub>DD</sub> = 6.2 V	1011110	AV <sub>DD</sub> = 9.4 V	1111110	AV <sub>DD</sub> = 12.6 V	AV <sub>DD</sub> = 12.6 V
	0111111	AV <sub>DD</sub> = 6.3 V	1011111	AV <sub>DD</sub> = 9.5 V	1111111	AV <sub>DD</sub> = 12.7 V	AV <sub>DD</sub> = 12.7 V
	1000000	AV <sub>DD</sub> = 6.4 V	1100000	AV <sub>DD</sub> = 9.6 V			
	1000001	AV <sub>DD</sub> = 6.5 V	1100001	AV <sub>DD</sub> = 9.7 V			



**AVDDCONFIG (02h)**

The **AVDDCONFIG** register can be written to and read from.

**Table 5. AVDDCONFIG Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>	<b>AVDD ILIM</b>	<b>SSI</b>		<b>FREQ1</b>		<b>LX1TS</b>	
<b>LX1TS</b>	Bit 1-0	These bits configure the falling speed of AVDD boost switch.					
		00	Tf = 0.5 V/ns				
		01	Tf = 0.7 V/ns				
		10	Tf = 0.9 V/ns				
		11	Tf = 1.1 V/ns				
<b>FREQ1</b>	Bit 3-2	These bits configure the switching frequency of AVDD boost.					
		00	f <sub>LX</sub> = 600 kHz				
		01	f <sub>LX</sub> = 800 kHz				
		10	f <sub>LX</sub> = 1000 kHz				
		11	f <sub>LX</sub> = 1200 kHz				
<b>SSI</b>	Bit 5-4	These bits configure the soft start duration for AVDD boost regulator					
		00	t <sub>SS1</sub> = 20 ms				
		01	t <sub>SS1</sub> = 40 ms				
		10	t <sub>SS1</sub> = 60 ms				
		11	t <sub>SS1</sub> = 80 ms				
<b>AVDD ILIM</b>	Bit 6	This bit select the AVDD boost current limite value					
		0	I <sub>LIM</sub> = 1 A				
		1	I <sub>LIM</sub> = 2 A				
<b>Reserved</b>	Bits 7	This bit is reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**VGHHOT (03h)**

The **VGHHOT** register can be written to and read from.

**Table 6. VGHHOT Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>			<b>VGHHOT</b>				
<b>VGHHOT</b>	Bits	These bits select VGH output voltage at hot temperatures (VGHT=0) or all temperature range (VGHT=1).					
	4-0	00000	N.A.	10000	V <sub>GHHOT</sub> = 22 V		
		00001	N.A.	10001	V <sub>GHHOT</sub> = 23 V		
		00010	N.A.	10010	V <sub>GHHOT</sub> = 24 V		
		00011	N.A.	10011	V <sub>GHHOT</sub> = 25 V		
		00100	N.A.	10100	V <sub>GHHOT</sub> = 26 V		
		00101	N.A.	10101	V <sub>GHHOT</sub> = 27 V		
		00110	N.A.	10110	V <sub>GHHOT</sub> = 28 V		
		00111	N.A.	10111	V <sub>GHHOT</sub> = 29 V		
		01000	N.A.	11000	V <sub>GHHOT</sub> = 30 V		
		01001	V <sub>GHHOT</sub> = 15 V	11001	V <sub>GHHOT</sub> = 31 V		
		01010	V <sub>GHHOT</sub> = 16 V	11010	V <sub>GHHOT</sub> = 32 V		
		01011	V <sub>GHHOT</sub> = 17 V	11011	V <sub>GHHOT</sub> = 33 V		
		01100	V <sub>GHHOT</sub> = 18 V	11100	V <sub>GHHOT</sub> = 34 V		
		01101	V <sub>GHHOT</sub> = 19 V	11101	V <sub>GHHOT</sub> = 35 V		
		01110	V <sub>GHHOT</sub> = 20 V	11110	V <sub>GHHOT</sub> = 36 V		
		01111	V <sub>GHHOT</sub> = 21 V	11111	V <sub>GHHOT</sub> = 37 V		
<b>Reserved</b>	Bits 7-5	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**VGHCOLD (04h)**

The **VGHCOLD** register can be written to and read from.

**Table 7. VGHCOLD Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>			<b>VGHCOLD</b>				
<b>VGHCOLD</b>	Bits	These bits select VGH output voltage at cold temperatures (VGHT=0)					
	4-0	00000	N.A.	10000	V <sub>GHCOLD</sub> = 22 V		
		00001	N.A.	10001	V <sub>GHCOLD</sub> = 23 V		
		00010	N.A.	10010	V <sub>GHCOLD</sub> = 24 V		
		00011	N.A.	10011	V <sub>GHCOLD</sub> = 25 V		
		00100	N.A.	10100	V <sub>GHCOLD</sub> = 26 V		
		00101	N.A.	10101	V <sub>GHCOLD</sub> = 27 V		
		00110	N.A.	10110	V <sub>GHCOLD</sub> = 28 V		
		00111	N.A.	10111	V <sub>GHCOLD</sub> = 29 V		
		01000	N.A.	11000	V <sub>GHCOLD</sub> = 30 V		
		01001	V <sub>GHCOLD</sub> = 15 V	11001	V <sub>GHCOLD</sub> = 31 V		
		01010	V <sub>GHCOLD</sub> = 16 V	11010	V <sub>GHCOLD</sub> = 32 V		
		01011	V <sub>GHCOLD</sub> = 17 V	11011	V <sub>GHCOLD</sub> = 33 V		
		01100	V <sub>GHCOLD</sub> = 18 V	11100	V <sub>GHCOLD</sub> = 34 V		
		01101	V <sub>GHCOLD</sub> = 19 V	11101	V <sub>GHCOLD</sub> = 35 V		
		01110	V <sub>GHCOLD</sub> = 20 V	11110	V <sub>GHCOLD</sub> = 36 V		
		01111	V <sub>GHCOLD</sub> = 21 V	11111	V <sub>GHCOLD</sub> = 37 V		
<b>Reserved</b>	Bits 7-5	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**VGHCONFIG (05h)**

The VGHMISC register can be written to and read from.

**Table 8. VGHCONFIG Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>		<b>FREQ4</b>		<b>SS4</b>		<b>LX4TS</b>	
<b>LX4TS</b>	Bit	These bits configure the falling speed of VGH boost switch.					
	1-0	00	Tf = 2.2 V/ns				
		01	Tf = 3.5 V/ns				
		10	Tf = 4.8 V/ns				
		11	Tf = 6 V/ns				
<b>SS4</b>	Bit	These bits configure the soft start duration for VGH boost regulator					
	3-2	00	t <sub>SS4</sub> = 4 ms				
		01	t <sub>SS4</sub> = 8 ms				
		10	t <sub>SS4</sub> = 12 ms				
		11	t <sub>SS4</sub> = 16 ms				
<b>FREQ4</b>	Bit	This bit configures the switching frequency of VGH boost regulator					
	4	0	F <sub>VGH_LX</sub> = 400 kHz				
		1	F <sub>VGH_LX</sub> = 800 kHz				
<b>Reserved</b>	Bits	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					
	7-5						

**VGL (06h)**

The **VGL** register can be written to and read from.

