

MIC23603

4 MHz PWM 6A Buck Regulator with HyperLight Load®

Features

- Input Voltage: 2.7V to 5.5V
- 6A Output Current
- Up to 93% Efficiency and 81% at 1 mA
- 24 µA Typical Quiescent Current
- 4 MHz PWM Operation in Continuous Mode
- Ultra-Fast Transient Response
- Power Good
- Programmable Soft-Start
- Low Voltage Output Ripple
	- 14 mV_{PP} Ripple in HyperLight Load Mode
	- 5 mV Output Voltage Ripple in Full PWM Mode
- Fully Integrated MOSFET Switches
- 0.01 uA Shutdown Current
- Thermal Shutdown and Current Limit Protection
- Output Voltage as Low as 0.65V
- \cdot 20-pin 4 mm x 5 mm DFN
- -40° C to +125°C Junction Temperature Range

Applications

- 5V POL Supplies
- µC/µP, FPGA and DSP Power
- Test and Measurement Systems
- Barcode Readers
- Set-Top Box, Modems, and DTV
- Distributed Power Systems
- Networking Systems

General Description

The MIC23603 is a high-efficiency 4 MHz 6A synchronous buck regulator with HyperLight Load[®] mode. HyperLight Load provides very high efficiency at light loads and ultra-fast transient response which is perfectly suited for supplying processor core voltages. An additional benefit of this proprietary architecture is very low output ripple voltage throughout the entire load range with the use of small output capacitors. The tiny 4 mm x 5 mm DFN package saves precious board space and requires few external components.

The MIC23603 is designed for use with a very small inductor, down to 0.33 µH, and an output capacitor as small as 47 µF that enables a sub-1 mm height.

The MIC23603 has a very low quiescent current of 24 µA and achieves as high as 81% efficiency at 1 mA. At higher loads, the MIC23603 provides a constant switching frequency around 4 MHz while achieving peak efficiencies up to 93%.

The MIC23603 is available in 20-pin 4 mm x 5mm DFN package with an operating junction temperature range from -40° C to +125 $^{\circ}$ C.

Package Type

Typical Application Circuit

Simplified Functional Block Diagram

1.0 ELECTRICAL CHARACTERISTICS

Absolute Maximum Ratings †

Operating Ratings ††

† Notice: Exceeding absolute maximum rating may cause damage to the device.

†† Notice: The device is not guaranteed to function outside its operating rating.

Note 1: Devices are ESD sensitive. Handling precautions are recommended. Human body model, 1.5 kΩ in series with 100 pF.

ELECTRICAL CHARACTERISTICS [\(Note 1\)](#page-2-0)

Electrical Characteristics: Unless otherwise indicated, $T_A = +25^{\circ}$ C; V_{IN} = V_{EN} = 3.6V; V_{OUT} = 1.8V; L = 0.33 µH; C_{OUT} = 47 µF x 2 unless otherwise specified. **Bold** values indicate -40° C ≤ T_J ≤ +125°C.

Note 1: Specification for packaged product only.

ELECTRICAL CHARACTERISTICS (CONTINUED)(Note 1)

Electrical Characteristics: Unless otherwise indicated, T_A = +25°C; V_{IN} = V_{EN} = 3.6V; V_{OUT} = 1.8V; L = 0.33 µH; $\rm C_{OUT}$ = 47 μF x 2 unless otherwise specified. **Bold** values indicate –40°C ≤ T_J ≤ +125°C.

Note 1: Specification for packaged product only.

TEMPERATURE SPECIFICATIONS [\(Note 1](#page-4-0))

Note 1: The maximum allowable power dissipation is a function of ambient temperature, the maximum allowable junction temperature and the thermal resistance from junction to air (i.e., T_A, T_J, θ_{JA}). Exceeding the maximum allowable power dissipation will cause the device operating junction temperature to exceed the maximum +125°C rating. Sustained junction temperatures above +125°C can impact the device reliability.

2.0 TYPICAL PERFORMANCE CURVES

Note: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

Current.

FIGURE 2-2: Efficiency vs. Output Current V_{OUT} *= 1.8V.*

FIGURE 2-3: Efficiency vs. Output Current V_{OUT} = 1.2V.

FIGURE 2-4: Output Voltage vs. Input Voltage.

FIGURE 2-5: Output Voltage vs. Input Voltage.

Current (HLL).

FIGURE 2-6: Output Voltage vs Output

FIGURE 2-7: Output Voltage vs Output Current (CCM).

