Preferred Device

Power MOSFET 25 Amps, 600 Volts N-Channel TO-264

This high voltage MOSFET uses an advanced termination scheme to provide enhanced voltage-blocking capability without degrading performance over time. In addition, this advanced Power MOSFET is designed to withstand high energy in the avalanche and commutation modes. Designed for high voltage, high speed switching applications in power supplies, converters and PWM motor controls, these devices are particularly well suited for bridge circuits where diode speed and commutating safe operating areas are critical and offer additional safety margin against unexpected voltage transients.

- Robust High Voltage Termination
- Avalanche Energy Specified
- Diode is Characterized for Use in Bridge Circuits
- I_{DSS} and V_{DS(on)} Specified at Elevated Temperature

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	600	Vdc
Drain–Gate Voltage (R_{GS} = 1 M Ω)	V _{DGR}	600	Vdc
Gate–Source Voltage – Continuous – Non–Repetitive (t _p ≤ 10 ms)	V _{GS} V _{GSM}	±20 ±40	Vdc Vpk
Drain Current – Continuous @ $T_C = 25^{\circ}C$ – Single Pulse ($t_p \le 10 \ \mu s$)	I _D I _{DM}	25 65	Adc Apk
Total Power Dissipation Derate above 25°C	PD	300 2.38	Watts W/°C
Operating and Storage Temperature Range	T _J , T _{stg}	-55 to 150	°C
Single Pulse Drain-to-Source Avalanche Energy – Starting $T_J = 25^{\circ}C$ ($V_{DD} = 100 \text{ Vdc}, V_{GS} = 10 \text{ Vdc}, \text{ Peak}$ $I_L = 25 \text{ Apk}, L = 10 \text{ mH}, R_G = 25 \Omega$)	Eas	3000	mJ
Thermal Resistance – Junction to Case – Junction to Ambient	$\begin{array}{c} R_{\theta JC} \\ R_{\theta JA} \end{array}$	0.42 40	°C/W
Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds	ΤL	260	°C

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25 AMPERES 600 VOLTS $R_{DS(on)} = 210 \text{ m}\Omega$

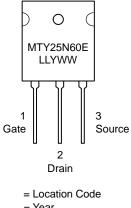
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N-Channel



CASE 340G Style 1

MARKING DIAGRAM **& PIN ASSIGNMENT**



LL = Year Y ww = Work Week

ORDERING INFORMATION

Device	Package	Shipping
MTY25N60E	TO-264	25 Units/Rail

Preferred devices are recommended choices for future use and best overall value.

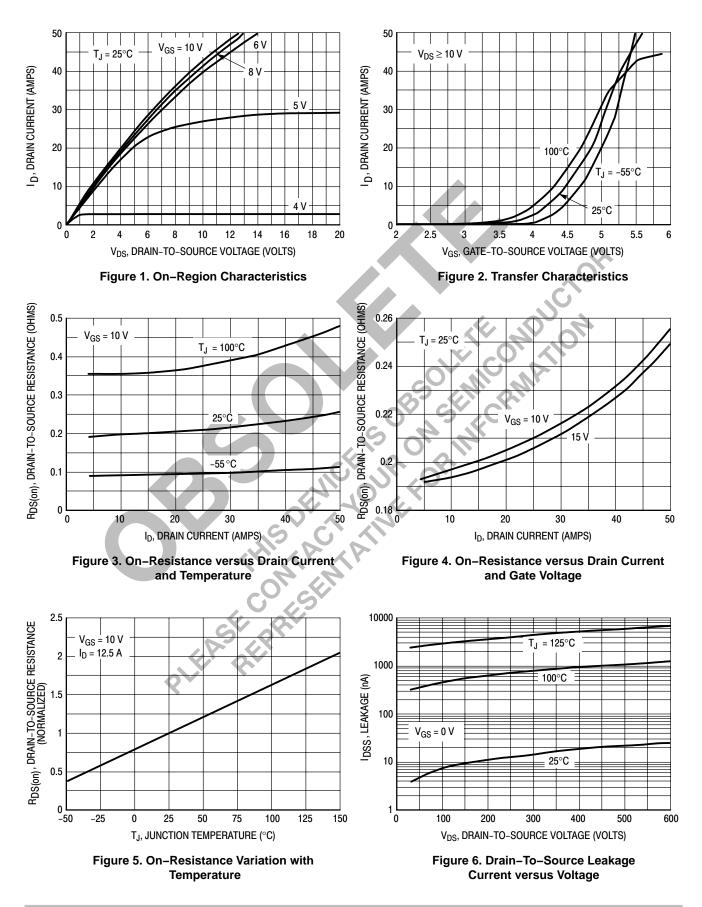
ELECTRICAL CHARACTERISTICS (T₁ = 25°C unless otherwise noted)