**Table 9. VGL Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>		<b>VGL</b>					
<b>VGL</b>	Bits	These bits select VGL output voltage					
	5-0	000000	N.A.	010110	$V_{GL} = -3.9\text{ V}$	101100	$V_{GL} = -6.1\text{ V}$
		000001	N.A.	010111	$V_{GL} = -4.0\text{ V}$	101101	$V_{GL} = -6.2\text{ V}$
		000010	N.A.	011000	$V_{GL} = -4.1\text{ V}$	101110	$V_{GL} = -6.3\text{ V}$
		000011	N.A.	011001	$V_{GL} = -4.2\text{ V}$	101111	$V_{GL} = -6.4\text{ V}$
		000100	N.A.	011010	$V_{GL} = -4.3\text{ V}$	110000	$V_{GL} = -6.5\text{ V}$
		000101	N.A.	011011	$V_{GL} = -4.4\text{ V}$	110001	$V_{GL} = -6.6\text{ V}$
		000110	N.A.	011100	$V_{GL} = -4.5\text{ V}$	110010	$V_{GL} = -6.7\text{ V}$
		000111	N.A.	011101	$V_{GL} = -4.6\text{ V}$	110011	$V_{GL} = -6.8\text{ V}$
		001000	N.A.	011110	$V_{GL} = -4.7\text{ V}$	110100	$V_{GL} = -6.9\text{ V}$
		001001	N.A.	011111	$V_{GL} = -4.8\text{ V}$	110101	$V_{GL} = -7.0\text{ V}$
		001010	N.A.	100000	$V_{GL} = -4.9\text{ V}$	110110	$V_{GL} = -7.1\text{ V}$
		001011	N.A.	100001	$V_{GL} = -5.0\text{ V}$	110111	$V_{GL} = -7.2\text{ V}$
		001100	N.A.	100010	$V_{GL} = -5.1\text{ V}$	111000	$V_{GL} = -7.3\text{ V}$
		001101	N.A.	100011	$V_{GL} = -5.2\text{ V}$	111001	$V_{GL} = -7.4\text{ V}$
		001110	N.A.	100100	$V_{GL} = -5.3\text{ V}$	111010	$V_{GL} = -7.5\text{ V}$
		001111	N.A.	100101	$V_{GL} = -5.4\text{ V}$	111011	$V_{GL} = -7.6\text{ V}$
		010000	N.A.	100110	$V_{GL} = -5.5\text{ V}$	111100	$V_{GL} = -7.7\text{ V}$
		010001	N.A.	100111	$V_{GL} = -5.6\text{ V}$	111101	$V_{GL} = -7.8\text{ V}$
		010010	N.A.	101000	$V_{GL} = -5.7\text{ V}$	111110	$V_{GL} = -7.9\text{ V}$
		010011	N.A.	101001	$V_{GL} = -5.8\text{ V}$	111111	$V_{GL} = -8.0\text{ V}$
		010100	N.A.	101010	$V_{GL} = -5.9\text{ V}$		
		010101	$V_{GL} = -3.8\text{ V}$	101011	$V_{GL} = -6.0\text{ V}$		
<b>Reserved</b>	Bits 7-6	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**V25 (07h)**

The **V25** register can be written to and read from.

**Table 10. V25 Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>				<b>V25</b>			

<b>V25</b>	Bits	These bits select V25 buck converter's output voltage					
	3-0	0000	$V_{25} = 1.5\text{ V}$	1000	$V_{25} = 2.3\text{ V}$		
		0001	$V_{25} = 1.6\text{ V}$	1001	$V_{25} = 2.4\text{ V}$		
		0010	$V_{25} = 1.7\text{ V}$	1010	$V_{25} = 2.5\text{ V}$		
		0011	$V_{25} = 1.8\text{ V}$	1011	$V_{25} = 2.6\text{ V}$		
		0100	$V_{25} = 1.9\text{ V}$	1100	$V_{25} = 2.7\text{ V}$		
		0101	$V_{25} = 2.0\text{ V}$	1101	$V_{25} = 2.8\text{ V}$		
		0110	$V_{25} = 2.1\text{ V}$	1110	$V_{25} = 2.9\text{ V}$		
		0111	$V_{25} = 2.2\text{ V}$	1111	$V_{25} = 3.0\text{ V}$		
<b>Reserved</b>	Bits 7-4	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**VDIV (08h)**

The **VDIV** register can be written to and read from.

**Table 11. VDIV Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>				<b>VDIV</b>			

<b>VDIV</b>	Bits	These bits select the threshold voltage of the $\overline{\text{RESET}}$ signal					
	3-0	000	$V_{\text{DIV}} = 1.2\text{ V}$				
		001	$V_{\text{DIV}} = 1.4\text{ V}$				
		010	$V_{\text{DIV}} = 1.6\text{ V}$				
		011	$V_{\text{DIV}} = 1.8\text{ V}$				
		100	$V_{\text{DIV}} = 2.0\text{ V}$				
		101	$V_{\text{DIV}} = 2.2\text{ V}$				
		110	$V_{\text{DIV}} = 2.4\text{ V}$				
		111	$V_{\text{DIV}} = 2.6\text{ V}$				
<b>Reserved</b>	Bits 7-4	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**RESET (09h)**

The **RESET** register can be written to and read from.

**Table 12. RESET Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>				<b>RESET</b>			

<b>RESET</b>	Bits	These bits select the $\overline{\text{RESET}}$ generate delay time period					
	3-0	0000	$T_{\text{RESET}} = 0 \text{ ms}$	1000	$T_{\text{RESET}} = 16 \text{ ms}$		
		0001	$T_{\text{RESET}} = 2 \text{ ms}$	1001	$T_{\text{RESET}} = 18 \text{ ms}$		
		0010	$T_{\text{RESET}} = 4 \text{ ms}$	1010	$T_{\text{RESET}} = 20 \text{ ms}$		
		0011	$T_{\text{RESET}} = 6 \text{ ms}$	1011	$T_{\text{RESET}} = 22 \text{ ms}$		
		0100	$T_{\text{RESET}} = 8 \text{ ms}$	1100	$T_{\text{RESET}} = 24 \text{ ms}$		
		0101	$T_{\text{RESET}} = 10 \text{ ms}$	1101	$T_{\text{RESET}} = 26 \text{ ms}$		
		0110	$T_{\text{RESET}} = 12 \text{ ms}$	1110	$T_{\text{RESET}} = 28 \text{ ms}$		
		0111	$T_{\text{RESET}} = 14 \text{ ms}$	1111	$T_{\text{RESET}} = 30 \text{ ms}$		
<b>Reserved</b>	Bits 7-4	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**DLY (0Ah)**

The **DLY** register can be written to and read from.

**Table 13. DLY Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>Reserved</b>					<b>DLY</b>		

<b>DLY</b>	Bits	These bits configure the gate voltage shaping delay time period					
	1-0	00	$V_{\text{DLY}} = 0 \text{ ms}$				
		01	$V_{\text{DLY}} = 20 \text{ ms}$				
		10	$V_{\text{DLY}} = 40 \text{ ms}$				
		11	$V_{\text{DLY}} = 60 \text{ ms}$				
<b>Reserved</b>	Bits 7-2	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.					

**VCOMHOT (0Bh)**

 The **VCOMHOT1** register can be written to and read from.

**Table 14. VCOMHOT Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>VCOMHOT</b>							
<b>VCOMHOT</b>	Bits	These bits select VCOM output voltage at hot temperatures (VCOMT = 0) or all temperature range (VCOMT = 1).					
		<b>VCOMR = 0</b>	<b>VCOMR = 1</b>				
	00000000	V <sub>COMHOT</sub> = N.A	V <sub>COMHOT</sub> = N.A				
	00000001	V <sub>COMHOT</sub> = N.A	V <sub>COMHOT</sub> = N.A				
	00000010	V <sub>COMHOT</sub> = N.A	V <sub>COMHOT</sub> = N.A				
	.....	V <sub>COMHOT</sub> = N.A	V <sub>COMHOT</sub> = N.A				
	00100111	V <sub>COMHOT</sub> = N.A	V <sub>COMHOT</sub> = N.A				
	00101000	V <sub>COMHOT</sub> = 0.80 V	V <sub>COMHOT</sub> = 0.20 V				
	00101001	V <sub>COMHOT</sub> = 0.82 V	V <sub>COMHOT</sub> = 0.18 V				
	00101010	V <sub>COMHOT</sub> = 0.84 V	V <sub>COMHOT</sub> = 0.16 V				
	00101011	V <sub>COMHOT</sub> = 0.86 V	V <sub>COMHOT</sub> = 0.14 V				
	10111100	V <sub>COMHOT</sub> = 0.86 V	V <sub>COMHOT</sub> = 0.12 V				
	.....	.....	.....				
	11111101	V <sub>COMHOT</sub> = 5.06 V	V <sub>COMHOT</sub> = -4.06 V				
	11111110	V <sub>COMHOT</sub> = 5.08 V	V <sub>COMHOT</sub> = -4.08 V				
	11111111	V <sub>COMHOT</sub> = 5.10 V	V <sub>COMHOT</sub> = -4.10 V				

**VCOMCOLD (0Ch)**

 The **VCOMCOLD** register can be written to and read from.