FIGURE 2-8: Enable Thresholds vs. Input Voltage.

Temperature.

Temperature.

FIGURE 2-10: Undervoltage Lockout vs.

FIGURE 2-11: PGOOD Delay Time vs. Input Voltage.

Input Voltage.

Temperature.

Temperature.

FIGURE 2-16: Quiescent Current vs. Input Voltage.

FIGURE 2-17: Switching Frequency vs. Load Current.

FIGURE 2-18: Current Limit vs. Input Voltage.

FIGURE 2-19: Maximum Output Current vs. Ambient Temperature.

FIGURE 2-20: Turn-On Input Current.

FIGURE 2-23: Load Transmit 10 mA to 200 mA.

FIGURE 2-24: Load Transmit 10 mA to 500 mA.

FIGURE 2-25: Load Transient 50 mA to 1A.

600 mA.

FIGURE 2-29: Load Transient 200 mA to 3A.

FIGURE 2-30: Load Transient 200 mA to 6A.

FIGURE 2-31: Line Transient 100 mA Load.

FIGURE 2-33: Switching Waveform Discontinuous Mode (1 mA).

FIGURE 2-34: Switching Waveform Discontinuous Mode (10 mA).

FIGURE 2-35: Switching Waveform Discontinuous Mode (50 mA).

FIGURE 2-36: Switching Waveform Continuous Mode (800 mA).

Continuous Mode (2A).

3.0 PIN DESCRIPTIONS

The descriptions of the pins are listed in [Table 3-1.](#page-12-0)

TABLE 3-1: PIN FUNCTION TABLE

4.0 FUNCTIONAL DESCRIPTION

4.1 PVIN

The input supply (PV_{1N}) provides power to the internal MOSFETs for the switch mode regulator and the driver circuitry. The PV $_{IN}$ operating range is 2.7V to 5.5V, so an input capacitor, with a minimum voltage rating of 6.3V, is recommended. Because of the high switching speed, a minimum 10 µF bypass capacitor placed close to V_{IN} and the power ground (PGND) pin is required.

4.2 AVIN

Analog V_{IN} (AV_{IN}) provides power to the internal control and analog circuitry. AV_{IN} and PV_{IN} must be tied together through a 10Ω resistor to minimize noise coupling from PV_{IN} . Consider the layout carefully to reduce high frequency switching noise caused by V_{IN} before reaching AV_{IN}. Place a 1 μ F capacitor as close to AV_{IN} as possible.

4.3 EN

A logic high signal on the enable pin activates the device's output voltage. A logic low signal on the enable pin deactivates the output and reduces supply current to 0.01 µA. The MIC23603 features built-in soft-start circuitry that reduces inrush current and prevents the output voltage from overshooting at start-up. Do not leave EN floating.

4.4 SW

The switch (SW) connects directly to one end of the inductor and provides the current path during switching cycles. The other end of the inductor is connected to the load, SNS pin, and output capacitor. Because of the high speed switching on this pin, route the switch node away from sensitive nodes whenever possible.

4.5 SNS

The sense (SNS) pin is connected to the device's output to provide feedback to the control circuitry. Place the SNS connection close to the output capacitor.

4.6 PG

The power good (PG) pin is an open-drain output that indicates logic high when the output voltage is typically above 90% of its steady state voltage. A pull-up resistor of more than 5 kΩ should be connected from PG to V_{OUT}.

4.7 AGND

The analog ground (AGND) is the ground path for the biasing and control circuitry. The current loop for the signal ground should be separate from the power ground (PGND) loop. Placing a 3Ω resistor between AGND and PGND reduces ground noise.

4.8 PGND

The power ground pin is the ground return path for the inductor current during the freewheeling stage. The current loop for the power ground should be as small as possible and separate from the analog ground (AGND) loop as applicable.

4.9 SS

The soft-start (SS) pin is used to control the output voltage ramp up time. The approximate equation for the ramp time in seconds is:

EQUATION 4-1:

 $250 \times 10^{3} \times L(10) \times C_{SS}$

For example, for C_{SS} = 2.2 nF, T_{RISE} ~ 1.26 ms. See the [Typical Performance Curves](#page-5-0) for a graphical guide. The minimum recommended value for C_{SS} is 2.2 nF.

4.10 FB

The feedback (FB) pin is provided for the adjustable voltage option (no internal connection for fixed options). This is the control input for programming the output voltage. A resistor divider network is connected to this pin from the output and is compared to the internal 0.62V reference within the regulation loop.