Ch	aracteristic	Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS		•		•		
$\begin{array}{l} \text{Drain-Source Breakdown Voltag}\\ (\text{V}_{\text{GS}}=0,\text{I}_{\text{D}}=250\;\mu\text{A})\\ \text{Temperature Coefficient (Posit)} \end{array}$		V _{(BR)DSS}	600 -	_ 714		Vdc mV/°C
$\label{eq:VDS} \begin{array}{l} \mbox{Zero Gate Voltage Drain Current} \\ (V_{DS} = 600 \mbox{ Vdc}, \mbox{ V}_{GS} = 0 \mbox{ Vdc}) \\ (V_{DS} = 600 \mbox{ Vdc}, \mbox{ V}_{GS} = 0 \mbox{ Vdc}, \end{array}$	T _J = 125°C)	I _{DSS}			10 200	μAdc
Gate-Body Leakage Current (VG	$_{\rm S} = \pm 20$ Vdc, V _{DS} = 0)	I _{GSS}	-	-	100	nAdc
ON CHARACTERISTICS (Note 1.)						
Gate Threshold Voltage $(V_{DS} = V_{GS}, I_D = 250 \ \mu Adc)$ Threshold Temperature Coeffic	ient (Negative)	V _{GS(th)}	2 -	- 7	4 -	Vdc mV/°C
Static Drain-Source On-Resista	nce (V _{GS} = 10 Vdc, I _D = 12.5 Adc)	R _{DS(on)}	-	-	0.21	Ohm
$\label{eq:constraint} \begin{array}{l} \mbox{Drain-Source On-Voltage (V_{GS}:} \\ \mbox{(I}_D = 25 \mbox{ Adc}) \\ \mbox{(I}_D = 12.5 \mbox{ Adc}, \mbox{T}_J = 125^{\circ}\mbox{C}) \end{array}$	= 10 Vdc)	V _{DS(on)}	-	5.2 -	6 7	Vdc
Forward Transconductance (V _{DS}	= 15 Vdc, I _D = 12.5 Adc)	9FS	18		-	mhos
YNAMIC CHARACTERISTICS			0	<u>~</u> ,	1	
Input Capacitance		C _{iss}		7300	10220	pF
Output Capacitance	$(V_{DS} = 25 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}, f = 1.0 \text{ MHz})$	C _{oss}	C _Q	700	1100	
Reverse Transfer Capacitance		C _{rss}		110	250	
WITCHING CHARACTERISTICS	(Note 2.)	6				
Turn-On Delay Time		t _{d(on)}	0	32	60	ns
Rise Time	$(V_{DD} = 300 \text{ Vdc}, I_D = 25 \text{ Adc},$	tr	_	90	175	
Turn-Off Delay Time	$- V_{GS} = 10 \text{ Vdc}, \\ R_G = 4.7 \Omega$	t _{d(off)}	_	170	300	
Fall Time		tf	-	110	200	
Gate Charge		Q _T	-	240	350	nC
(See Figure 8)	(V _{DS} = 480 Vdc, I _D = 25 Adc,	Q ₁	-	30	-	1
	V _{GS} = 10 Vdc)	Q ₂	_	110	-	
		Q ₃	_	65	-	
OURCE-DRAIN DIODE CHARA	CTERISTICS					
Forward On–Voltage	$(I_{S} = 25 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $(I_{S} = 25 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 125^{\circ}\text{C})$	V _{SD}		0.9 0.8	1.2 -	Vdc
Reverse Recovery Time		t _{rr}	-	620	-	ns
(See Figure 14)		ta	-	310	_	
Q *	(I _S = 25 Adc, V _{GS} = 0 Vdc, dI _S /dt = 100 A/μs)	t _b	_	310	-	
Reverse Recovery Stored Charge		Q _{RR}	-	10.42	-	μC
NTERNAL PACKAGE INDUCTAN	ICE					
Internal Drain Inductance (Measured from the drain lead	0.25" from package to center of die)	L _D	-	4.5	-	nH