**Table 15. VCOMCOLD Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>VCOMCOLD</b>							
<b>VCOMCOLD</b>	Bits	These bits select VCOM output voltage at cold temperatures (VCOMT=0)					
		<b>VCOMR = 0</b>	<b>VCOMR = 1</b>				
	00000000	V <sub>COMCOLD</sub> = N.A	V <sub>COMCOLD</sub> = N.A				
	00000001	V <sub>COMCOLD</sub> = N.A	V <sub>COMCOLD</sub> = N.A				
	00000010	V <sub>COMCOLD</sub> = N.A	V <sub>COMCOLD</sub> = N.A				
	.....	V <sub>COMCOLD</sub> = N.A	V <sub>COMCOLD</sub> = N.A				
	00100111	V <sub>COMCOLD</sub> = N.A	V <sub>COMCOLD</sub> = N.A				
	00101000	V <sub>COMCOLD</sub> = 0.80 V	V <sub>COMCOLD</sub> = 0.20 V				
	00101001	V <sub>COMCOLD</sub> = 0.82 V	V <sub>COMCOLD</sub> = 0.18 V				
	00101010	V <sub>COMCOLD</sub> = 0.84 V	V <sub>COMCOLD</sub> = 0.16 V				
	00101011	V <sub>COMCOLD</sub> = 0.86 V	V <sub>COMCOLD</sub> = 0.14 V				
	10111100	V <sub>COMCOLD</sub> = 0.86 V	V <sub>COMCOLD</sub> = 0.12 V				
	.....	.....	.....				
	11111101	V <sub>COMCOLD</sub> = 5.06 V	V <sub>COMCOLD</sub> = -4.06 V				
	11111110	V <sub>COMCOLD</sub> = 5.08 V	V <sub>COMCOLD</sub> = -4.08 V				
	11111111	V <sub>COMCOLD</sub> = 5.10 V	V <sub>COMCOLD</sub> = -4.10 V				

**Control (FFh)****Table 16. Control Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>WED</b>	<b>Reserved</b>						<b>RED</b>

<b>RED</b>	Bit	The state of this bit determines whether read operations return the contents of the DAC registers or the contents of the E <sup>2</sup> PROM
	0	0 Read operations return the contents of the DAC registers
	1	1 Read operations return the contents of the E <sup>2</sup> PROM
<b>Reserved</b>	Bits 6-1	These bits are reserved for future use. During write operations data intended for these bits is ignored, and during read operations 0 is returned.
<b>WED</b>	Bit 7	Setting this bit forces the contents of all DAC registers to be copied into E <sup>2</sup> PROM, thereby making them the default values during power-up. When the contents of all the DAC registers have been written to the E <sup>2</sup> PROM, the TPS65640 automatically resets this bit.



**Example – Writing to a Single RAM Register**

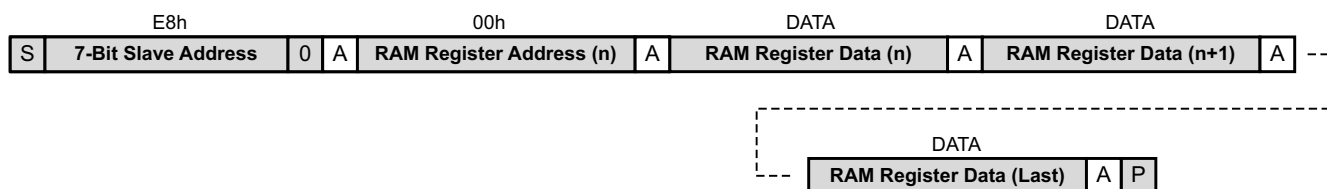
1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of RAM register (00h).
5. TPS65640 acknowledges.
6. Bus master sends data to be written.
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.



**Figure 41. Writing to a Single RAM Register**

**Example – Writing to Multiple RAM Registers**

1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of first RAM register to be written to (00h).
5. TPS65640 acknowledges.
6. Bus master sends data to be written to first RAM register.
7. TPS65640 acknowledges.
8. Bus master sends data to be written to RAM register at next higher address (auto-increment).
9. TPS65640 acknowledges.
10. Steps (8) and (9) repeated until data for final RAM register has been sent.
11. TPS65640 acknowledges.
12. Bus master sends STOP condition.



**Figure 42. Writing to Multiple RAM Registers**

**Example – Saving Contents of all RAM Registers to E<sup>2</sup>PROM**

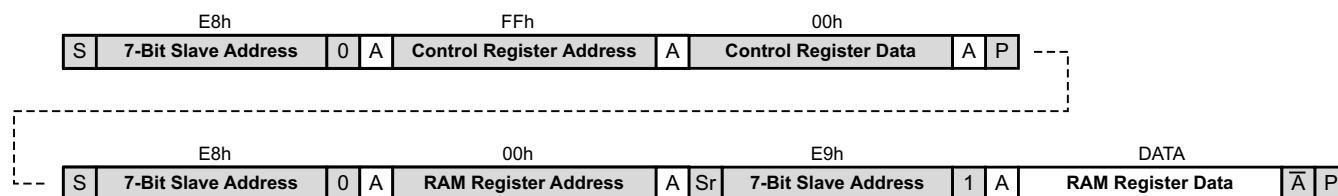
1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of Control Register (FFh).
5. TPS65640 acknowledges.
6. Bus master sends data to be written to the Control Register (80h).
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.

**Figure 43. Saving Contents of all RAM Registers to E<sup>2</sup>PROM**

The TPS65640 needs 50ms time period after TPS65640 receiving STOP condition for saving all RAM registers data to E<sup>2</sup>PROM. If bus master send 7-bit slave address to call TPS65640 again within 50ms period, the TPS65640 will pull down the SCL line to LOW until the all RAM registers data saving to E<sup>2</sup>PROM is completed.

**Example – Reading from a Single RAM Register**

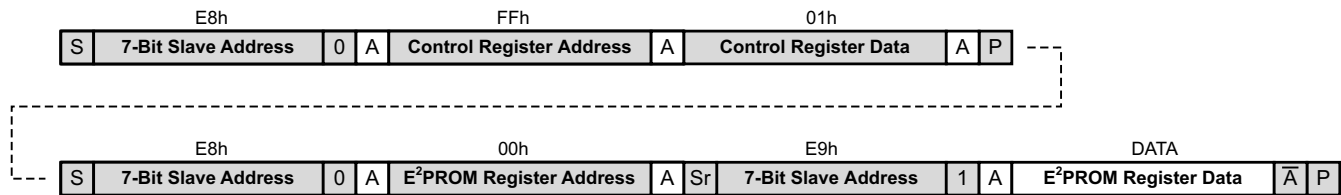
1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of Control Register (FFh).
5. TPS65640 acknowledges.
6. Bus master sends data for Control Register (00h).
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.
9. Bus master sends START condition.
10. Bus master sends 7-bit slave address plus low R/W bit (E8h).
11. TPS65640 acknowledges.
12. Bus master sends address of RAM register (00h).
13. TPS65640 acknowledges.
14. Bus master sends REPEATED START condition.
15. Bus master sends 7-bit slave address plus high R/W bit (E9h).
16. TPS65640 acknowledges.
17. TPS65640 sends RAM register data.
18. Bus master does not acknowledge.
19. Bus master sends STOP condition.