Use [Equation 4-2](#page-13-0) to program the output voltage between 0.65V and 3.6V:

EQUATION 4-2:

$$
V_{OUT} = V_{REF} \times \left(1 + \frac{R3}{R4}\right)
$$

Where: R3 is the top resistor, R4 is the bottom resistor.

TABLE 4-1: EXAMPLE FEEDBACK RESISTOR VALUES

5.0 APPLICATION INFORMATION

The MIC23603 is a high-performance DC/DC step-down regulator offering a small solution size. Because it supports an output current up to 6A inside a tiny 4 mm x 5 mm DFN package and requires only three external components, the MIC23603 meets todayís miniature portable electronic device needs. Using the HyperLight Load switching scheme, the MIC23603 maintains high efficiency throughout the entire load range while providing ultra-fast load transient response. The following sections provide additional device application information.

5.1 Input Capacitor

Place a 10 µF ceramic capacitor or greater close to the V_{IN} pin and PGND/GND pin for bypassing. The TDK C1608X5R0J106K, size 0603, 10 µF ceramic capacitor is recommended based upon performance, size, and cost. An X5R or X7R temperature rating is recommended for the input capacitor. Y5V temperature rating capacitors, aside from losing most of their capacitance over temperature, can also become resistive at high frequencies. This reduces their ability to filter out high frequency noise.

5.2 Output Capacitor

The MIC23603 was designed for use with a 47 µF or greater ceramic output capacitor. Increasing the output capacitance lowers output ripple and improves load transient response, but could increase solution size or cost. A low equivalent series resistance (ESR) ceramic output capacitor such as the TDK C3216X6S1A476M, size 1206, 47 µF ceramic capacitor is recommended based upon performance, size and cost. Both the X7R or X5R temperature rating capacitors are recommended. The Y5V and Z5U temperature rating capacitors are not recommended because of their wide variation in capacitance over temperature and increased resistance at high frequencies.

5.3 Inductor Selection

When selecting an inductor, consider the following factors (not necessarily in order of importance):

- Inductance
- Rated current value
- Size requirements
- DC resistance (DCR)

The MIC23603 was designed for use with a 0.33 µH to 1 µH inductor. For faster transient response, a 0.33 µH inductor yields the best result. For lower output ripple, a 1 μ H inductor is recommended.

Maximum current ratings of the inductor are generally given in two methods: permissible DC current and saturation current. Permissible DC current can be rated

either for a 40°C temperature rise or a 10% to 20% loss in inductance. Make sure that the inductor selected can handle the maximum operating current.

When saturation current is specified, make sure that there is enough margin so that the peak current does not cause the inductor to saturate. Peak current can be calculated using [Equation 5-1.](#page-14-0)

EQUATION 5-1:

$$
I_{PEAK} = \left[I_{OUT} + V_{OUT} \left(\frac{1 - V_{OUT} / V_{IN}}{2 \times f \times L} \right) \right]
$$

As [Equation 5-1](#page-14-0) shows, the peak inductor current is inversely proportional to the switching frequency and the inductance; the lower the switching frequency or the inductance, the higher the peak current. As input voltage increases, the peak current also increases.

The size of the inductor depends on the requirements of the application.

DC resistance (DCR) is also important. While DCR is inversely proportional to size, it can represent a significant efficiency loss. See [Efficiency](#page-14-1) [Considerations](#page-14-1) for information.

5.4 Compensation

The MIC23603 is designed to be stable with a 0.33 µH to 1 µH inductor with a minimum of 47 µF ceramic (X5R) output capacitor. A feed-forward capacitor (C_{FF}) in the range of 33 pF to 68 pF is recommended across the top feedback resistor to reduce the effects of parasitic capacitance and improve transient performance.

5.5 Duty Cycle

The typical maximum duty cycle of the MIC23603 is 80%.

5.6 Efficiency Considerations

Efficiency is defined as the amount of useful output power, divided by the amount of power supplied.

EQUATION 5-2:

$$
Efficiency = \left(\frac{V_{OUT} \times I_{OUT}}{V_{IN} \times I_{IN}}\right) \times 100
$$

Maintaining high efficiency serves two purposes. It reduces power dissipation in the power supply, reducing the need for heat sinks and thermal design considerations, and it reduces current consumption for battery powered applications. Reduced current draw from a battery increases the device's operating time and is critical in hand-held devices.