Internal Drain Inductance (Measured from the drain lead 0.25" from package to center of die)	L _D	-	4.5	-	nH
Internal Source Inductance (Measured from the source lead 0.25" from package to source bond pad)	L _S	_	7.5	_	nH

Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.
 Switching characteristics are independent of operating junction temperature.

TYPICAL ELECTRICAL CHARACTERISTICS



POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$

During the rise and fall time interval when switching a resistive load, V_{GS} remains virtually constant at a level known as the plateau voltage, V_{SGP} . Therefore, rise and fall times may be approximated by the following:

$$\label{eq:transform} \begin{split} t_r &= Q_2 \; x \; R_G / (V_{GG} - V_{GSP}) \\ t_f &= Q_2 \; x \; R_G / V_{GSP} \end{split}$$

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_G = the gate drive resistance

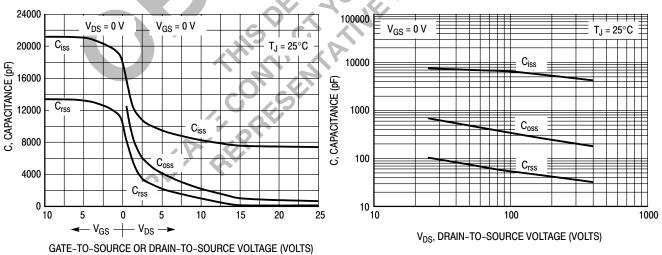
and Q_2 and V_{GSP} are read from the gate charge curve.

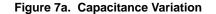
During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

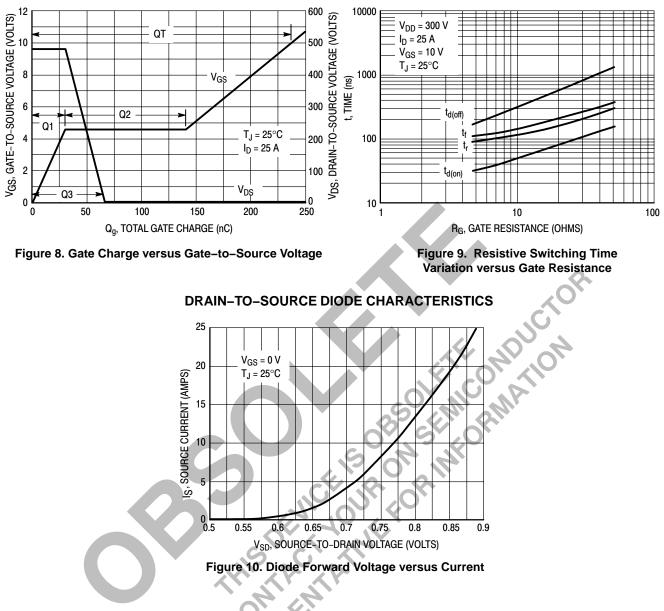
At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.











The Forward Biased Safe Operating Area curves define the maximum simultaneous drain–to–source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance–General Data and Its Use."