**Figure 44. Reading from a Single RAM Register**

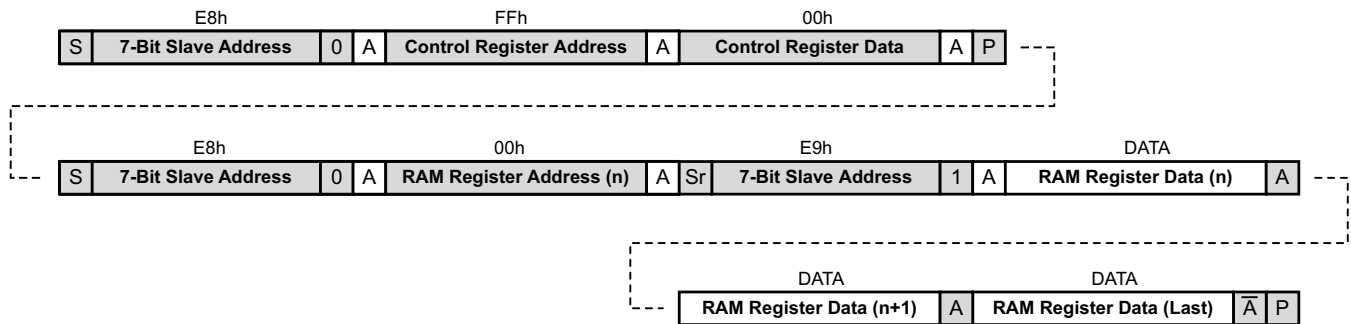
**Example – Reading from a Single E<sup>2</sup>PROM Register**

1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of Control Register (FFh).
5. TPS65640 acknowledges.
6. Bus master sends data for Control Register (01h).
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.
9. Bus master sends START condition.
10. Bus master sends 7-bit slave address plus low R/W bit (E8h).
11. TPS65640 acknowledges.
12. Bus master sends address of E<sup>2</sup>PROM register (00h).
13. TPS65640 acknowledges.
14. Bus master sends REPEATED START condition.
15. Bus master sends 7-bit slave address plus high R/W bit (E9h).
16. TPS65640 acknowledges.
17. TPS65640 sends E<sup>2</sup>PROM register data.
18. Bus master does not acknowledge.
19. Bus master sends STOP condition.

**Figure 45. Reading from a Single E<sup>2</sup>PROM Register**

**Example – Reading from Multiple RAM Registers**

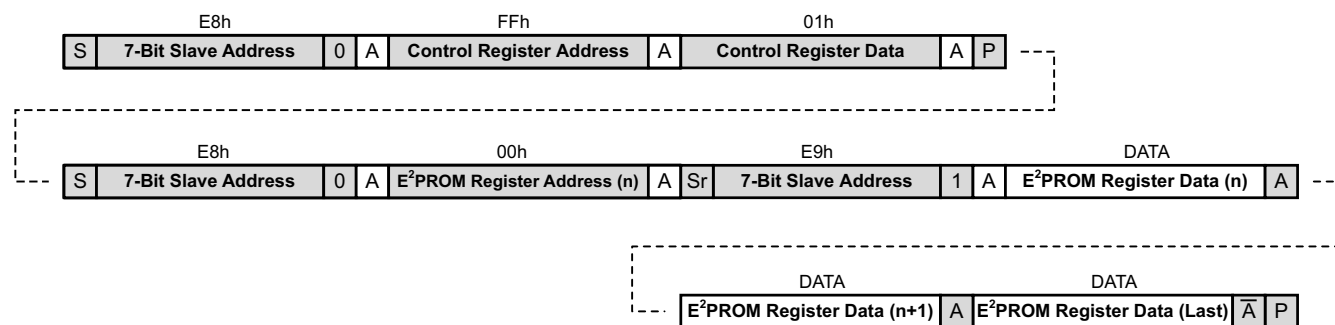
1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of Control Register (FFh).
5. TPS65640 acknowledges.
6. Bus master sends data for Control Register (00h).
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.
9. Bus master sends START condition.
10. Bus master sends 7-bit slave address plus low R/W bit (E8h).
11. TPS65640 acknowledges.
12. Bus master sends address of first register to be read (00h).
13. TPS65640 acknowledges.
14. Bus master sends REPEATED START condition.
15. Bus master sends 7-bit slave address plus high R/W bit (E9h).
16. TPS65640 acknowledges.
17. TPS65640 sends contents of first RAM register to be read.
18. Bus master acknowledges.
19. Bus master sends contents of second RAM register to be read.
20. Bus master acknowledges.
21. TPS65640 sends contents of third (last) RAM register to be read.
22. Bus master does not acknowledge.
23. Bus master sends STOP condition.



**Figure 46. Reading from Multiple RAM Registers**

**Example – Reading from Multiple E<sup>2</sup>PROM Registers**

1. Bus master sends START condition.
2. Bus master sends 7-bit slave address plus low R/W bit (E8h).
3. TPS65640 acknowledges.
4. Bus master sends address of Control Register (FFh).
5. TPS65640 acknowledges.
6. Bus master sends data for Control Register (01h).
7. TPS65640 acknowledges.
8. Bus master sends STOP condition.
9. Bus master sends START condition.
10. Bus master sends 7-bit slave address plus low R/W bit (E8h).
11. TPS65640 acknowledges.
12. Bus master sends address of first E<sup>2</sup>PROM register to be read (00h).
13. TPS65640 acknowledges.
14. Bus master sends REPEATED START condition.
15. Bus master sends 7-bit slave address plus high R/W bit (E9h).
16. TPS65640 acknowledges.
17. TPS65640 sends contents of first E<sup>2</sup>PROM register to be read.
18. Bus master acknowledges.
19. Bus master sends contents of second E<sup>2</sup>PROM register to be read.
20. Bus master acknowledges.
21. TPS65640 sends contents of third (last) E<sup>2</sup>PROM register to be read.
22. Bus master does not acknowledge.
23. Bus master sends STOP condition.

**Figure 47. Reading from Multiple E<sup>2</sup>PROM Registers**

## Configuration Parameter VCOM

The **VCOM** register can be written to and read from.

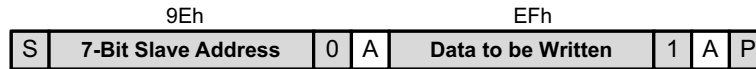
**Table 17. VCOM Register Bit Allocation**

Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0
<b>VCOM</b>							<b>P</b>

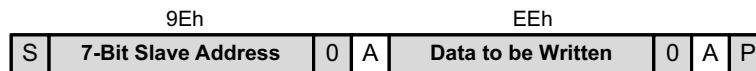
<b>P</b>	Bit	During write operations, this bit determines the target for the data:
	0	0 = Data written to E2PROM and RAM register 1 = Data written to RAM register only
		During read operations this bit indicates whether the contents of the E2PROM and RAM register are the same
		0 = E2PROM and RAM register contents are the same 1 = E2PROM and RAM register contents are different
<b>VCOM</b>	Bits	During write operations, these bits contain the data to be written.
	7-1	During read operations, these bits return the contents of the RAM. The factory default setting is <b>1000000</b> . Where VCOM is a 7-bit integer between 0 and 127 decimal.

**Example – Writing a VCOM Value of 77h to VCOM Register Only**

1. The bus master sends a START condition.
2. The bus Master sends (9E hexadecimal (7-bit slave address plus low R/W bit).
3. TPS65640 slave acknowledges.
4. The bus master sends EF hexadecimal (data to be written plus LSB = '1').
5. The TPS65640 slave acknowledges.
6. The bus master sends a STOP condition.

**Figure 48. Writing a VCOM Value of 77h to RAM Only****Example – Writing a VCOM Value of 77h to E<sup>2</sup>PROM and RAM**

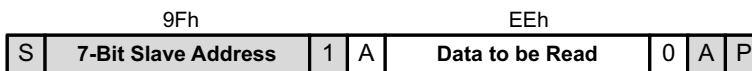
1. The bus master sends a START condition.
2. The bus Master sends 9E hexadecimal (7-bit slave address plus low R/W bit).
3. TPS65640 slave acknowledges.
4. The bus master sends EE hexadecimal (data to be written plus LSB = '0').
5. The TPS65640 slave acknowledges.
6. The bus master sends a STOP condition.