There are two types of losses in switching converters: DC losses and switching losses. DC losses are simply the power dissipation of 1^2R . Power is dissipated in the high side switch during the on cycle. Power loss is equal to the high side MOSFET R_{DSON} multiplied by the switch current squared. During the off cycle, the low side N channel MOSFET conducts, also dissipating power. Device operating current also reduces efficiency. The product of the quiescent (operating) current and the supply voltage represents another DC loss. The current needed to drive the gates on and off at a constant 4 MHz frequency and the switching transitions make up the switching losses.

FIGURE 5-1: Efficiency Under Load.

[Figure 5-1](#page-15-0) shows an efficiency curve, from no load to 300 mA. Efficiency losses are dominated by quiescent current losses, gate drive, and transition losses. By using the HyperLight Load mode, the MIC23603 can maintain high efficiency at low output currents.

Over 300 mA, efficiency loss is dominated by MOSFET R_{DSON} and inductor losses. Higher input supply voltages will increase the gate-to-source drive voltage on the internal MOSFETs, which reduces the internal R_{DSDN} . This improves efficiency by reducing DC losses in the device. All but the inductor losses are inherent to the device. In this case, inductor selection becomes increasingly critical in efficiency calculations. As the inductors get smaller, the DC resistance (DCR) can become quite significant. The DCR losses can be calculated in [Equation 5-3](#page-15-1).

EQUATION 5-3:

$$
P_{DCR} = I_{OUT}^2 \times DCR
$$

From that, the loss in efficiency due to inductor resistance can be calculated [Equation 5-5.](#page-15-2)

EQUATION 5-4:

$$
Efficiency Loss = \left[1 - \left(\frac{V_{OUT} \times I_{OUT}}{V_{OUT} \times I_{OUT} + P_{DCR}}\right)\right] \times 100
$$

Efficiency loss caused by DCR is minimal at light loads and gains significance as the load is increased. Inductor selection becomes a trade-off between efficiency and size.

5.7 HyperLight Load Mode

MIC23603 uses a minimum on and off time proprietary control loop. When the output voltage falls below the regulation threshold, the error comparator begins a switching cycle that turns the PMOS on and keeps it on for the duration of the minimum-on-time. This increases the output voltage. If the output voltage is over the regulation threshold, then the error comparator turns the PMOS off for a minimum-off-time until the output drops below the threshold. The NMOS acts as an ideal rectifier that conducts when the PMOS is off. Using an NMOS switch instead of a diode allows for lower voltage drop across the switching device when it is on. The asynchronous switching combination between the PMOS and the NMOS allows the control loop to work in discontinuous mode for light load operations. In discontinuous mode, the MIC23603 works in pulse frequency modulation (PFM) to regulate the output. As the output current increases, the off-time decreases, which provides more energy to the output. This switching scheme improves the efficiency of MIC23603 during light load currents by switching only when needed. As the load current increases, the MIC23603 goes into continuous conduction mode (CCM) and switches at a frequency centered at 4 MHz. The load when the MIC23603 goes into continuous conduction mode may be approximated by the formula in [Equation 5-5.](#page-15-2)

EQUATION 5-5:

$$
I_{LOAD} > \left(\!\frac{\left(V_{IN}-V_{OUT}\right)\times D}{2L\times f}\!\right)
$$

As shown in the previous equation, the load at which MIC23603 transitions from HyperLight Load mode to PWM mode is a function of the input voltage (V_{IN}) , output voltage (V_{OUT}), duty cycle (D), inductance (L), and frequency (f). As shown in [Figure 5-2](#page-16-0), as the Output Current increases, the switching frequency also increases, until the MIC23603 goes from HyperLight Load mode to PWM mode at approximately 300 mA. The MIC23603 switches a relatively constant frequency around 4 MHz after the output current is over 300 mA.

FIGURE 5-2: SW Frequency vs. Load Current.

6.0 PACKAGING INFORMATION

6.1 Package Marking Information

20-Lead 4.0 mm x 5.0 mm DFN Package Outline and Recommended Land Pattern

APPENDIX A: REVISION HISTORY

Revision A (July 2017)

- Converted Micrel document MIC23603 to Microchip data sheet template DS2005636A.
- Minor text changes throughout.

MIC23603

NOTES:

PRODUCT IDENTIFICATION SYSTEM

To order or obtain information, e.g., on pricing or delivery, contact your local Microchip representative or sales office.

Note 1: 1.DFN is GREEN RoHS-compliant package. Lead finish is NiPdAu. Mold compound is Halogen Free.

MIC23603

NOTES:

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