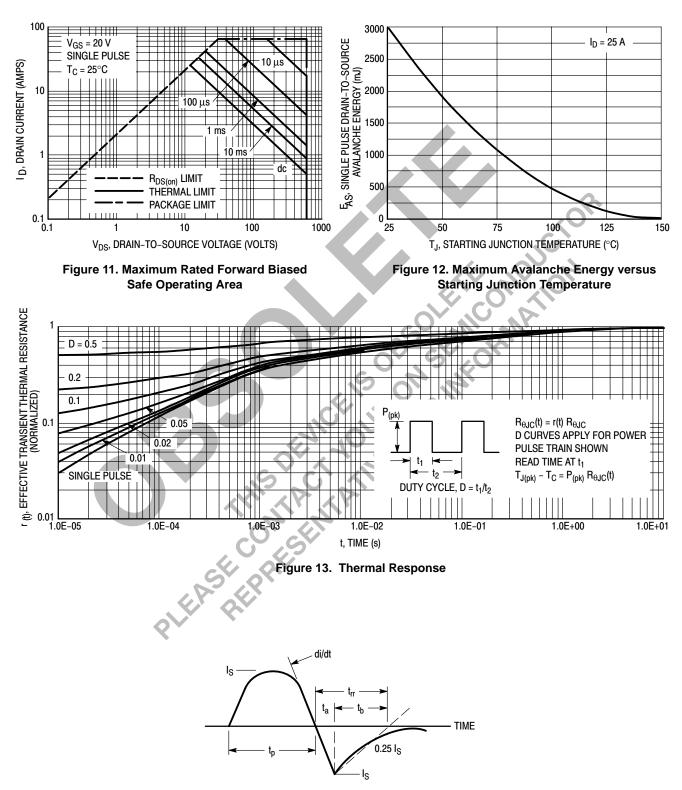
Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (I_{DM}) nor rated voltage (V_{DSS}) is exceeded and the transition time (t_r,t_f) do not exceed 10 µs. In addition the total power averaged over a complete switching cycle must not exceed (T_{J(MAX)} – T_C)/(R_{θJC}).

A Power MOSFET designated E–FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E–FETs can withstand the stress of drain–to–source avalanche at currents up to rated pulsed current (I_{DM}), the energy rating is specified at rated continuous current (I_D), in accordance with industry custom. The energy rating must be derated for temperature as shown

in the accompanying graph (Figure 12). Maximum energy

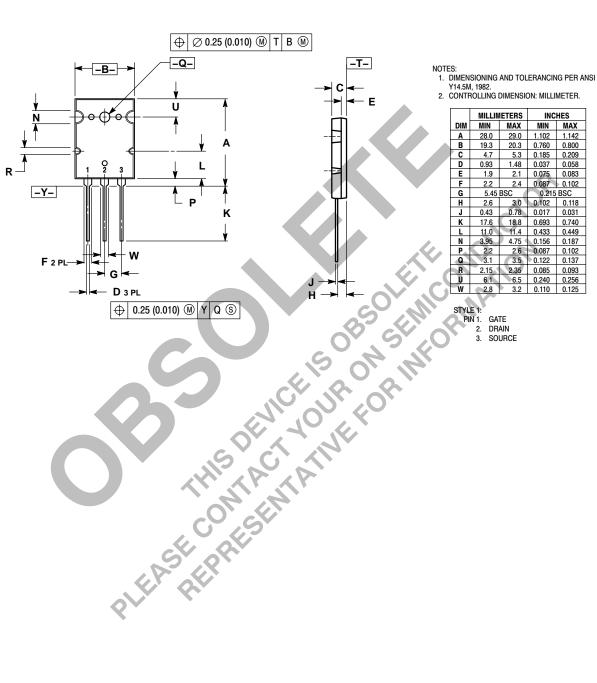
at currents below rated continuous $I_{\rm D}\,\text{can}$ safely be assumed to equal the values indicated.



SAFE OPERATING AREA

Figure 14. Diode Reverse Recovery Waveform

PACKAGE DIMENSIONS



TO-264 CASE 340G-02 ISSUE H

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