**Figure 49. Writing a VCOM Value of 77h to E<sup>2</sup>PROM and RAM**



**Example – Reading a VCOM Value of 77h from RAM when E<sup>2</sup>PROM Contents are Identical**

1. The bus master sends a START condition.
2. The bus Master sends 9F hexadecimal (7-bit slave address plus low R/W bit).
3. TPS65640 slave acknowledges.
4. The bus master sends EE hexadecimal from E<sup>2</sup>PROM (data to be read plus LSB = '0').
5. The bus master does not acknowledge.
6. The bus master sends a STOP condition.



**Figure 50. Reading 77h from RAM when E<sup>2</sup>PROM Contents are Identical**

**Example – Reading a VCOM Value of 77h from RAM when E<sup>2</sup>PROM Contents are Different**

1. The bus master sends a START condition.
2. The bus Master sends 9F hexadecimal (7-bit slave address plus low R/W bit).
3. TPS65640 slave acknowledges.
4. The bus master sends EF hexadecimal from RAM (data to be read plus LSB = '1').
5. The bus master does not acknowledge.
6. The bus master sends a STOP condition.



**Figure 51. Reading 77h from E<sup>2</sup>PROM when RAM Contents are Different**

**I<sup>2</sup>C INTERFACE**

Configuration parameters and the V<sub>COM</sub> voltage setting are programmed via an industry standard I<sup>2</sup>C serial interface. The TPS65640 always works as a slave device and supports standard (100kbps) and fast (400kbps) modes of operation.

During write operations, all further attempts to access its slave addresses are ignored until the current write operation has completed.

## POWER SEQUENCY

Buck converter ( $V_{25\text{Buck}}$ ) or the linear regulator ( $V_{25\text{LDO}}$ ) start as soon as  $V_{\text{IN}} > V_{\text{UVLO}}$ .

The reset generator holds  $\overline{\text{RST}}$  low until  $t_{\text{RESET}}$  seconds after  $V_{25}$  has reached power good status.

Boost converter 1 starts after  $V_{25}$  reached power good status.

Boost converter 2 starts as soon as  $\text{AV}_{\text{DD}}$  has reached power good status.

Figure 52 show the typical power-up/down characteristic of the TPS65640.

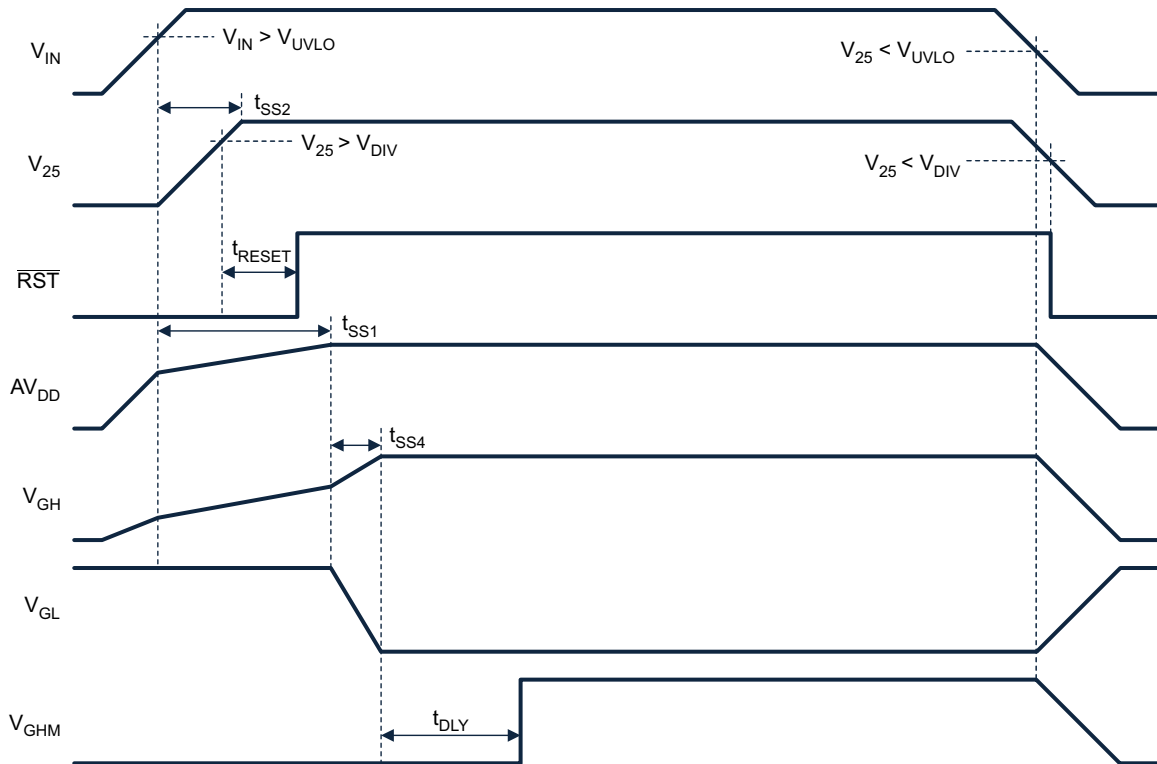
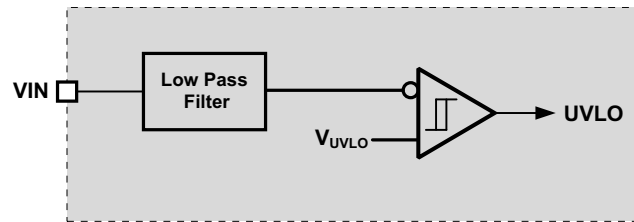


Figure 52. Power-Up and Power-Down Sequencing

## UNDERVOLTAGE LOCKOUT

An undervoltage lockout function disables the IC when the supply voltage is too low for proper operation. A low-pass filter at the input of the UVLO comparator ensures that short transients on  $V_{IN}$  do not cause premature shutdown of the IC.



**Figure 53. Undervoltage Lockout Comparator with Low-Pass Filter**

## THERMAL SHUTDOWN

A thermal shutdown function automatically disables all functions if the device's junction temperature exceeds the safe maximum. The device automatically starts operating again once it has cooled down and operation may safely continue. A restart after a thermal shutdown event follows the same sequence as following a normal power-up condition (see [Figure 52](#)).

APPLICATION INFORMATION

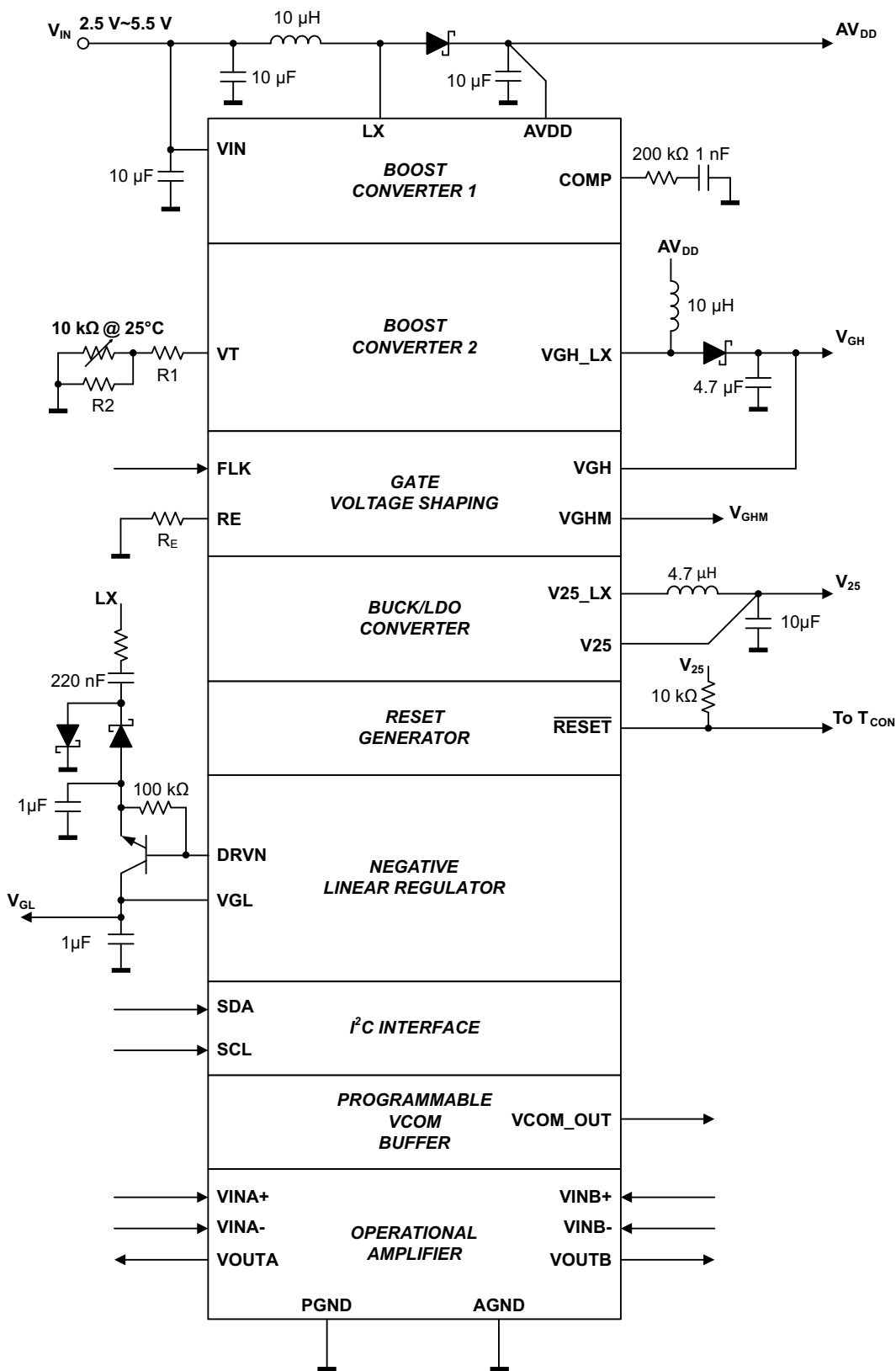
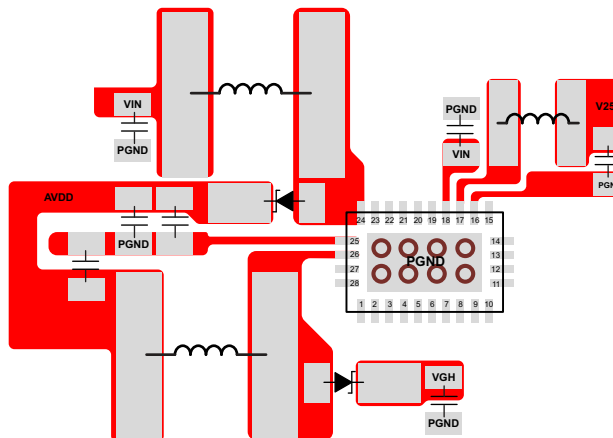


Figure 54. Typical Application Circuit

## LAYOUT RECOMMENDATION

As for all switching power supplies, especially those providing high current and using high switching frequencies, layout is an important design step. If layout is not carefully done, the regulator could show instability as well as EMI problems. Therefore, use wide and short traces for high current paths. The input capacitor in the typical application circuit, should also be placed close to the VIN pin, but also to the GND in order to reduce the input ripple seen by the IC. The LX pin carries high current with fast rising and falling edges. Therefore, the connection between the pin to the inductor and schottky diode should be kept as short and wide as possible. It is also beneficial to have the ground of the output capacitor for both Boost converter 1, Boost converter 2 and Buck converter close to the PGND pin since there is a large ground return current flowing between them. When laying out signal grounds, it is recommended to use short traces separated from power ground traces, and connect them together at a single point, for example on the thermal pad. The thermal pad needs to be soldered on to the PCB and connected to the GND pin of the IC. An additional thermal via can significantly improve power dissipation of the IC.



**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp (3)	Op Temp (°C)	Top-Side Markings (4)	Samples
TPS65640RHRR	PREVIEW	WQFN	RHR	28	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	PZXI	

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

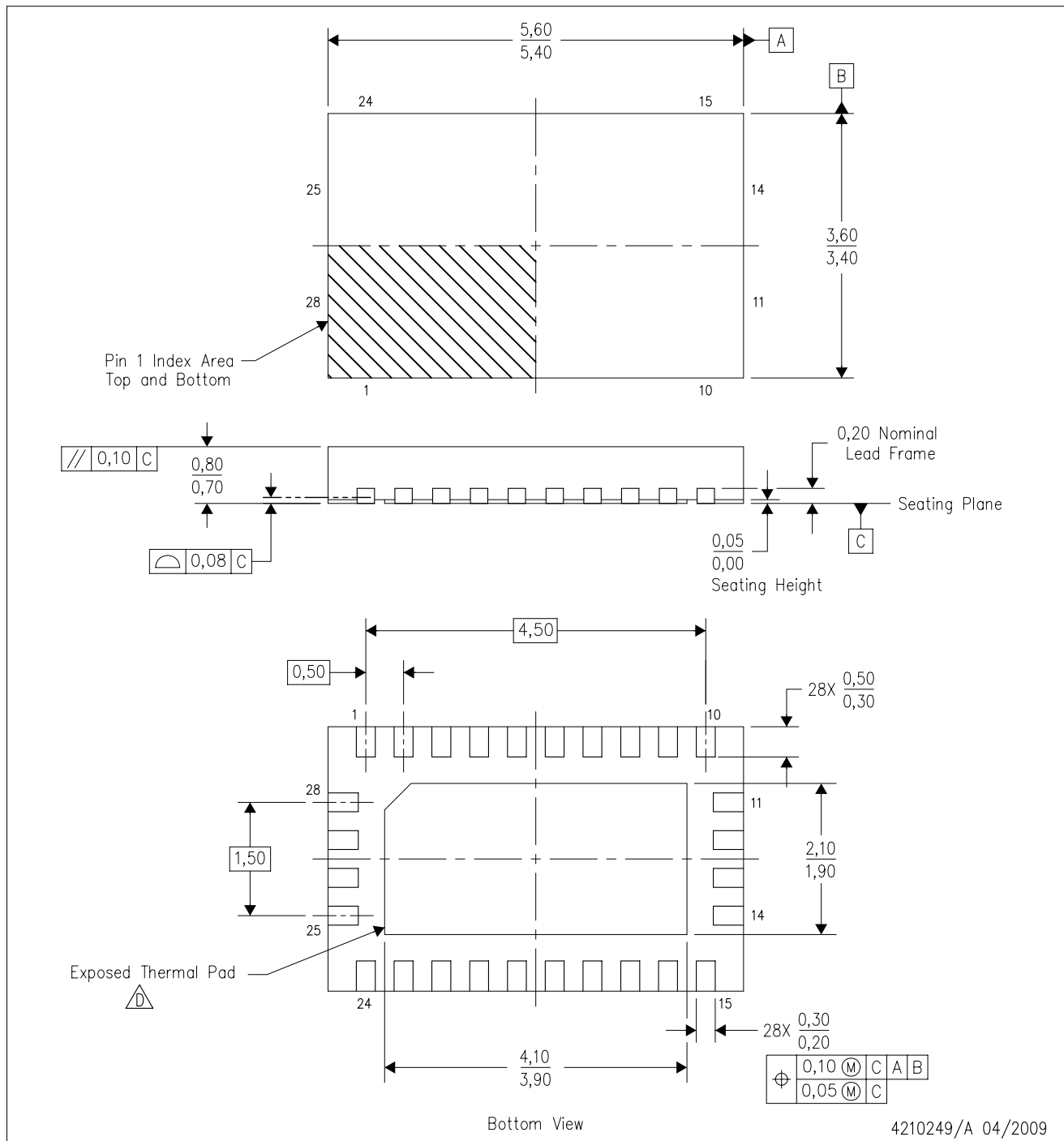
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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

# MECHANICAL DATA

RHR (R-PWQFN-N28)

PLASTIC QUAD FLATPACK NO-LEAD



- NOTES:
- All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - This drawing is subject to change without notice.
  - QFN (Quad Flatpack No-Lead) package configuration.
  - The package thermal pad must be soldered to the board for thermal and mechanical performance.
  - Reference JEDEC MO-220.

## THERMAL PAD MECHANICAL DATA

RHR (R-PWQFN-N28)

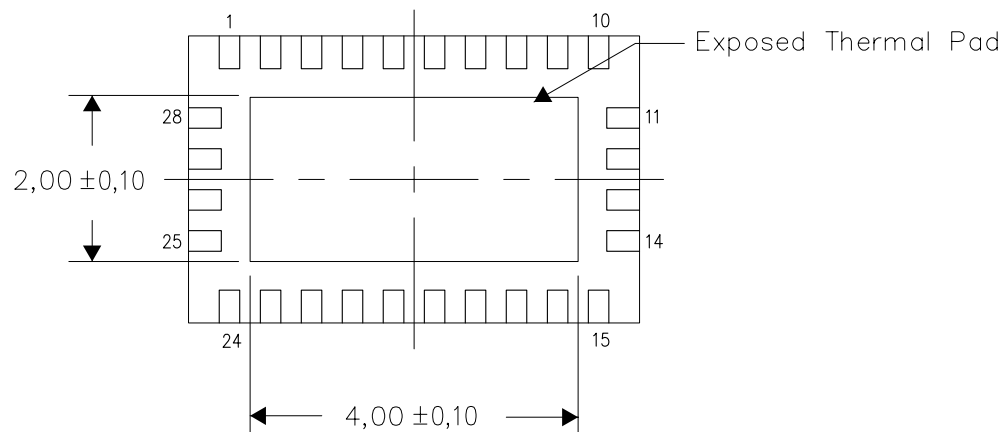
PLASTIC QUAD FLATPACK NO-LEAD

### THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at [www.ti.com](http://www.ti.com).

The exposed thermal pad dimensions for this package are shown in the following illustration.



Bottom View

Exposed Thermal Pad Dimensions

4210524/D 04/11

NOTE: A. All linear dimensions are in millimeters



**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS65640RHRR	ACTIVE	WQFN	RHR	28	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	PZXI	Samples

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

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**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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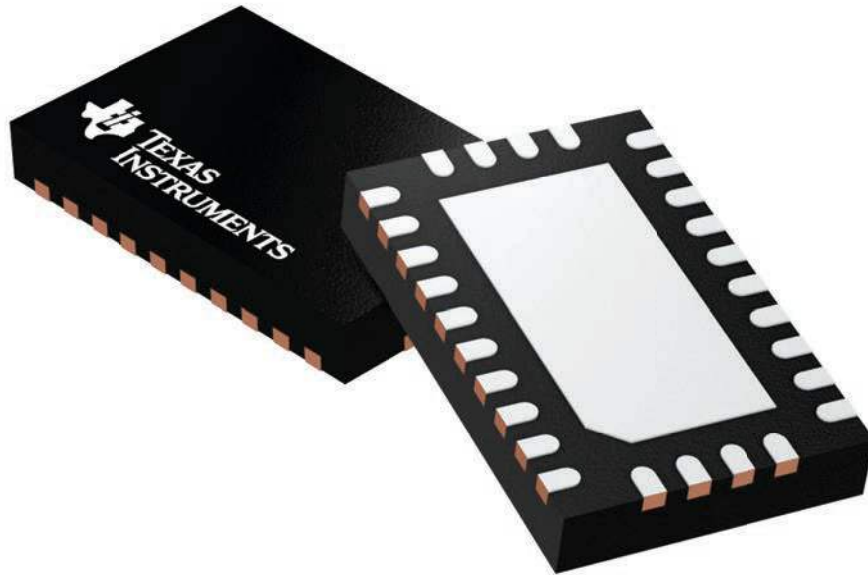
## GENERIC PACKAGE VIEW

**RHR 28**

**WQFN - 0.8 mm max height**

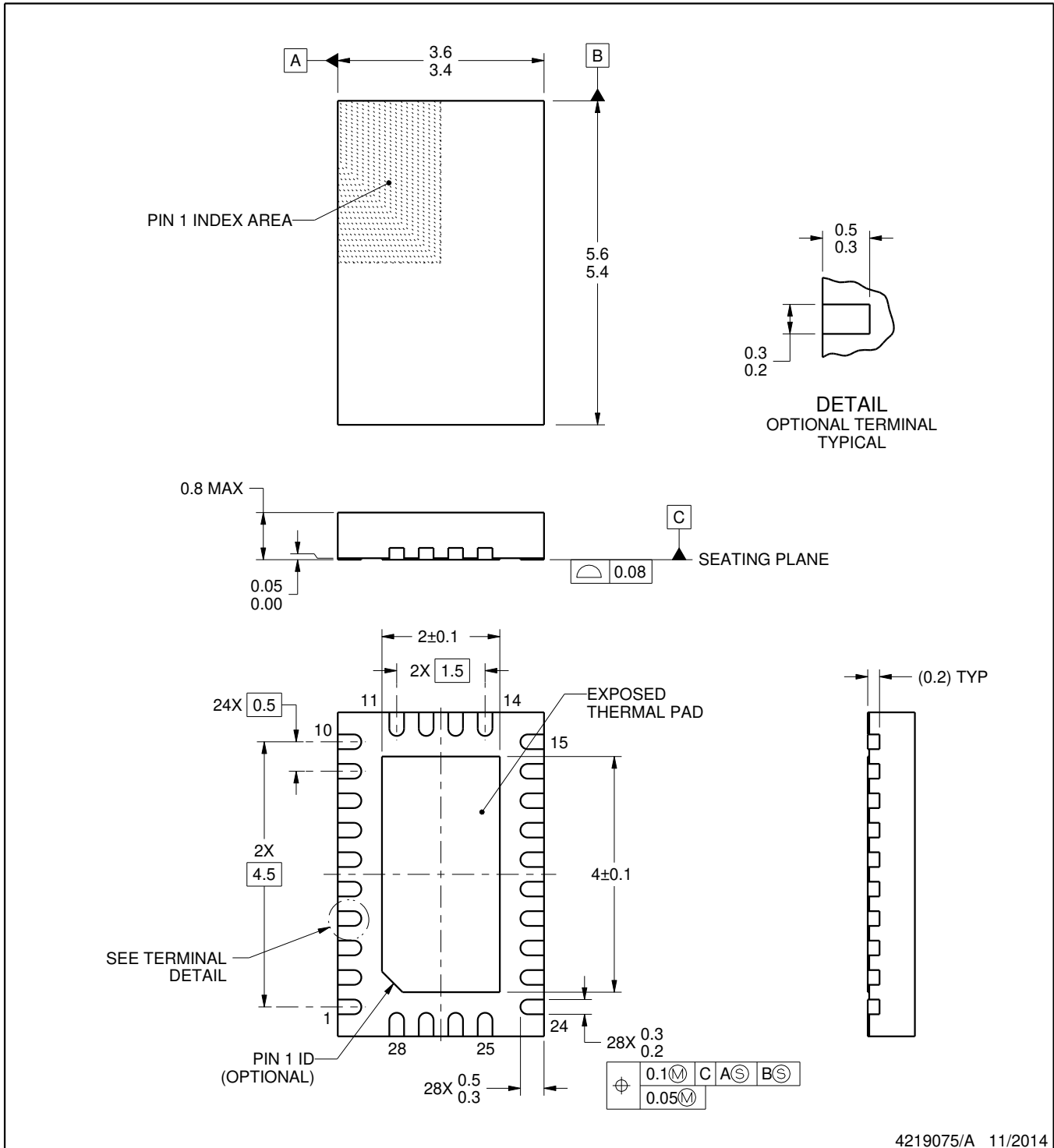
3.5 x 5.5, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD



Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.

4210249/B



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NOTES:

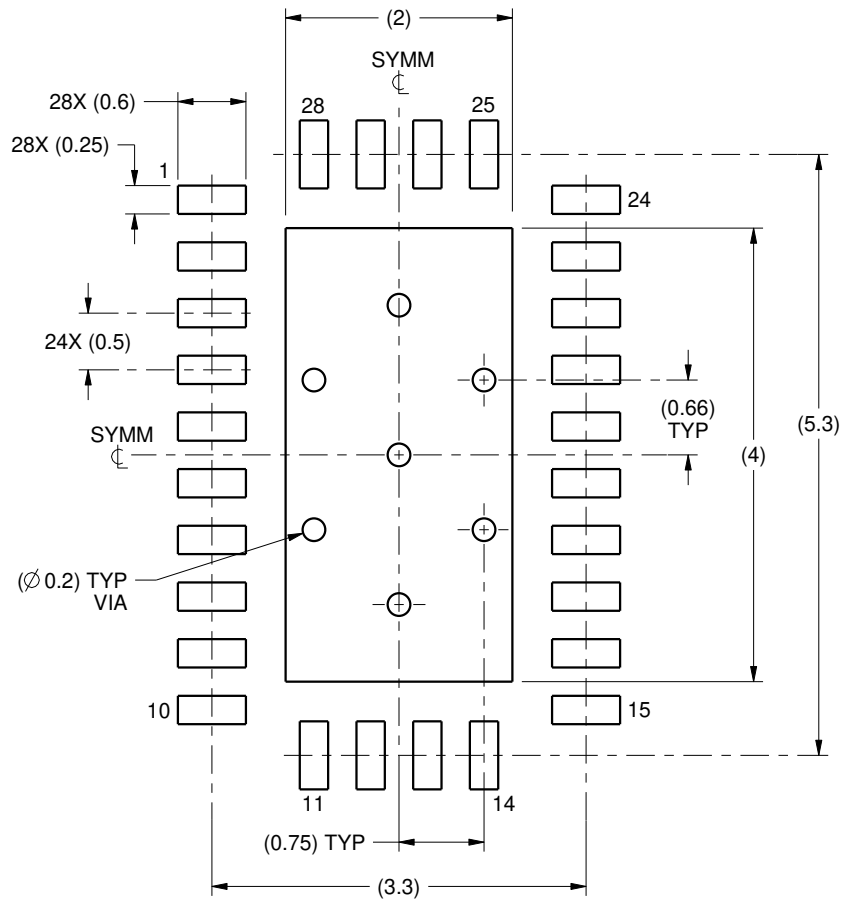
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

# EXAMPLE BOARD LAYOUT

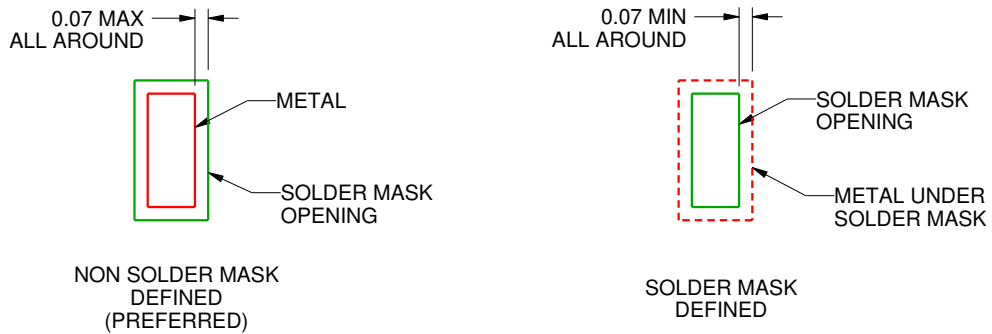
RHR0028A

WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



LAND PATTERN EXAMPLE  
SCALE:15X



SOLDER MASK DETAILS

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NOTES: (continued)

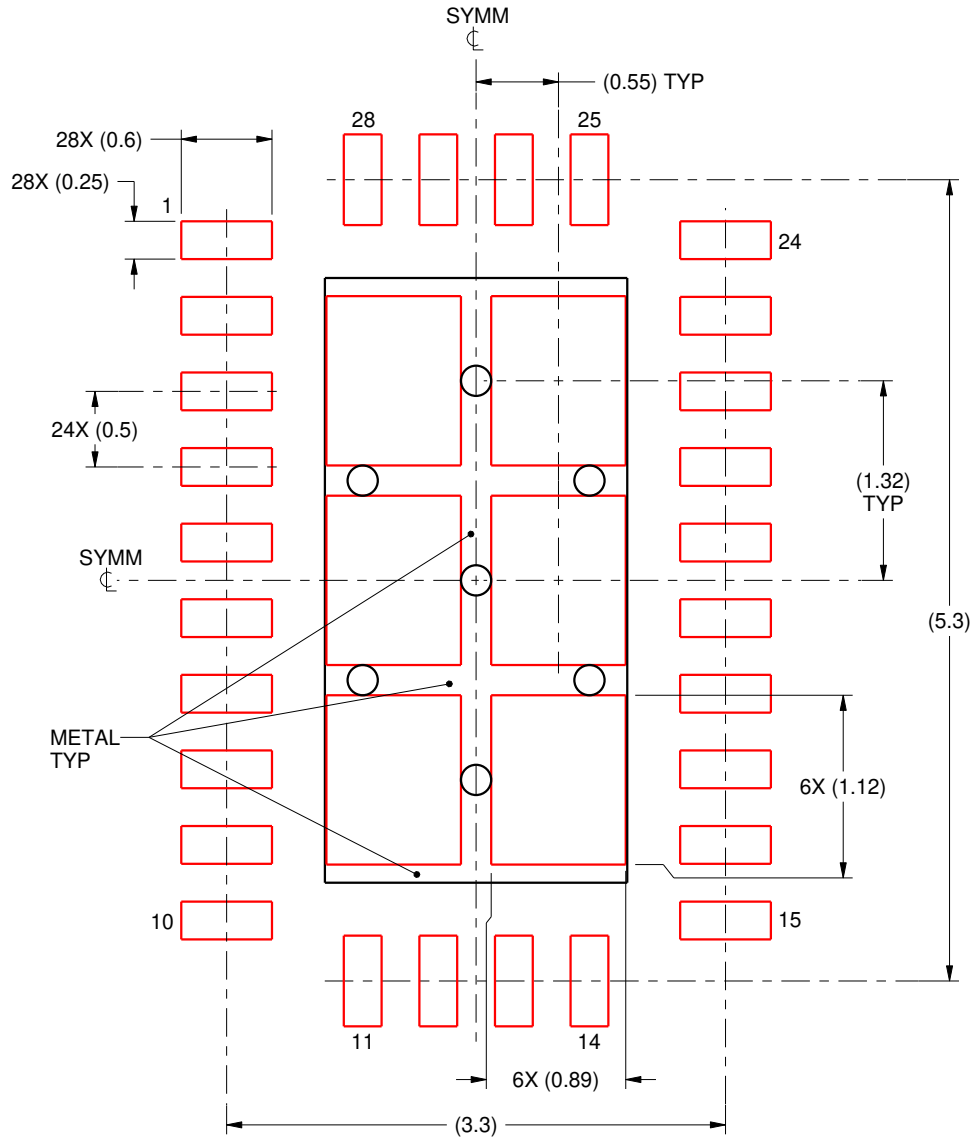
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/slua271](http://www.ti.com/lit/slua271)).

# EXAMPLE STENCIL DESIGN

RHR0028A

WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



**SOLDER PASTE EXAMPLE**  
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD  
75% PRINTED SOLDER COVERAGE BY AREA  
SCALE:20X

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NOTES: (continued)

5. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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